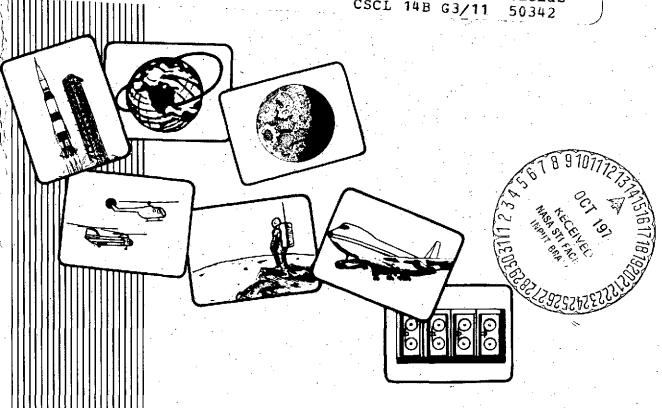
D2-118546-1

DYNAMIC DOCKING TEST SYSTEM (DDTS) ACTIVE TABLE FREQUENCY RESPONSE TEST RESULTS

(NASA-CR-140285) (NASA-CR-140285) DYNAMIC DOCKING TEST SYSTEM (DDTS) ACTIVE TABLE FREQUENCY RESPONSE TEST RESULTS (Boeing Aerospace Co., Houston, Tex.) 242 p HC \$15.25

N74-33777

Unclas CSCI 14B G3/11



BOEING COMPANY HOUSTON, TEXAS

August 30, 1974

DYNAMIC DOCKING TEST SYSTEM (DDTS) ACTIVE TABLE FREQUENCY RESPONSE TEST RESULTS

Contract NAS 9-13136

August 30, 1974

.Prepared by

R. M. Gates

Approved by

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Technical Program Manager

BOEING AEROSPACE COMPANY Houston, Texas

REVISIONS

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ABSTRACT

This document presents the results of the frequency response test performed on the Dynamic Docking Test System (DDTS) active table. Sinusoidal displacement commands were applied to the table and the dynamic response determined from measured actuator responses and accelerometers mounted to the table and one actuator.

KEY WORDS

Docking Simulator

Dynamic Docking Test System (DDTS)

Frequency Response Test

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TABLE

DDTS	TABLE	FREQUENCY	RESPONSE	TEST	ACCELEROMETERS		9
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REFERENCES

- Boeing Document D2-118544-1, "Mathematical Model for the Simulation of Dynamic Docking Test System (DDTS) Active Table Motion," August 30, 1974.
- Boeing Document D2-118544-2, "Dynamic Docking Test System (DDTS)
 Active Table Computer Program NASA Advanced Docking System (NADS),"
 August 30, 1974.

1.0 INTRODUCTION

The DDTS is a six-degree-of-freedom motion simulator developed to perform docking simulations using the USA and USSR docking hardware for the Apollo Soyuz Test Project. The simulator consists of a rigid structure supporting one set of docking hardware and active table to which the other set of docking hardware is attached as shown in Figure 1. The active table is a rigid structure supported by six hydraulic actuators. The motion of each actuator is controlled by an electronic control system which receives commands from equations of motion which provide the desired relative motions of the two spacecraft during docking.

Frequency response tests were conducted to determine the dynamic response of the active table to sinusoidal table motion commands. This document presents the results of these tests and compares them with analytical predictions provided by NASA Advanced Docking System (NADS), a computer program developed to model the dynamics of the active table in response to table motion commands. The mathematical model is derived in Reference 1, and the computer program is described in Reference 2.

2.0 INSTRUMENTATION

2.1 TABLE MOTION

Table displacements are determined by recording time-histories of the six actuator displacements measured by the linear potentiometers used in the displacement feedback of each actuator control system. These measured actuator lengths are then transformed to table displacements.

Simplified transformations from actuator lengths to table displacements are derived assuming small displacements about a nominal table position. Frequency response tests were run with no angular misalignments of the table; therefore, the Euler angles are zero. The inertial components of the actuator lengths at the reference position are then:

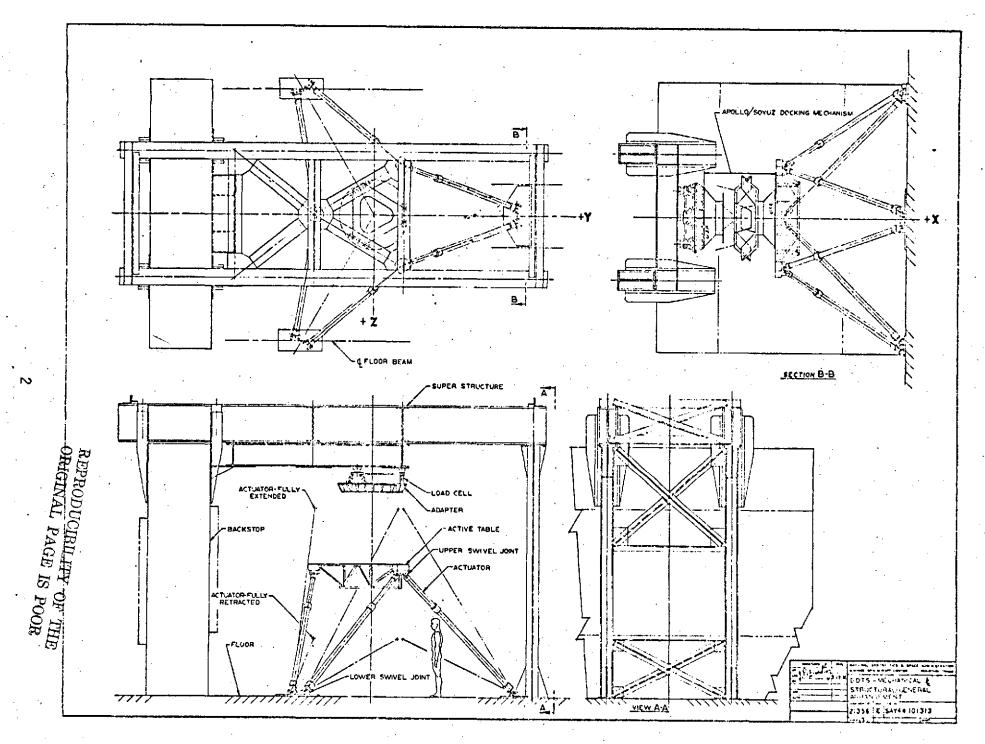


Figure 1. DDTS Simulator Facility

where x_{I_0} , y_{I_0} , and z_{I_0} are the initial inertial positions of the table c.g.; r_{xa_i} , r_{ya_i} , r_{za_i} , are the x, y, z coordinates of the $i\frac{th}{t}$ table swivel joint with respect to the table c.g.; and x_{f_i} , y_{f_i} , z_{f_i} are the inertial coordinates of the floor swivel joints for the $i\frac{th}{t}$ actuator (see Figure 2).

Initial actuator lengths are then:

$$l_{o_{i}} = \sqrt{r_{s_{x_{i}}}^{2} + r_{s_{y_{i}}}^{2} + r_{s_{z_{i}}}^{2}}$$
 (2)

For geometry transformation purposes, it can be assumed that r_s , r_y , and l_{o_i} are constant. Incremental motions of the actuators can then be transformed to table motions. The transformation between table coordinates and inertial coordinates is unity.

In general:

$$i_{p_i} = \left[r_{s_{x_i}} \dot{r}_{s_{x_i}} + r_{s_{y_i}} \dot{r}_{s_{y_i}} + r_{s_{z_i}} \dot{r}_{s_{z_i}} \right] / l_{p_i}$$
 (3)

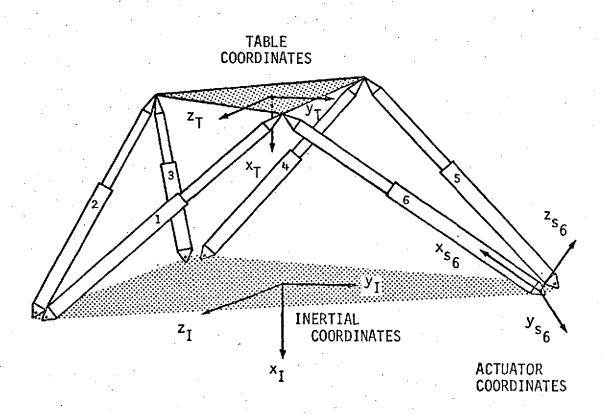


Figure 2. Active Table Coordinate Systems

but, if we let

$$\begin{cases}
\dot{r}_{S_{x_{i}}} \\
\dot{r}_{S_{y_{i}}} \\
\dot{r}_{S_{z_{i}}}
\end{cases} = \begin{cases}
\dot{x}_{T} \\
\dot{y}_{T} \\
\dot{z}_{T}
\end{cases} + \begin{bmatrix}
0 & -\omega_{z} & \omega_{y} \\
\omega_{z} & 0 & -\omega_{x} \\
-\omega_{y} & \omega_{x} & 0
\end{bmatrix} \begin{Bmatrix} r_{xa_{i}} \\ r_{ya_{i}} \\ r_{za_{i}}
\end{cases}$$
(4)

where \dot{x}_T , \dot{y}_T , \dot{z}_T are table translational velocities at any centerline reference point, and ω_x , ω_y , ω_z are table angular velocities.

A system of six equations (one for each actuator) and six unknowns $(\dot{x}_T, \dot{z}_T, \dot{z}_T, \omega_x, \omega_y, \omega_z)$ can be written and solved.

$$\begin{bmatrix} A \end{bmatrix} \begin{pmatrix} \dot{x}_T \\ \dot{y}_T \\ \dot{z}_T \\ \omega_X \\ \omega_y \\ \omega_z \end{pmatrix} = \begin{pmatrix} \dot{1}_1 \\ \dot{1}_2 \\ \dot{1}_3 \\ \dot{1}_4 \\ \dot{1}_5 \\ \dot{1}_6 \end{pmatrix}$$
 (5)

hence:

$$\begin{pmatrix}
\dot{x}_{T} \\
\dot{y}_{T} \\
\dot{z}_{T} \\
\omega_{x} \\
\omega_{y} \\
\omega_{z}
\end{pmatrix} = \begin{bmatrix} A \end{bmatrix}^{-1} \begin{pmatrix} i_{1} \\ i_{2} \\ i_{3} \\ i_{4} \\ i_{5} \\ i_{6} \end{pmatrix} (6)$$

The elements of the $i^{\frac{th}{m}}$ row of the [A] matrix are:

$$A_{i1} = r_{s_{x_{i}}} / l_{o_{i}}$$

$$A_{i2} = r_{s_{y_{i}}} / l_{o_{i}}$$

$$A_{i3} = r_{s_{z_{i}}} / l_{o_{i}}$$

$$A_{i4} = \left(-r_{s_{y_{i}}} r_{za_{i}} + r_{s_{z_{i}}} r_{ya_{i}}\right) / l_{o_{i}}$$

$$A_{i5} = \left(r_{s_{x_{i}}} r_{za_{i}} - r_{s_{z_{i}}} r_{xa_{i}}\right) / l_{o_{i}}$$

$$A_{i6} = \left(-r_{s_{x_{i}}} r_{ya_{i}} + r_{s_{y_{i}}} r_{xa_{i}}\right) / l_{o_{i}}$$

Likewise, the same transformation can be used to solve for incremental table displacements relative to its initial position.

$$\begin{pmatrix}
\Delta x_{T} \\
\Delta y_{T} \\
\Delta z_{T} \\
\Delta \theta_{X} \\
\Delta \theta_{y} \\
\Delta \theta_{z}
\end{pmatrix} = \begin{bmatrix} A \end{bmatrix}^{-1} \begin{cases}
1_{1} - 1_{o_{1}} \\
1_{2} - 1_{o_{2}} \\
1_{3} - 1_{o_{3}} \\
1_{4} - 1_{o_{4}} \\
1_{5} - 1_{o_{5}} \\
1_{6} - 1_{o_{6}}
\end{cases} (8)$$

where:

$$\Delta\theta_{\mathbf{X}} = \phi$$

$$\Delta\theta_{\mathbf{y}} = \theta$$

$$\Delta\theta_{\mathbf{z}} = \psi$$
Euler angles (9)

2.2 ACCELERATIONS

Accelerometers were mounted to the active table and to one of the six hydraulic actuators. Figure 3 shows the location of the ten accelerometers available. One triaxial accelerometer is mounted to the active table truss structure and measures accelerations in the x, y, and z directions. A second triaxial accelerometer mounted to the table corner measures x, radial, and tangential accelerations. Actuator 6 accelerations are measured at the top of the cylinder in two orthogonal lateral directions and the axial direction. Actuator extension accelerations are measured by a Kistler servo accelerometer mounted to the upper end of the actuator piston.

The table on Page 9 shows the accelerometers recorded and those used as abort limit cues.

2.3 HYDRAULIC PRESSURES

Hydraulic pressure measurements were recorded on oscillograph recorders for each actuator. Due to recorder channel limitations, supply pressure measurements for all six actuators were measured while differential pressure measurements for actuators 1 through 5 were recorded. Differential pressures were obtained from the pressure feedback signals in the control system for each actuator.

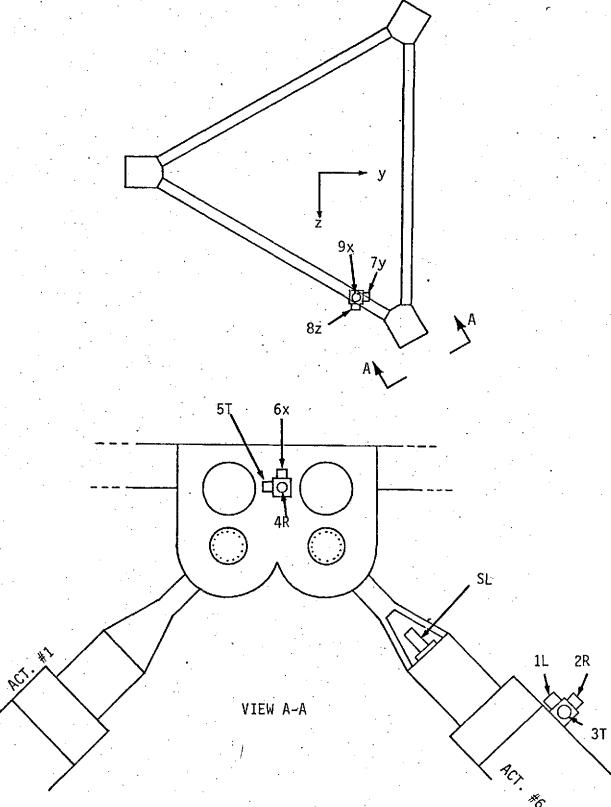


Figure 3. Active Table Accelerometer Locations

DDTS TABLE
FREQUENCY RESPONSE TEST ACCELEROMETERS

	•	· ·	
ACCEL. NO.	RECORD ON TAPE	USED AS ABORT LIMIT.	LIMIT ACCEL.
1L			
2R	Х	X	±3.0 g
3T	<u>,</u> X	X	±3.0 g
4R	X		
5T	X		
6X			
7 Y	X	X	±3.0 g
87	X	X	±3.0 g
9X	Х	X	±3.0 g
SL	. X	•	

3.0 TEST INPUTS

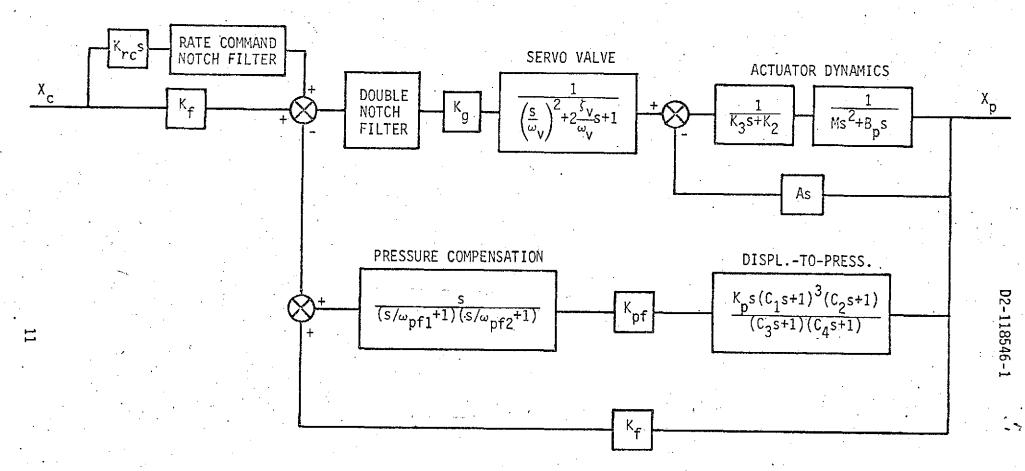
The frequency response test was conducted with the table positioned on the simulator centerline with the actuators at mid-stroke ($x_{I_0} = 88.159$; $y_{I_0} = z_{I_0} = 0$). Sinusoidal table commands of 0.05 inch amplitude were used in each of the x, y, and z directions.

Commanded actuator lengths are determined from

where the terms of the [A] matrix are defined in equation (7).

During docking simulations, each actuator receives a position command and a velocity command as indicated in the actuator control system block diagram shown in Figure 4. However, for the frequency response test, the rate command gain, K_{rc} , was set to zero because the automatic signal generator used in the test was not capable of generating a constant amplitude sine sweep position command and a corresponding rate command simultaneously.

To minimize the magnitudes of table and actuator responses and to reduce the wear and tear on the linear potentiometers, a .05 inch magnitude sinusoidal table position command signal was used. An automatic frequency sweeping signal generator was used to sweep from 1.0 Hz to 40 Hz in 1.0 Hz increments. Fifteen cycles of command signal were used at each frequency.



RATE COMMAND NOTCH FILTER =
$$\frac{(s/\omega_c)^2 + D_{cn}s + 1}{(s/\omega_c)^2 + D_{cd}s + 1}$$

$$K_3 = \frac{\text{Vol.}}{4 \beta_e}$$

DOUBLE NOTCH FILTER =
$$\frac{(s^2 + 51680.)(s^2 + 725690.)}{(s^2 + 533.3 s + 51680.)(s^2 + 533.4 s + 725690.)}$$

Figure 4. Single-Axis Servo Block Diagram

4.0 FREQUENCY RESPONSE PREDICTIONS

Frequency response characteristics of the table for position commands in the x, y, and z directions were obtained using NADS computer program (References 1 and 2). These predictions are shown in Figure 5. The table frequency response exhibits two resonances—one at the hydraulic resonant frequency (\sim 30 Hz) and another which corresponds to the bending frequency of the actuators (\sim 11 Hz). In the lateral directions, the hydraulic resonance occurs at approximately 22 Hz due to increased effective mass in the lateral direction.

Table and actuator acceleration predictions for each test were also obtained (Figures 6 and 7). Based on these acceleration predictions, a table and actuator acceleration limit of ±3.0 g was established to preclude possible damage to the table or actuators. Accelerometers on the table and actuator 6 (see Section 2.1) were monitored during the test, and an automatic abort capability was utilized.

5.0 TEST RESULTS

Frequency response tests were attempted in the x, y, and z directions. The first test (z-axis) was aborted automatically at 9 Hz due to measured accelerations exceeding the abort limit of 2.5 g. The abort limit was raised to 3.0 g, and the test was rerun. Again the test was automatically aborted at 9 Hz due to excessive accelerations.

It was apparent that the table possessed a resonant peak in the 10-15~Hz range which is higher in magnitude than predicted. Therefore, to prevent possible damage to the table, actuators, or potentiometers, the tests in the y and x directions were conducted using the same 3.0~g abort limit. The y-axis test was automatically aborted at 9~Hz, and the x-axis test was aborted at 11~Hz.

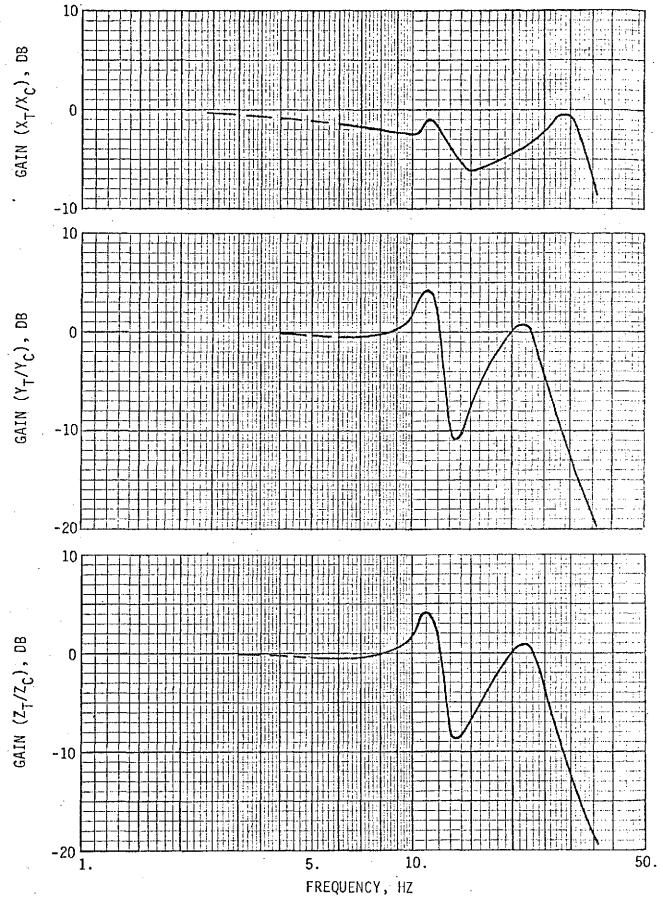


Figure 5. Table Displacement Prediction

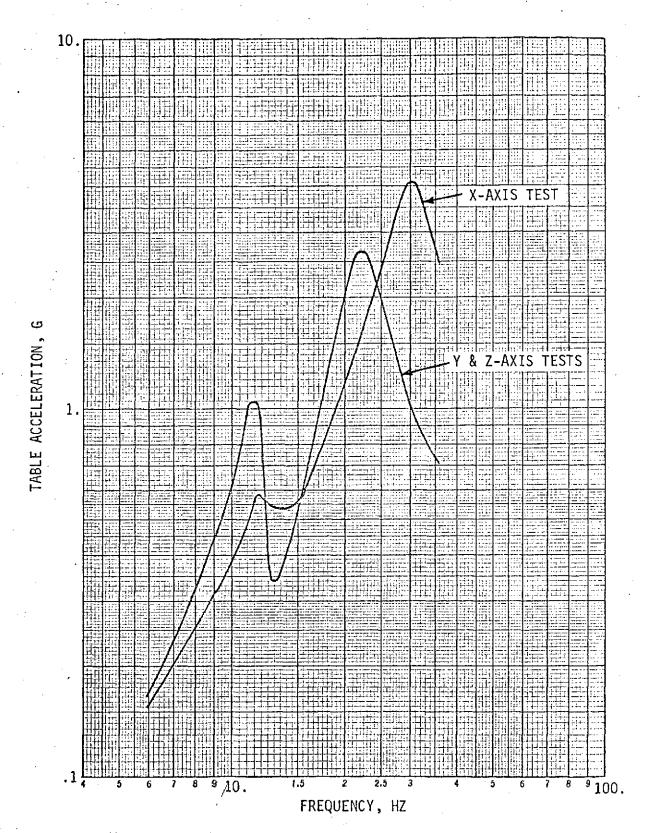


Figure 6. Table Acceleration Prediction

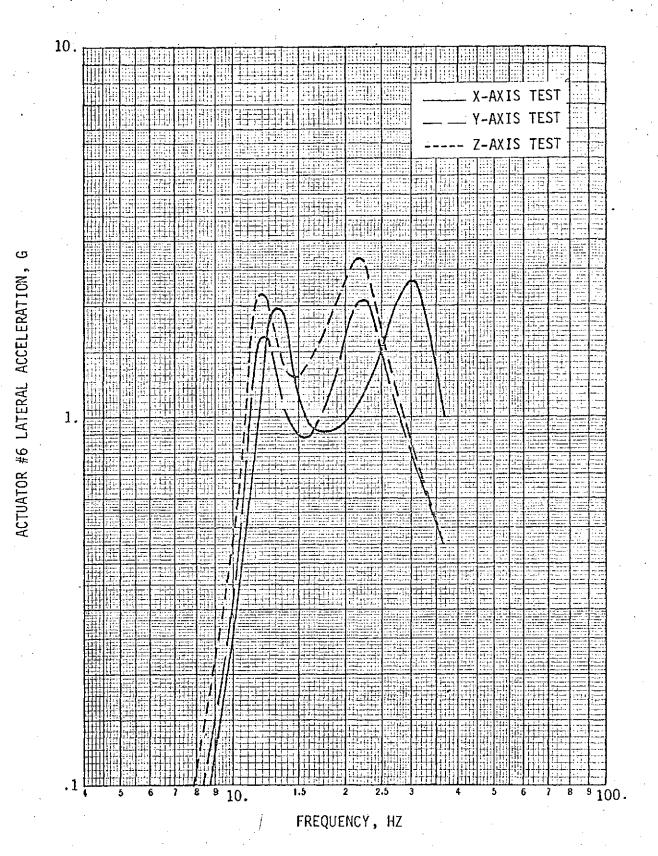


Figure 7. Actuator Acceleration Prediction

A comparison of frequency response test table motions with predicted table displacements is shown in Figure 8. A complete set of table motion frequency response test data is presented in the appendices. Measured table accelerations are compared with predicted table accelerations in Figure 9. Figure 10 compares measured actuator lateral accelerations at the upper end of actuator 6 cylinder with predicted actuator accelerations.

The cause of the higher dynamic responses has not been identified. Reducing the damping associated with actuator bending dynamics resulted in slightly higher analytical table dynamics, but could not account for the observed difference.

The analytical frequency response predictions show negligible coupling between table responses in the commanded direction and responses in the other directions. Test results show that the off-axis coupling was less than 30 percent of the commanded table motion at frequencies below 10 Hz. Test results shown in the appendices indicate that the coupling becomes more significant as the command frequency approaches the resonant frequency of the table.

6.0 CONCLUSIONS AND RECOMMENDATIONS

The DDTS active table exhibits significantly higher dynamic characteristics than was predicted. It is recommended that further study be conducted to understand this discrepancy. This information is desirable so that the feasibility of utilizing the DDTS to perform other dynamic motion simulations and dynamic tests can be assessed.

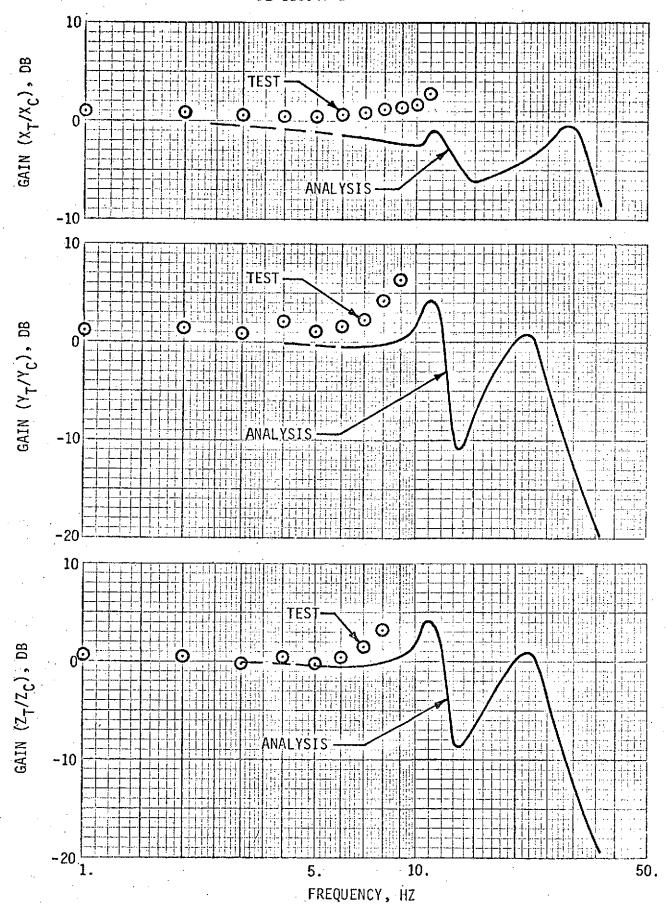


Figure 8. Table Displacement Frequency Response

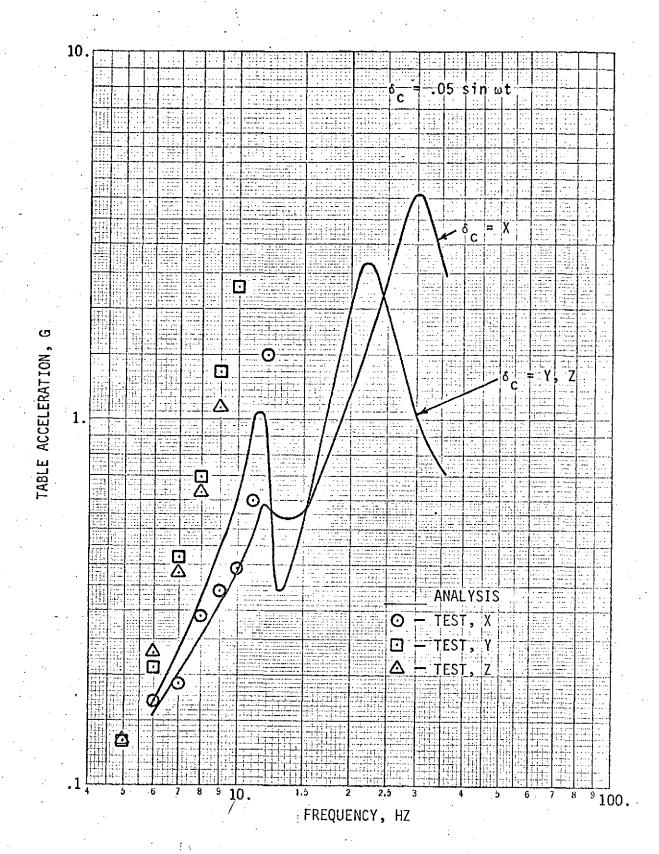


Figure 9. Table Accelerations, Frequency Response Test

Figure 10. Actuator Accelerations, Frequency Response Test

APPENDIX A

TEST NO. 1 Z-AXIS

DDTS FREQUENCY RESPONSE TEST SUMMARY OF INPUT INERTIAL CONDITIONS AND TRANSFORM MATRIX

FREQUENCY RESPONCE TEST 1

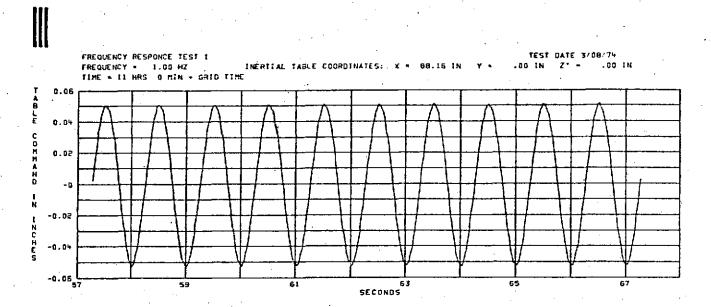
TEST CATE 3/08/79

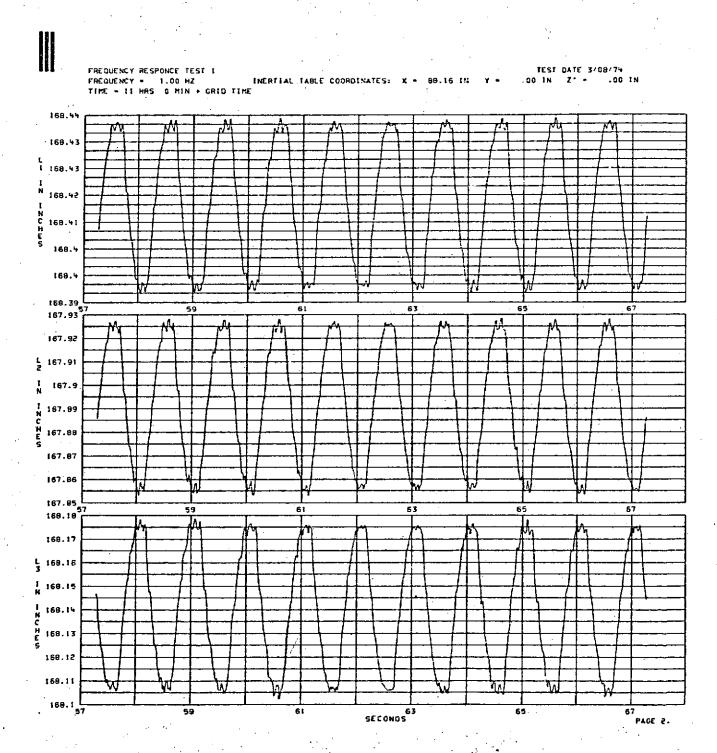
•				x	Y	Z			
	•	TABLE CO	ORDINATES	68.159	.cco	.000			
•	reave Tible	SHIVEL JOINTS	FLOOR	SHIVEL J	DINTS	COMPONENTS	OF ACTUAT	OR LENGTH	ACTUATOR
	SERVO FABLE	SHITEE DOTRES		¥	7	x	Y	Ž	LENGTH
ACTUATOR	x	1 4	• •		•				
_	.0000 25	1.1020 49.5000	210.4070	-64.3110	123.1780	-122.2483	89.4130	-73.6720	168.4272
a		5,4190 3.0000		-76.3809	116.1240	-122.2700	20.9610	-113.1240	167-8679
_		1.4190 -3.0000	210.4220	-74.5730	-116.8193	-122.2630	19.1540	113.0190	169.1365
		.1020 -49.5000	210.4170	-62.4120	-123.6836	-122.2580	87.5140	74.1830	167.6569
5		.2980 -46.5000	210.4100	138.4639	-5.9750	-122.2510			169.1881
Ž.		.2980 46.5000	210.3690	138.3890	8.0550	-122.2100	-108.0910	38.4950	167.6330

TRANSFORM MATRIX

227798+00	229422+00	228575+00	229554 • 00	228265+00	2305:0+00
-447118+00	236022-01	303266-01	.442709-00	4!6853+30	410525+00
222802-00			.228740+00	276033+00	.268561-00
450573-02				450071-02	.446595-02
648215-02				.794358-02	796988-02
	835884-02			.209540-02	.29:976-02

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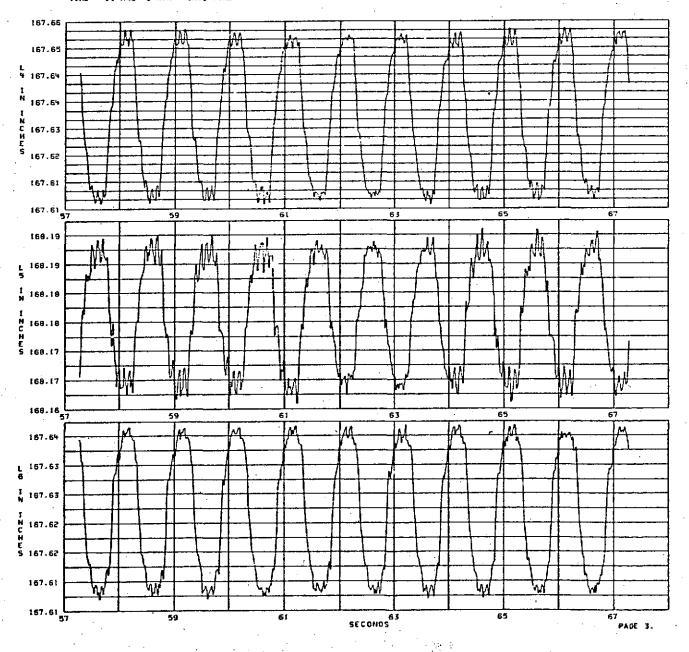




FREQUENCY RESPONCE TEST 1

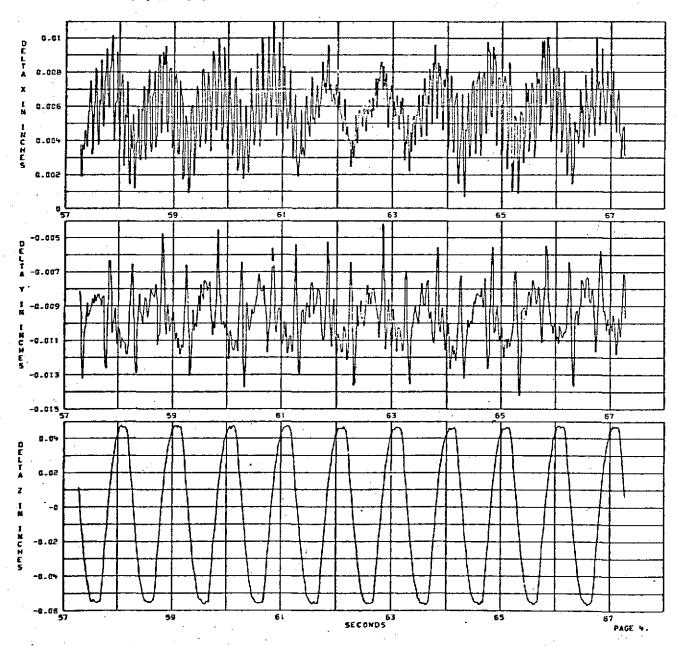
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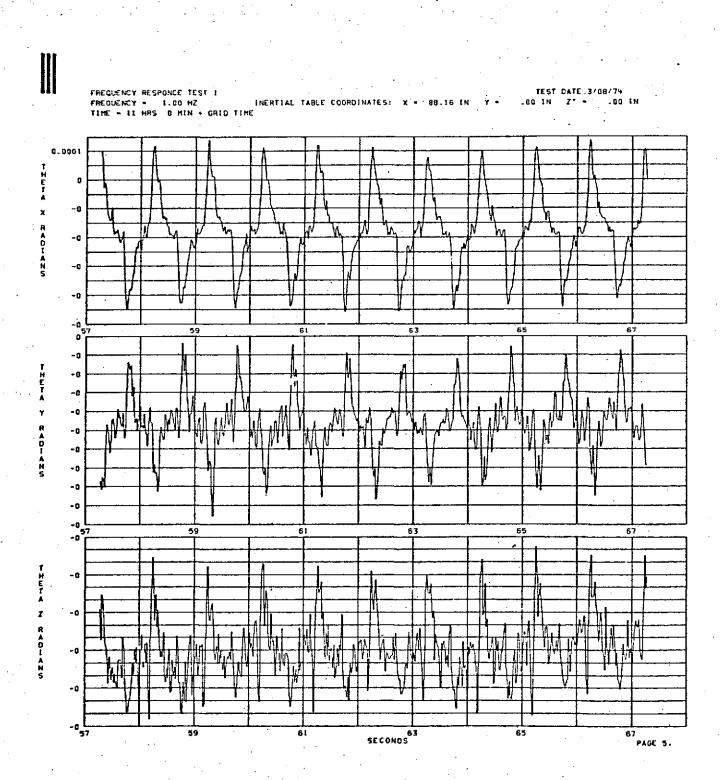
TIME = 11 HRS 0 MIN + ORIO TIME

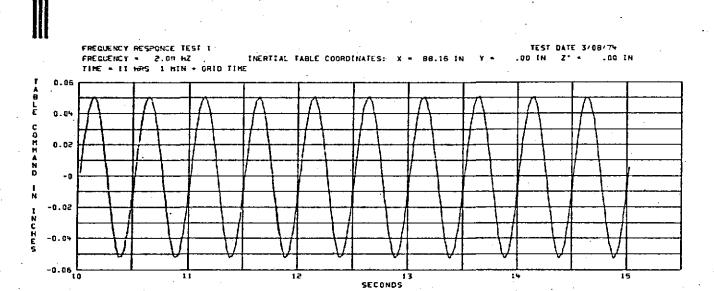


FREQUENCY RESPONCE TEST 1

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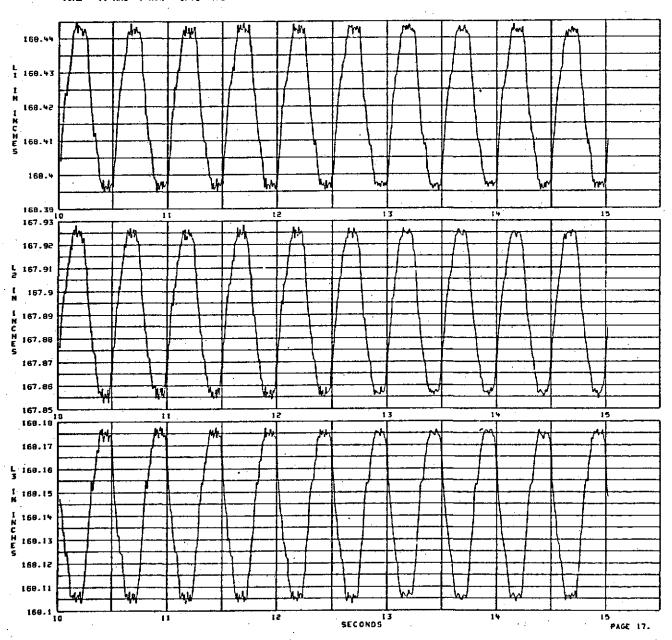




FREQUENCY RESPONCE TEST 1

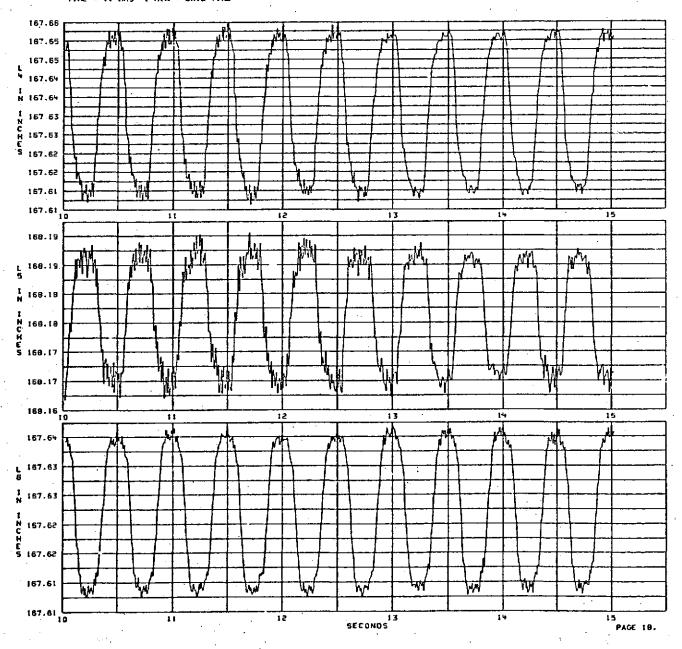
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TIME = 11 HRS | 1 HIM + ORIO TIME





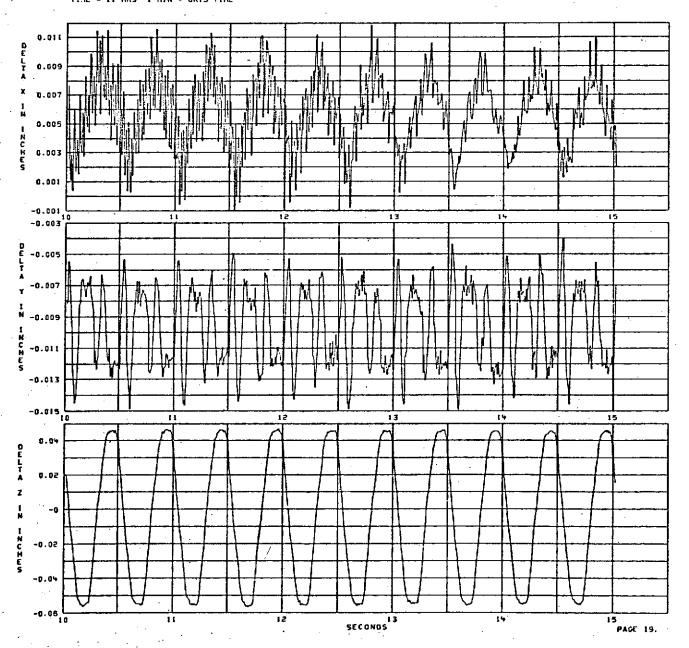
FREQUENCY RESPONCE TEST 1 TEST DATE 3/08/74 FREQUENCY = 2.00 HZ THERTIAL TABLE COORDINATES: X = 68.16 IN Y = .00 IN $Z^* = .00$ IN Time = 11 HRS | I HIN + ORIO TIME

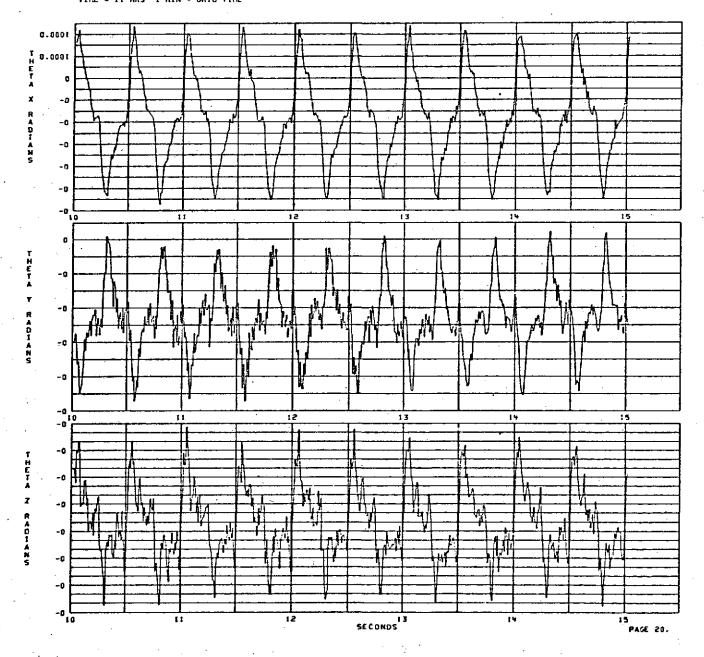


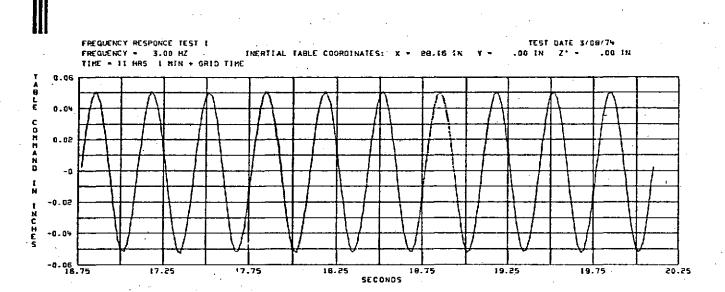


FREQUENCY RESPONCE TEST 1

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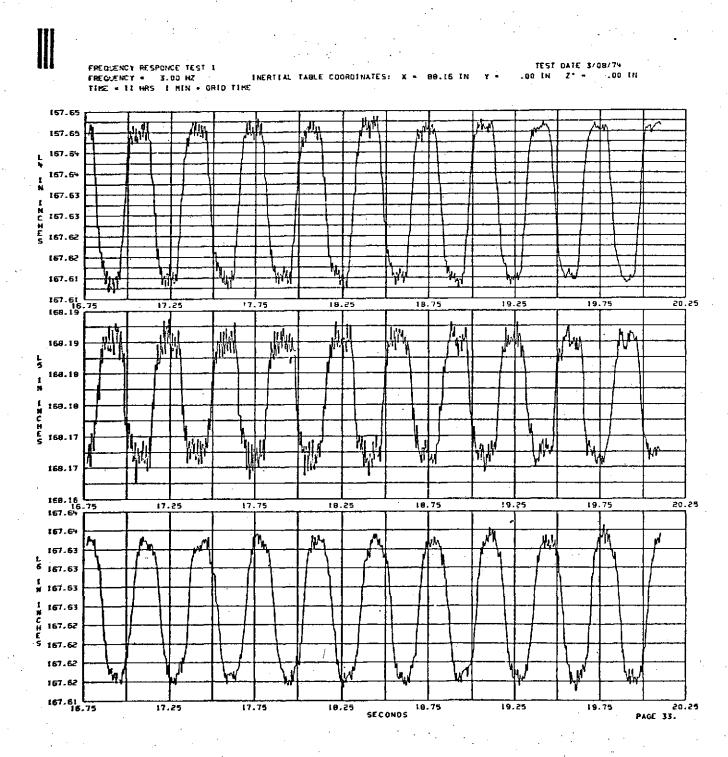


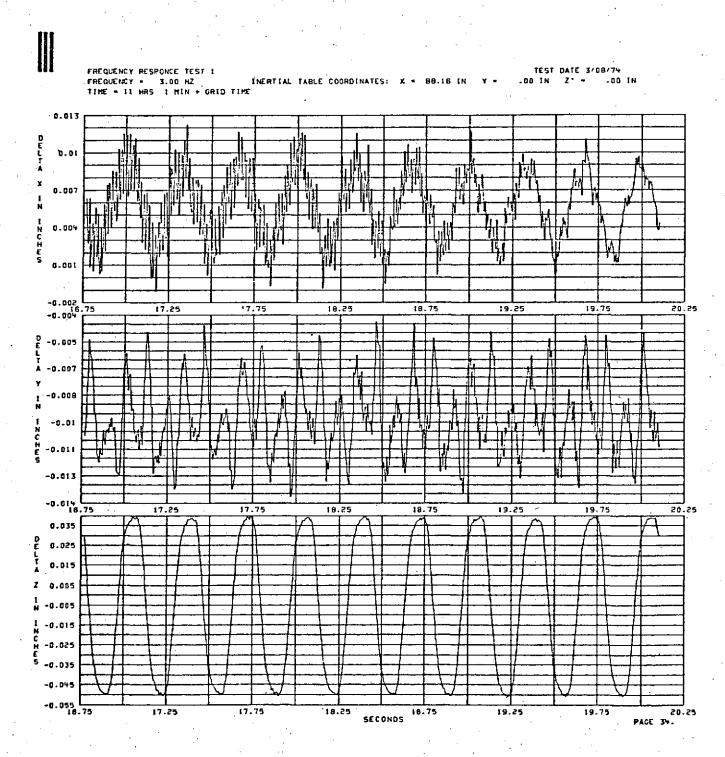


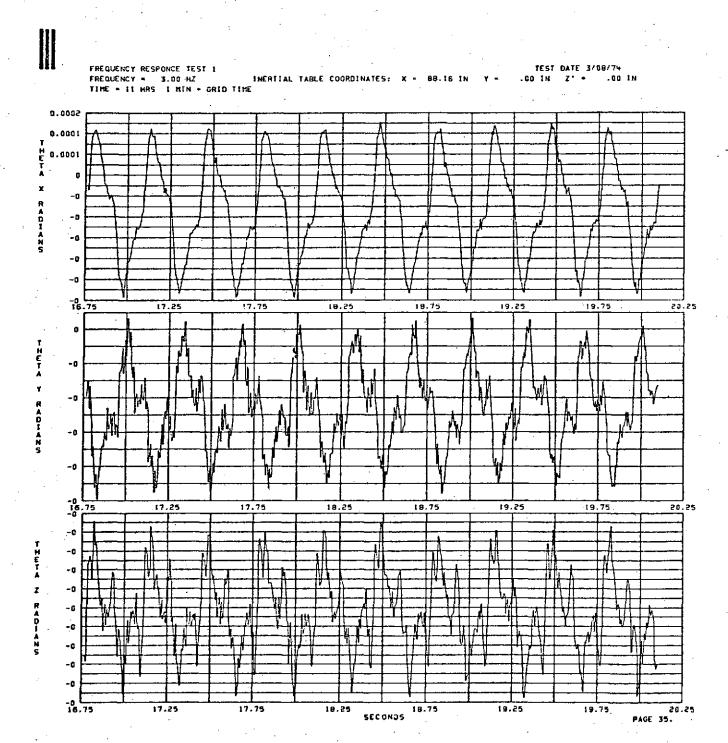


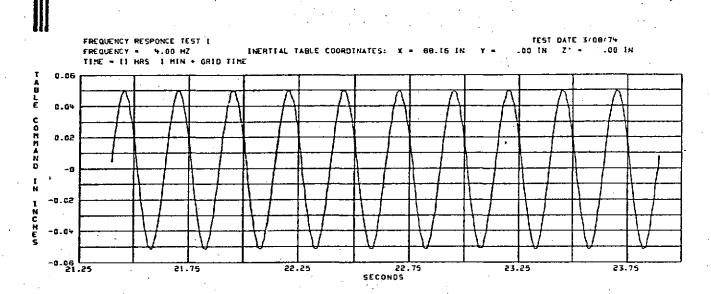
PAGE 31

FREQUENCY RESPONCE TEST 1
FREQUENCY = 3.00 HZ
TIME = 11 HRS 1 HIN + GRID TIME INEPPIAL TABLE COGRDINATES: X = 88.16 IN 168.44 168.43 168.43 160.42 168.42 N C 168.41 H E 168.41 168.4 168.4 168.39 16.75 167.93 17.25 17.75 18.25 18.75 19.25 19.75 20.25 167.92 L N 167.9 С н 167.89 Е S 167.87 167.96 16.75 18.25 19.25 19.75 17.25 17,75 18.75 20.25 141 169.16 \$ 168.15 160.14 166.13 160.12 17.25 20.25 PAGE 32. 17.75 18.25 18.75 19.25 SECONDS





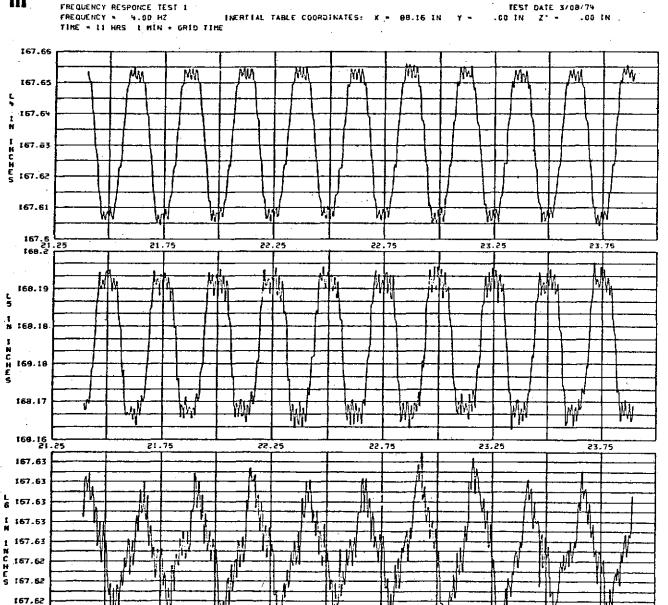




PAGE 48

FREQUENCY RESPONCE TEST 1 TEST DATE 3/08/74 .CC IN FREQUENCY = 4.00 HZ TIME = 11 H9S | 1 HIN + GRID TIME INERTIAL TABLE COORDINATES: X = 88.16 IN .00 IN 169.44 168.43 1 160.43 168.42 168.42 N C 168.41 H E S 168.41 168.4 168.4 168.39 21.75 22.25 22.75 23.25 23.75 157.93 167.92 167.91 I N 167.9 167.89 H E 167.88 167.87 167.86 167. 85 21.25 168.18 23.25 22.25 22.75 21.75 23.75 168.17 L 168.15 1 168.15 169.14 Ĉ ₩ 188.13 189.12 168.11 SECONDS 23.75 PAGE 49. 21.75 22.25 23.25

167.62



\$2.75 SECONDS 23.25

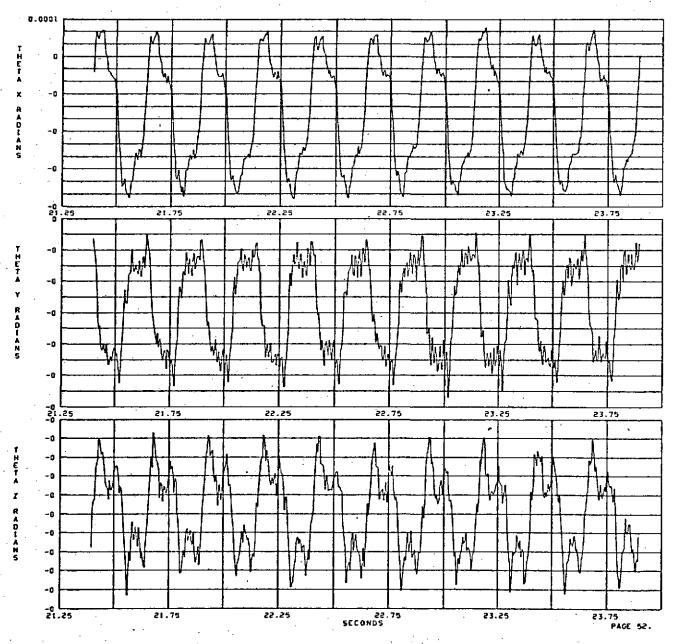
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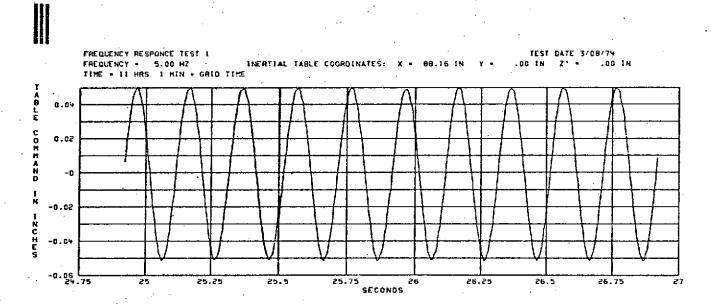
FREQUENCY RESPONCE TEST 1 FREQUENCY = 4.00 HZ TIME = 11 HRS | MIN + GRID TIME INERTIAL TABLE COORDINATES: X . 0.01 Å. 0.008 0.006 0.004 0.002 -0.002 21.75 22.25 22.75 -0.004 -0.006 -0.008 -0.61 -0.012 -0.014 -0.016 -0.018 22.25 22.75 23.25 23.75 0.04 0.02 -0.02 -0.04 22.75 SECONOS 22.25 23.25 23.75 PAGE 51.

FREQUENCY RESPONCE TEST 1

FREQUENCY = 4.00 HZ INERTIAL TABLE COORDINATES: X = 88.16 IN Y = .00 IN Z = .00 I

TIME = 11 HRS I MIN + GRID TIME





FREQUENCY RESPONSE TEST 1
FREQUENCY - 5.00 HZ
TIME - 11 HRS 1-MIN + GRID TIME INERTIAL TABLE COORDINATES: 168.44 168.44 k 169.42 168.42 C H 168.41 E S 168.41 168.41 168.4 168.4 168.39 167.93 26.75 25.25 26.5 25.25 167.92 L 167.91 167.9 167.90 157.87 167.85 26.25 26.75 25.25 168.18 168.17 168.15 168.14 H € 168.13 169.12 168.11

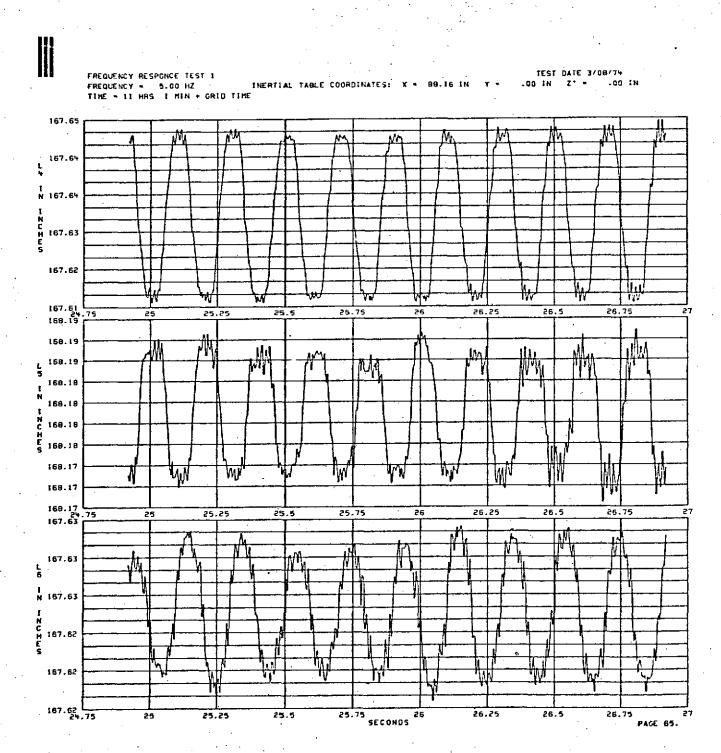
25.75

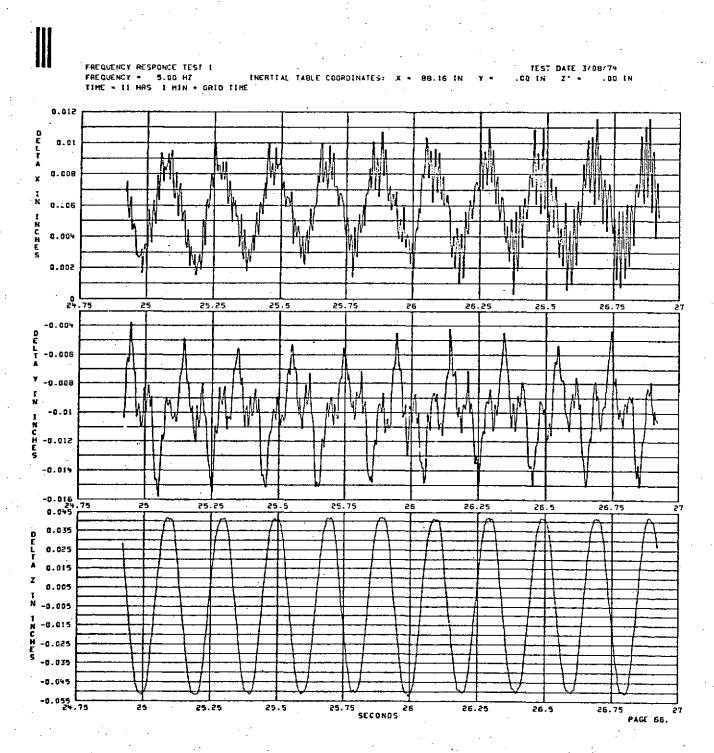
26.25

26.5

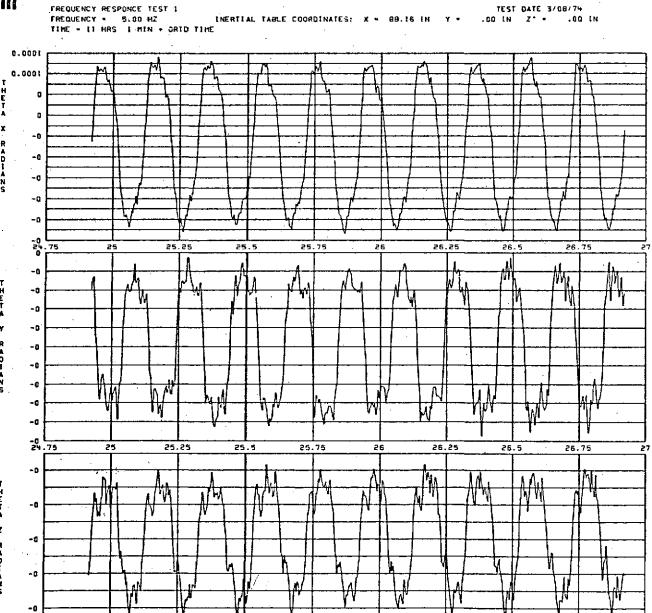
26.75

25.25



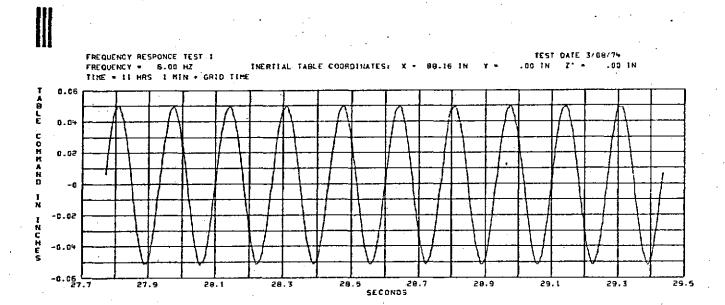






25.75 26 SECONDS

PAGE 67.

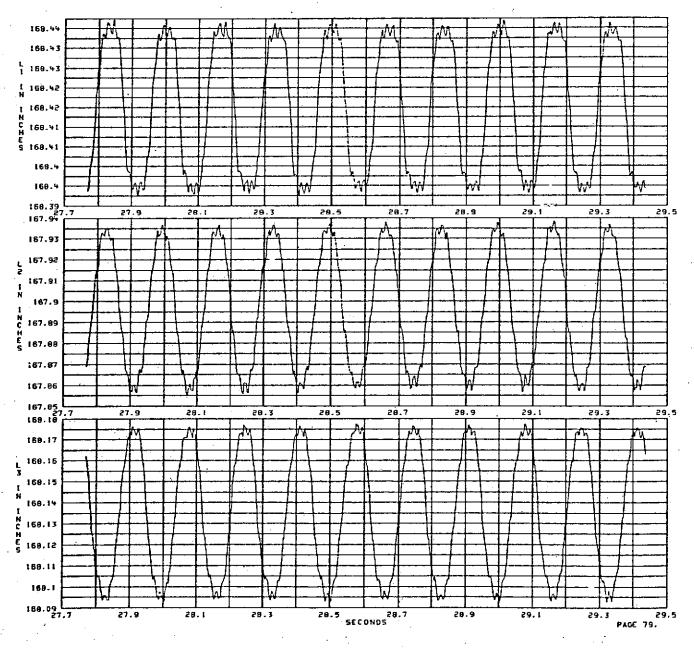


PAGE 78

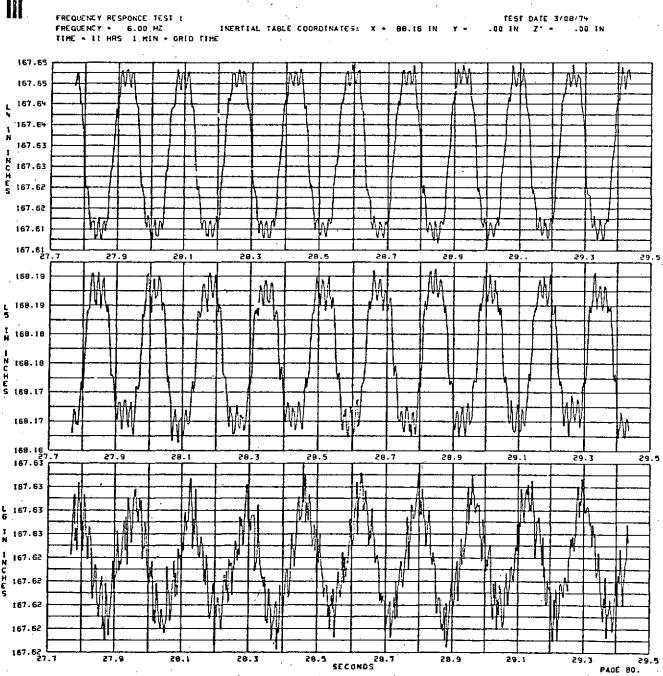
FREQUENCY RESPONCE TEST I

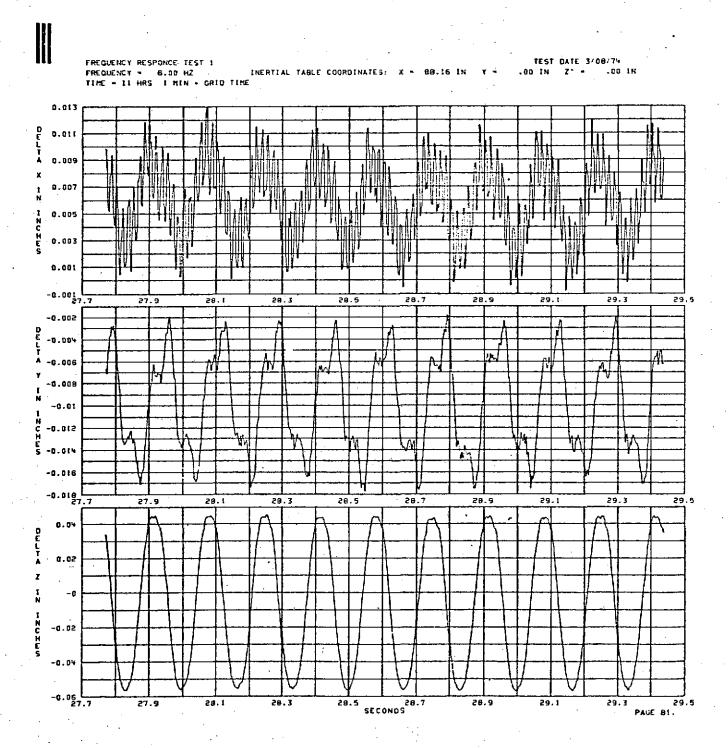
FREQUENCY = 6.00 HZ INERTIAL TABLE COORDINATES: X = 88.16 IN Y = .00 IN Z = .00 IN

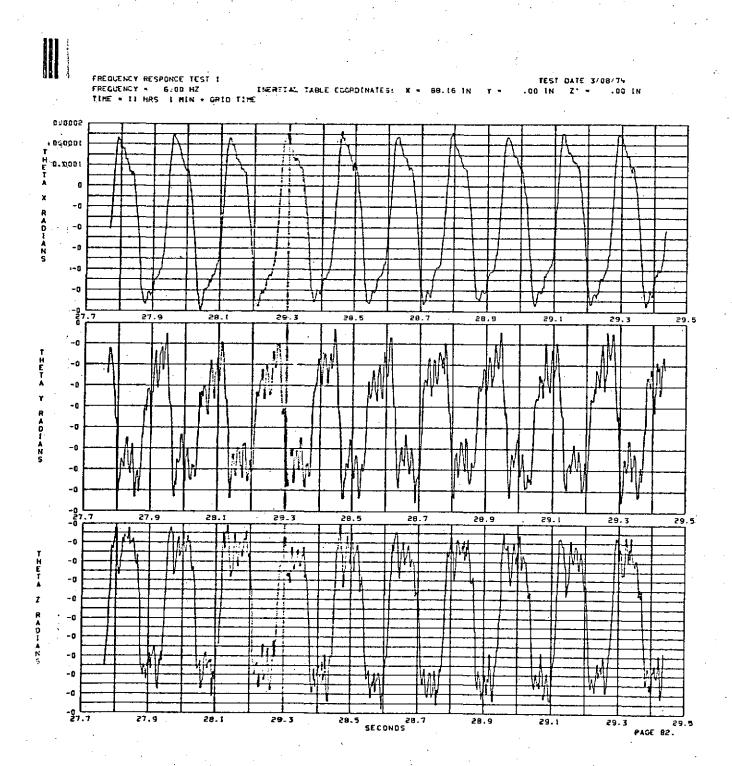
TIME = 11 HRS I MIN + GRID TIME



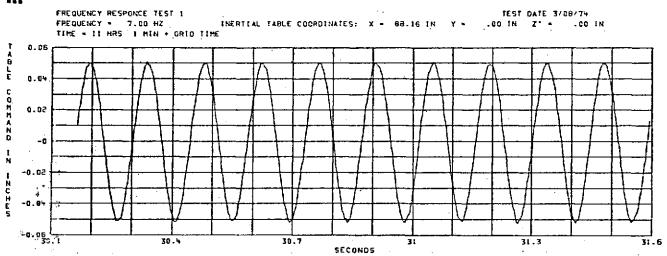




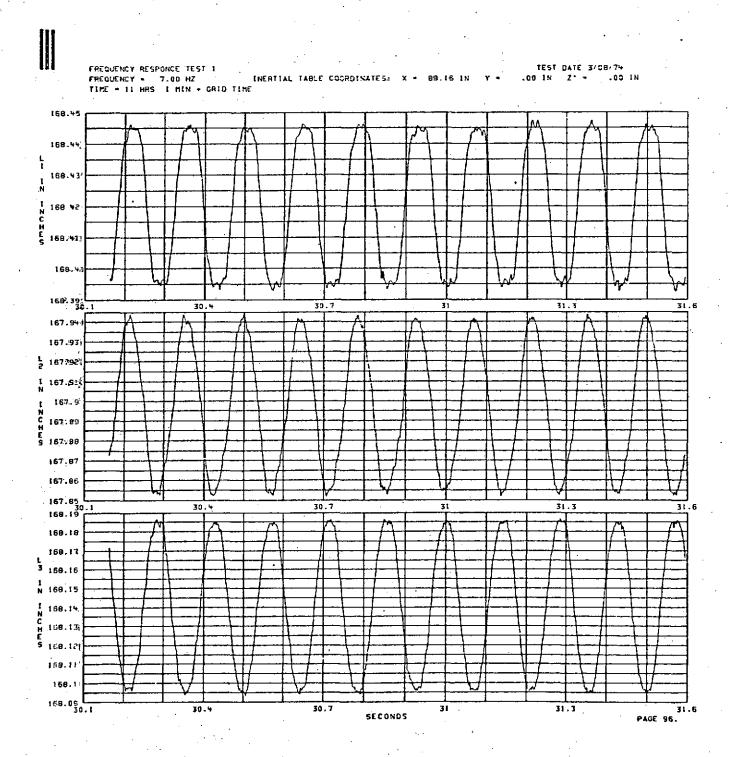


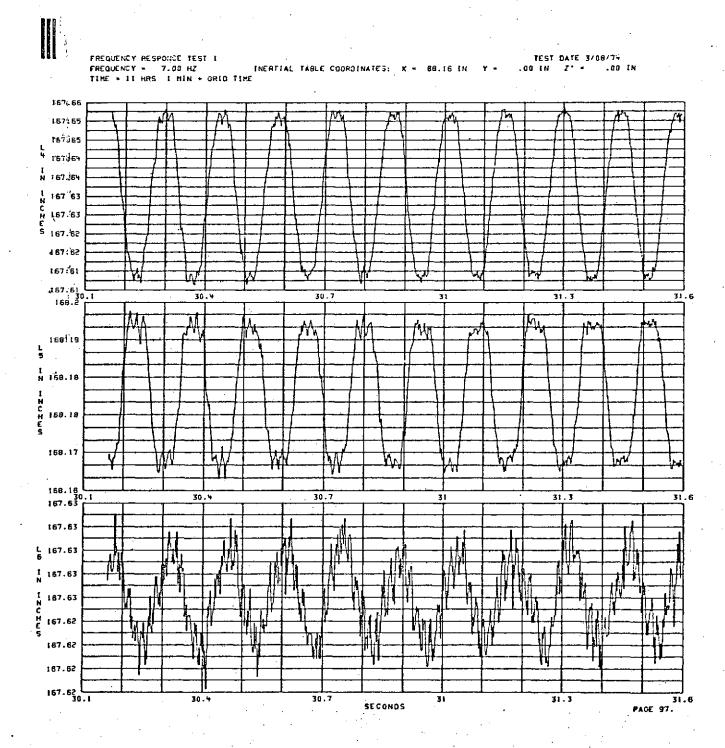


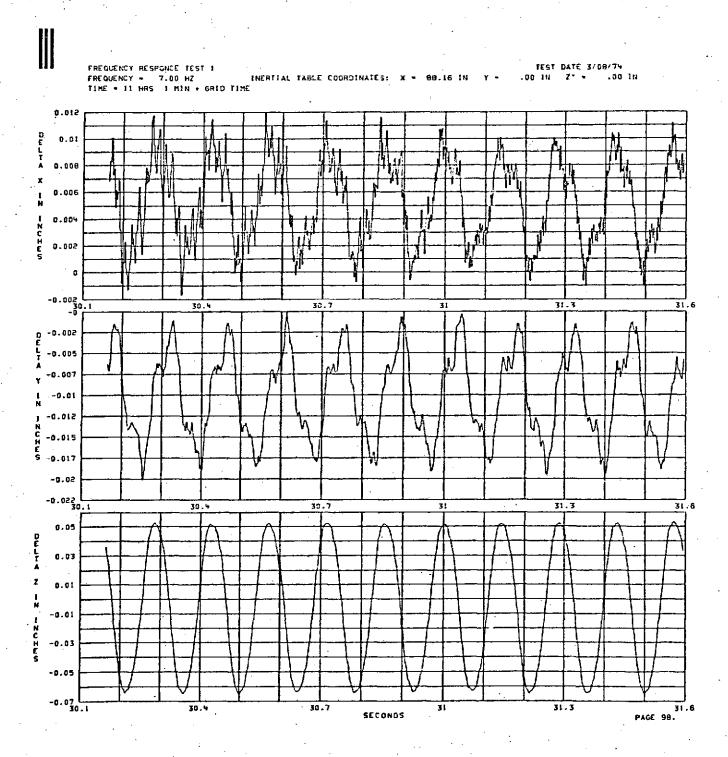




PAGE 95

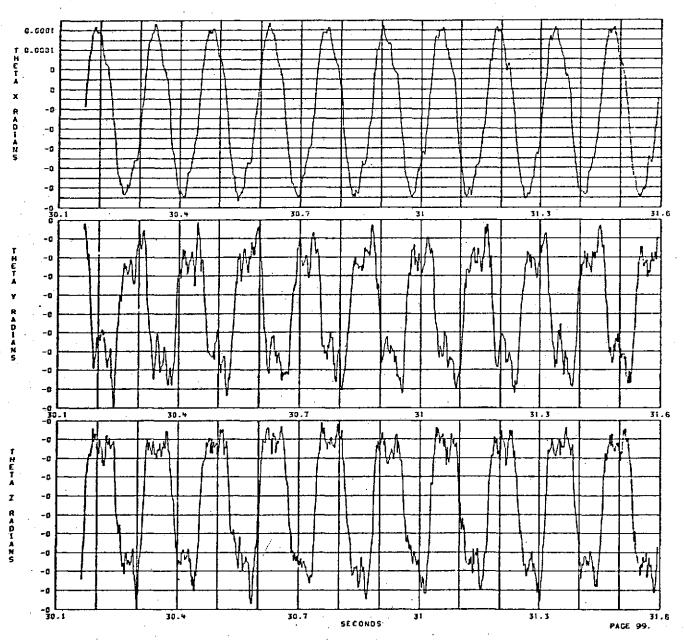


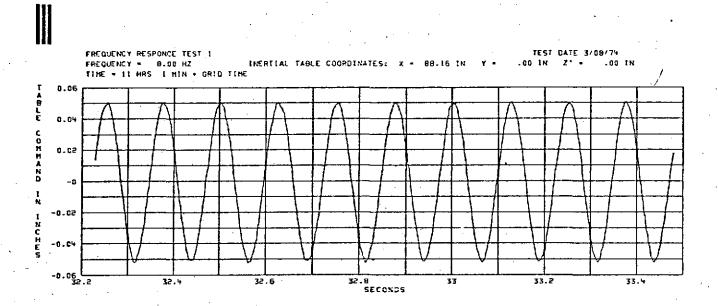




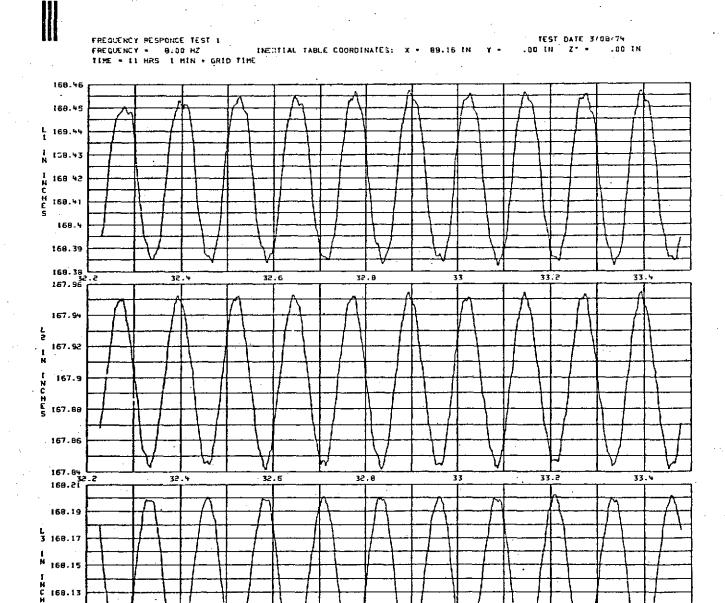


FREQUENCY RESPONSE TEST 1 TEST DATE 3/08/74 FREQUENCY = 7.00 HZ INERTIAL TABLE COORDINATES: X = BB.16 IN Y = .00 IN Z* = .00 IN TIME = II HRS 1 MIN + ORIO TIME





PAGE 115.



32.6

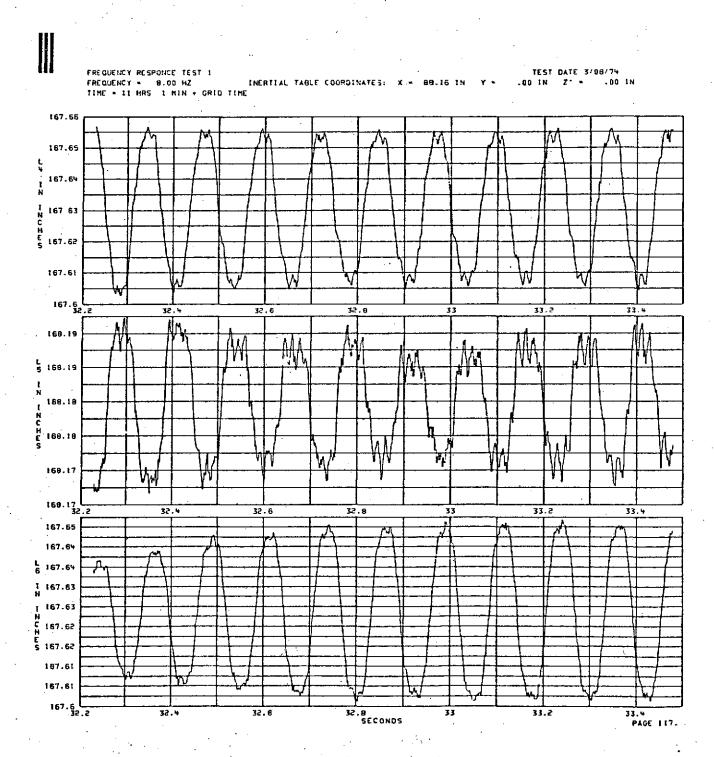
32.8 SECONDS 33.2

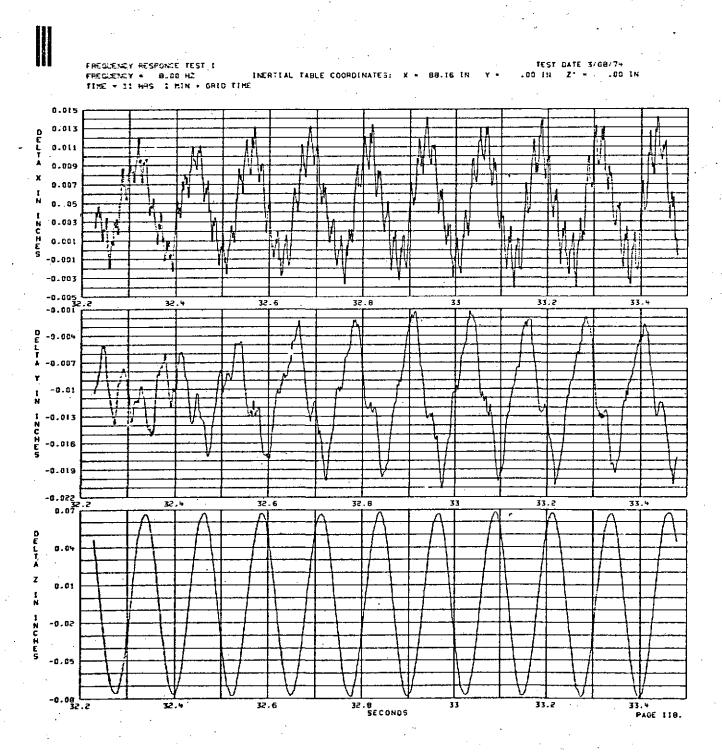
33.4 PAGE 116.

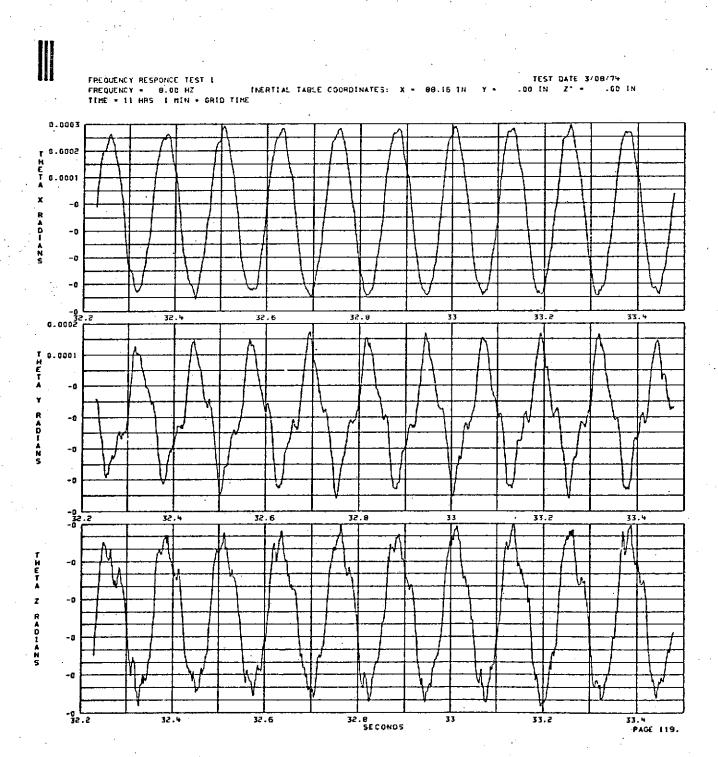
168.11

168.09

168.07





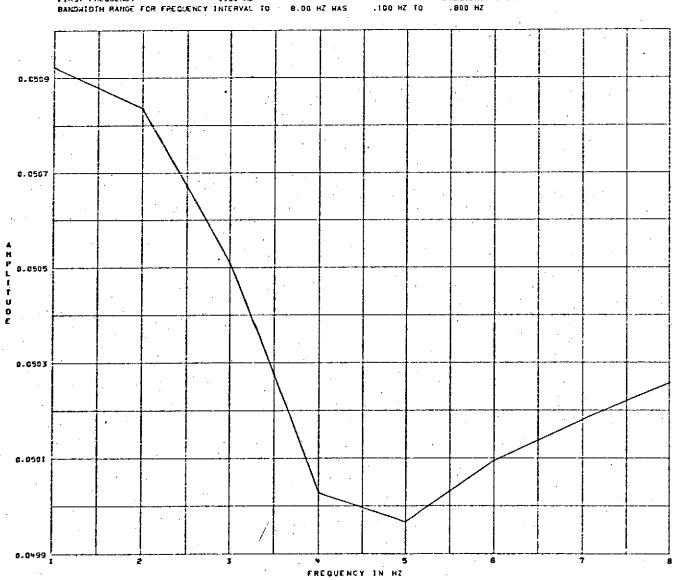


DATE PROCESSED - 09APR74

FREQUENCY RESPONSE FEST 1
REFERENCE SENSOR - TABCOM
TOTAL CYCLES PROCESSED - 0
FIRST FREQUENCY - 1.00 HZ

TOTAL PERIOD PROCESSED = FREQUENCY INCREMENTS =

40.77 SEC 1.00 HZ



DATE PROCESSED - 094PR74

FREQUENCY RESPONCE TEST 1

SENSOR -DELT X NORMALIZED BY REFERENCE SENSOR -TABCOM
TOTAL CYCLES PROCESSED - 0

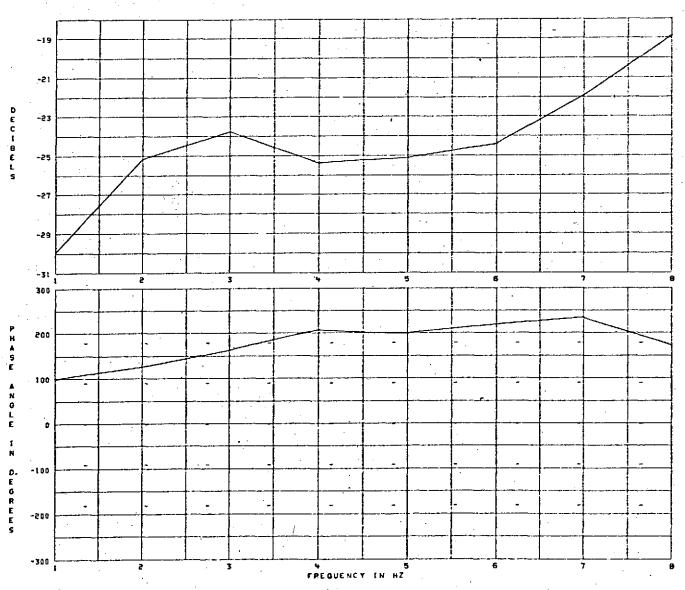
FIRST FREQUENCY * 1.00 MZ

BANDWIDTH RANGE FOR FREQUENCY INTERVAL TO 0.00 HZ MAS

TOTAL PERIOD PROCESSED = FREGUENCY INCREMENTS = 1800 HZ

.100 HZ TO

1.00 HZ



FREQUENCY RESPONCE TEST 1

SENSOR -DELT Y NORMALIZED BY REFERENCE SENSOR -TABCOM

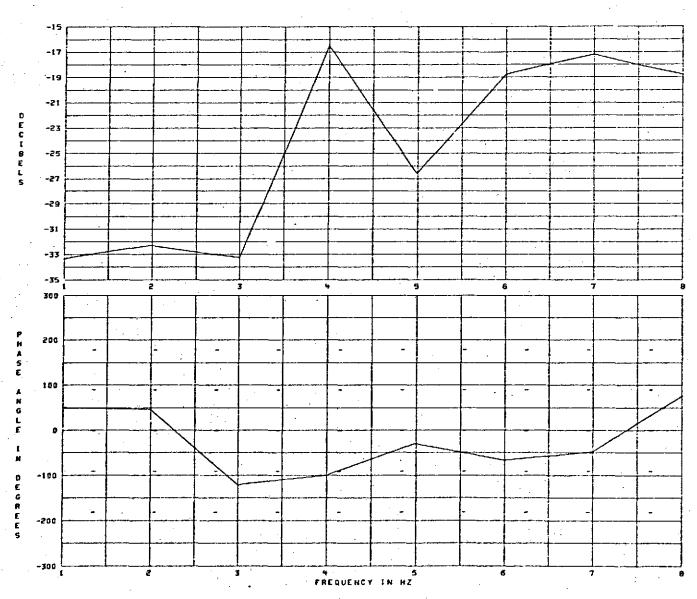
TOTAL CYCLES PROCESSED - 0

FIRST FREQUENCY - 1.00 HZ

BANDWIDTH RANGE FOR FREQUENCY INTERVAL TO 8.00 HZ HAS

DATE PROCESSED - 39APR74

TOTAL PERIOD PROCESSED - 40.77 SEC FREQUENCY INCREMENTS - 1.00 HZ .800 HZ



.100 HZ TO

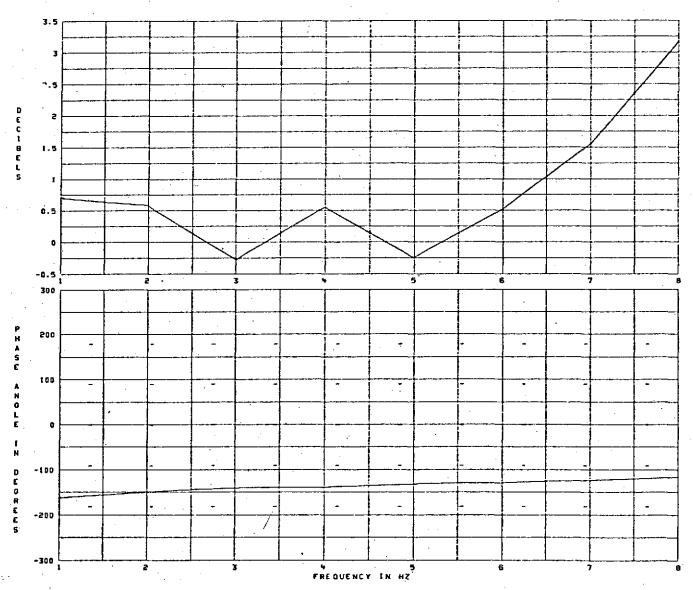
PAGE 2.

DATE PROCESSED - 09APR74

FREQUENCY RESPONCE TEST I
SENSOR -DELT Z NORMALIZED BY REFERENCE SENSOR -TABCOM
TOTAL CYCLES PROCESSED = 0
FIRST FREQUENCY = 1.00 HZ
BANDHIDTH RANGE FOR FREQUENCY INTERVAL TO 8.00 HZ HAS

TOTAL PERIOD PROCESSED = FREQUENCY INCREMENTS = .800 HZ .100 HZ TO

40.77 SEC 1.00 HZ



DATE PROCESSED - 09APR74

FREQUENCY RESPONCE TEST 1 FREGUENCY MESPOSSE 1551 1

SENSOR -XINETA NORMALIZED BY REFERENCE SENSOR -TABLOM

TOTAL CYCLES PROCESSED = 0

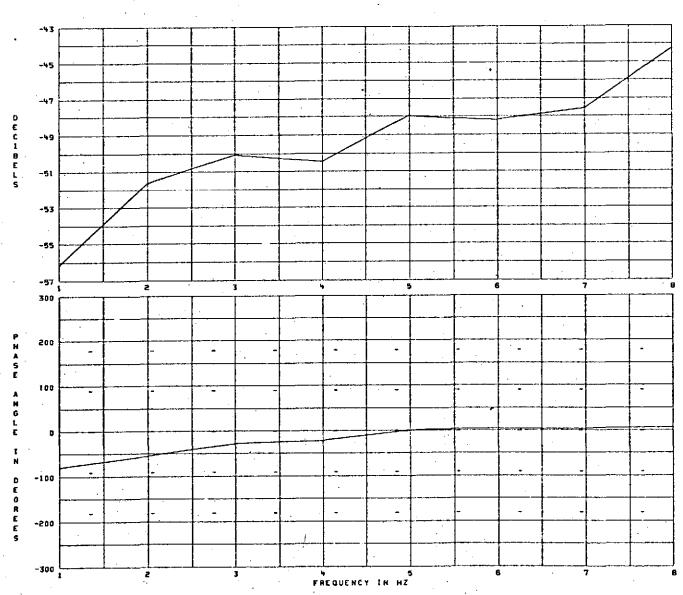
FIRST FREGUENCY = 1.00 HZ

BANDHIDTH RANGE FOR FREQUENCY INTERVAL TO 8.00 HZ HAS

TOTAL PERIOD PROCESSED = FREQUENCY INCREMENTS -.100 HZ TO

40.77 SEC 1.00 HZ

.800 HZ



FREQUENCY RESPONCE TEST : SENSOR -YTHETA NORMALIZED BY REFERENCE SENSOR -TABCOM TOTAL CYCLES PROCESSED *
FIRST FREQUENCY * 0 1.00 HZ

TOTAL PERIOD PROCESSED . FREQUENCY INCREMENTS -

BANDHIDTH RANGE FOR FREQUENCY INTERVAL TO B.DO HZ HAS -.100 HZ 10 .800 HZ

-49 51 -53 -55 -57 -59 -61 -63 300 200 100 -100 -500 -300 FREQUENCY IN HZ

PAGE 5.

DATE PROCESSED - 094PR74

40.77 SEC

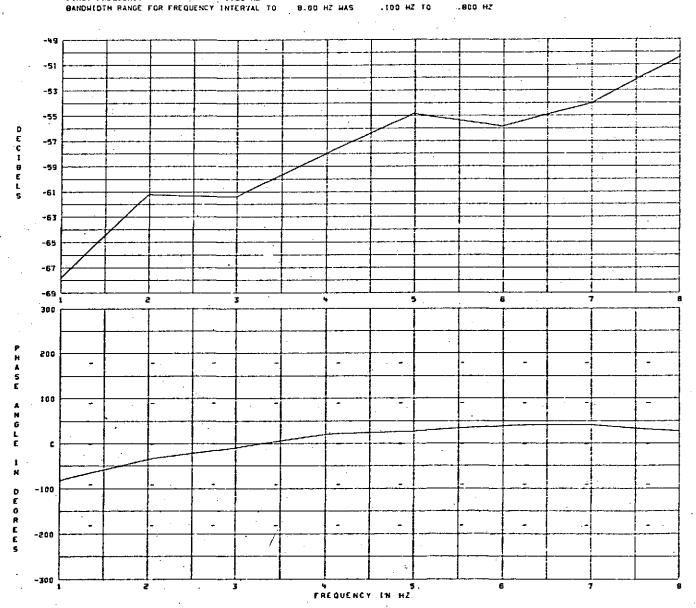
1.00 HZ

FREQUENCY RESPONCE TEST I SENSOR -ZTHETA NORMALIZED BY REFERENCE SENSOR -TABCOM
TOTAL CYCLES PROCESSED = 0
FIRST PREQUENCY = 1.00 HZ
BANDHIDTH RANGE FOR FREQUENCY INTERVAL TO 8.00 HZ HAS

DATE PROCESSED - 09APR74

TOTAL PERIOD PROCESSED -FREQUENCY INCPEMENTS -.800 HZ

40.77 SEC 1.00 HZ



APPENDIX B

TEST NO. 2 Z-AXIS

DOTS FREQUENCY RESPONSE TEST SUMMARY OF INPUT INERTIAL CONDITIONS AND TRANSFORM MATRIX

FREQUENCY RESPONCE TEST 2

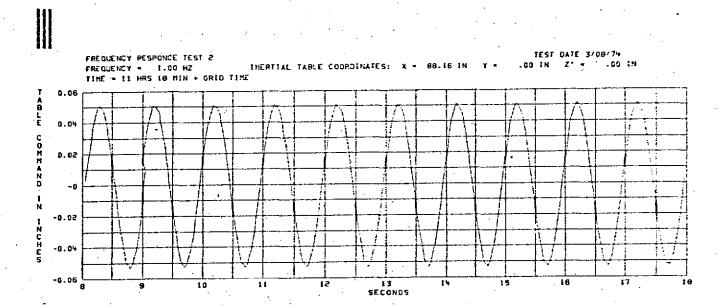
TEST DATE 3/08/74

	•		TABLE	COORDINATES	88. Í 59	.000		.000			
-	SERVO TA	BLE SHIVE	JOINTS	FLOOR	SWIVEL J	OINTS		COMPONENT	S OF ACTUA	TOP LENGTH	ACTUATOR
ACTUATOR	x	Y	2	×	Y	Z	•		Y	z	LENGTH
1	.0000	25.1020	49.5000	210.4070	-64.3110	123.1780		-122.2480	89.4130	-73.6789	168.4272
2	.0000	-55.41,90	3.0000	210.4290	-76.3900	116.1240		-122.2700	20.9510	-113.1290	167.8879
. 3	.0000	~55.4190	-3.0000	210.4220	-74.5730	-116.0193		-122.2630	19.1540	113.0:95	168,1365
. 4	.0000	25.1020	-49.5000	210.4170	-62.4120	-123.6030		-122.2580	87.5140	74.1830	167.6569
5	.0000	30.2980	-46.5000	210.4160	138.4630	-5.9750		-122.2510	-150.1650	-40.5250	160.1881
6	.0000	30.2980	46.5000	21C.3690	138.3890	8.0050		-122.2100	-100.0910	38.4950	167.6330

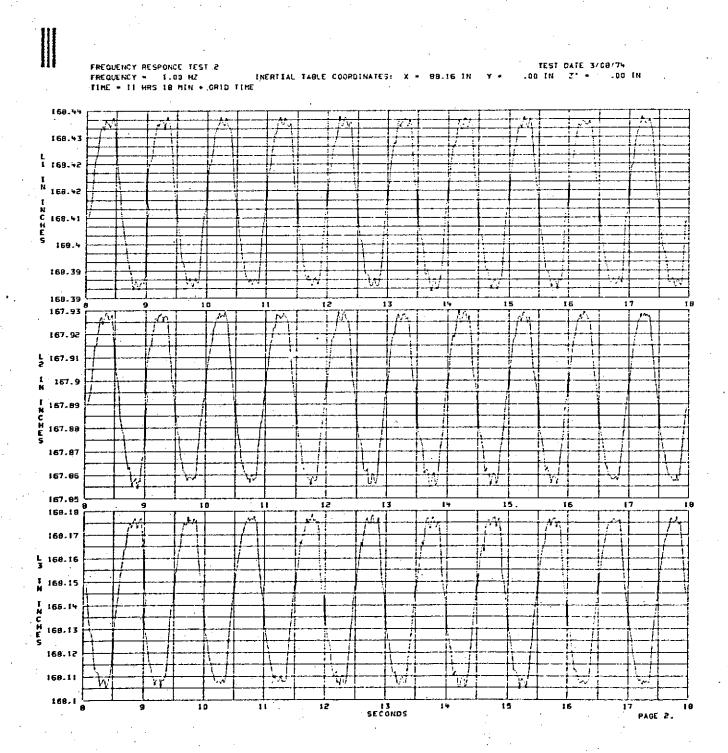
TRANSFORM HATRIX

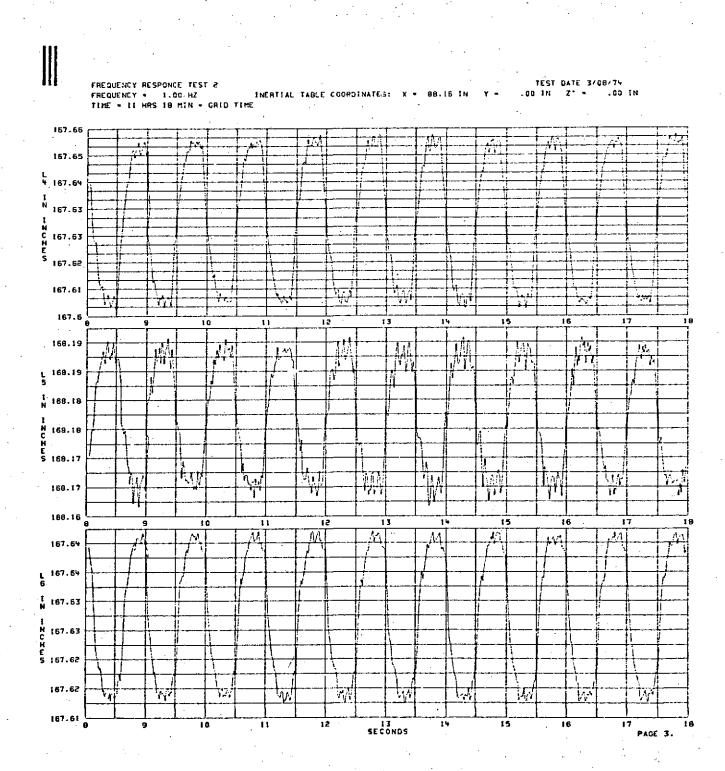
~.227798+00	229422+00	228575+00	229554+00	228265-08	230510+00
.447118+00	236022-01	303266-01	.442709+00	416853+00	418525+00
222802+00	498159+80	.498501+00	.228740+00	275033+00	.260651+00
450573-02	449077-02	449777-02	448626-02	450071-G2	.448595-32
648215-02	.145547-02	146094-02	.650505-02	.794358-02	796996-0≥
.543719-02	835964-02	833211-02	_5449B0-02	269540-02	.291976-02

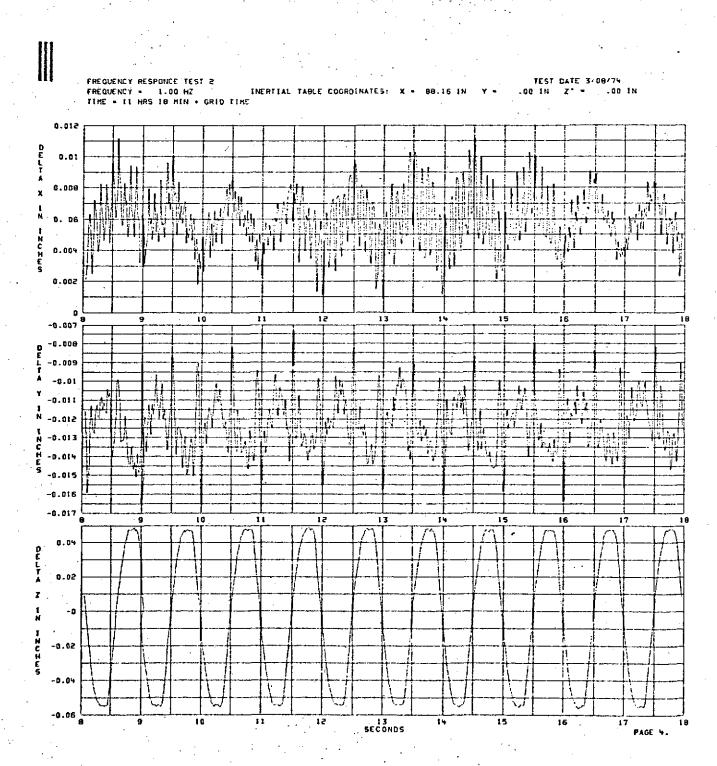
REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

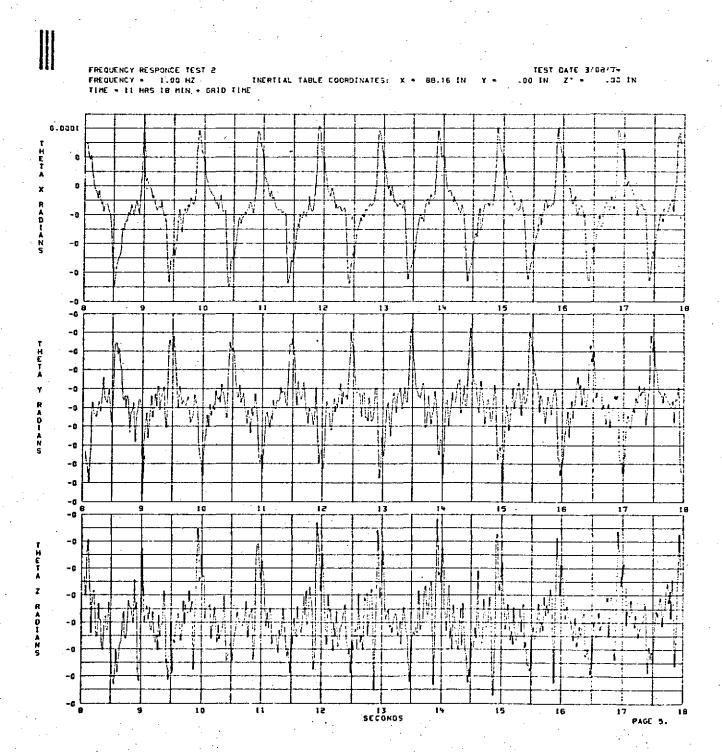


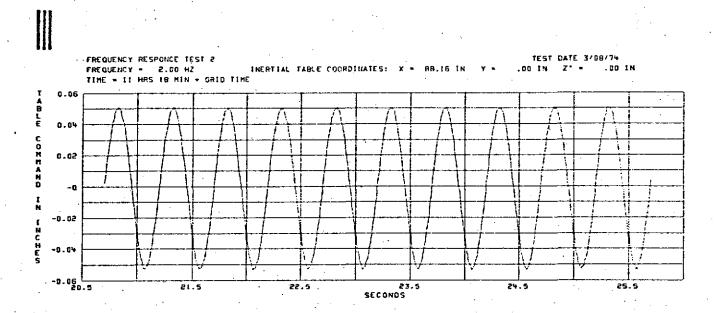
PAGE 1.



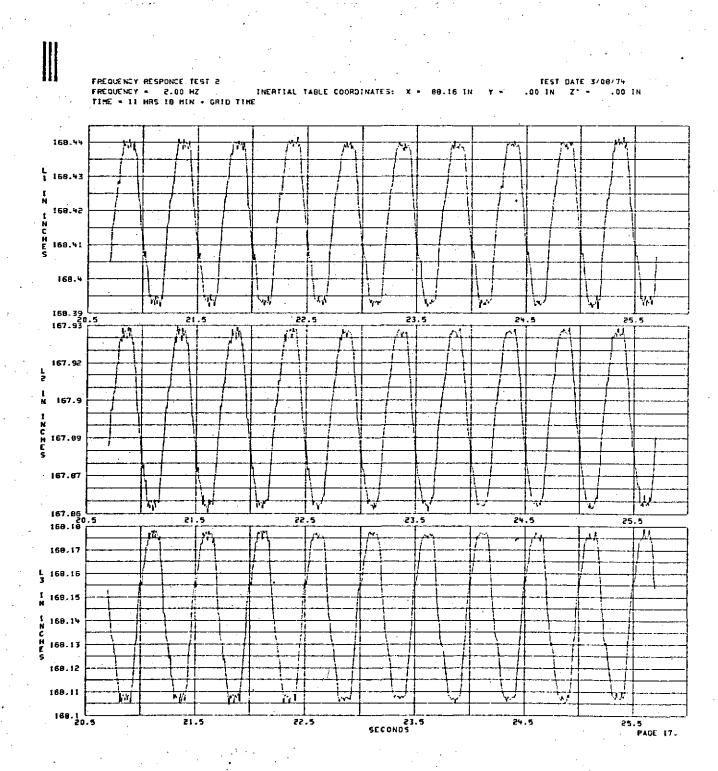


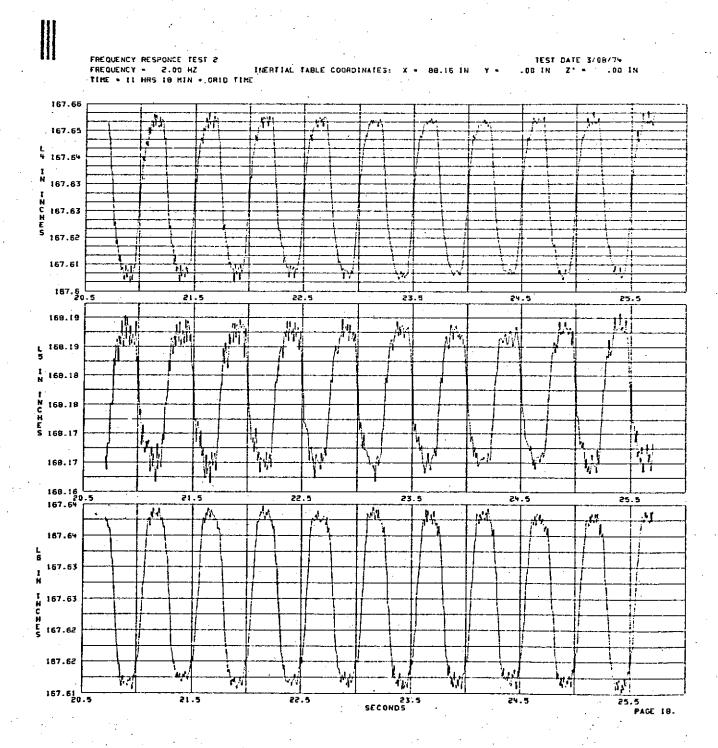


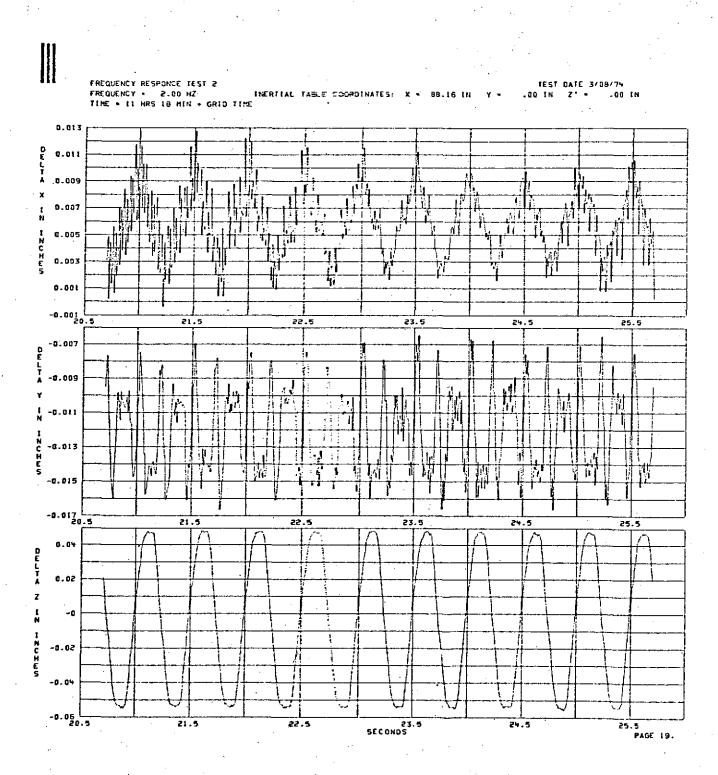


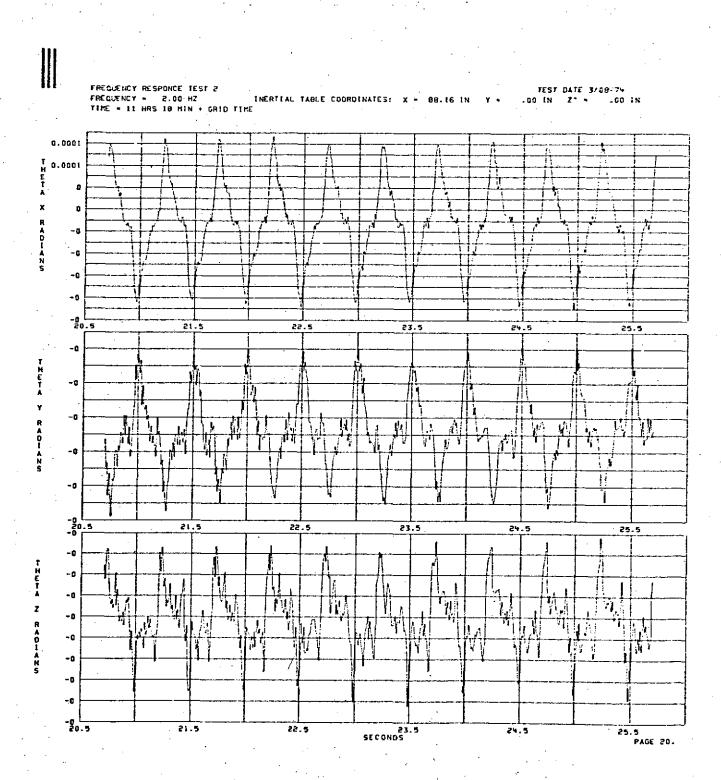


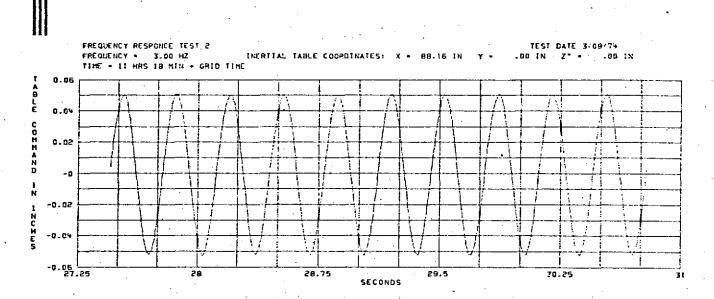
PAGE 16.

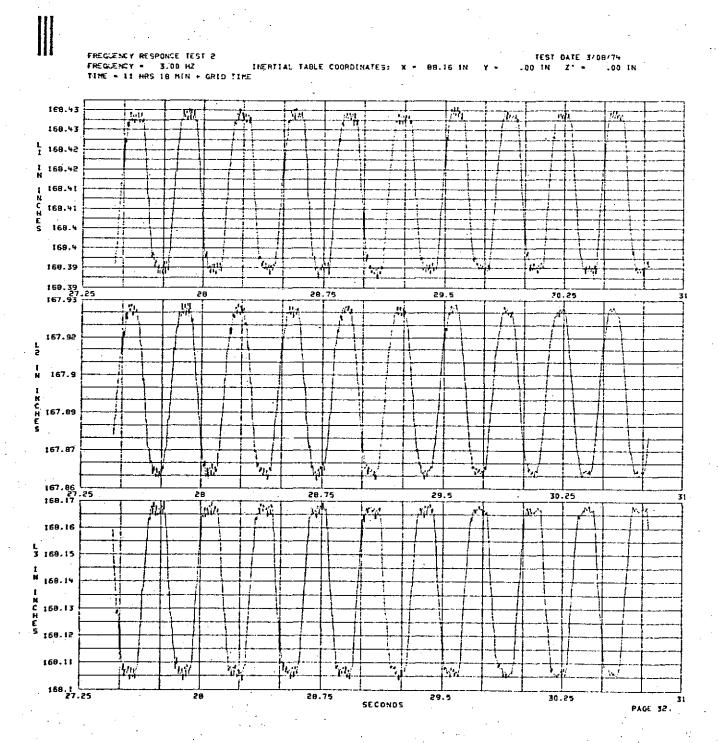


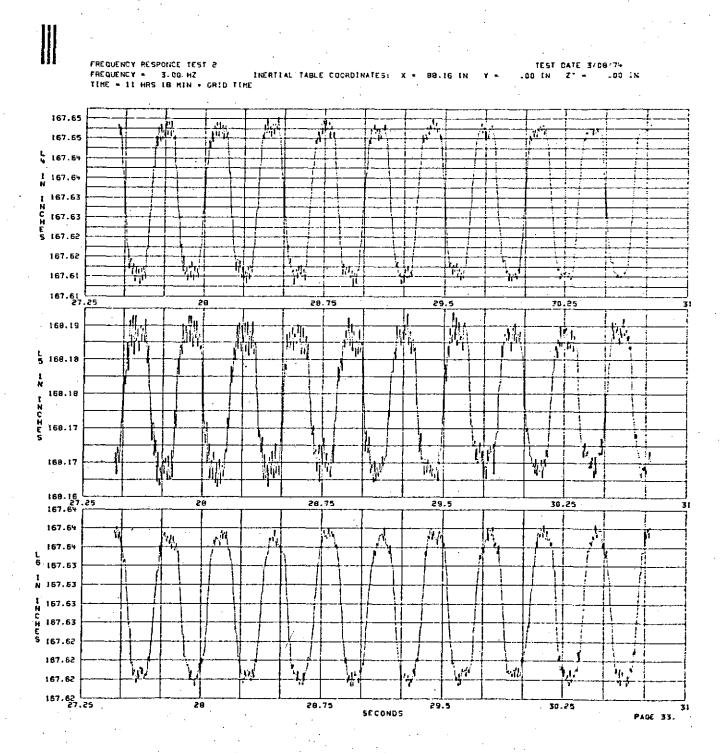


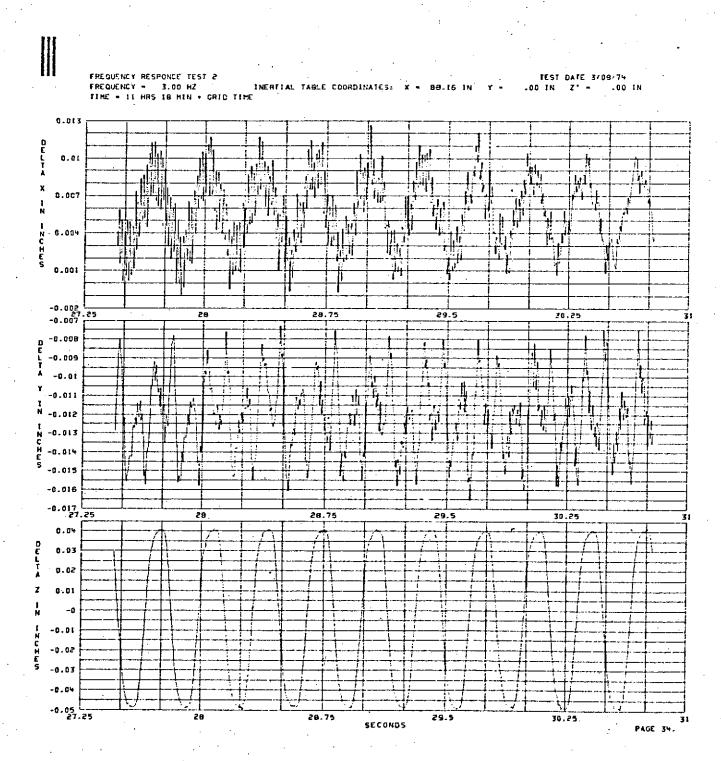


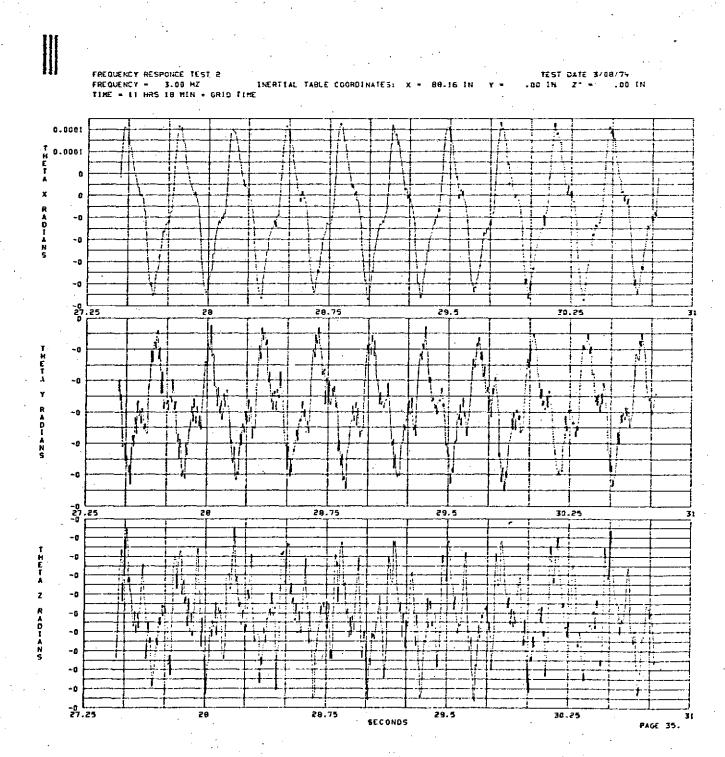


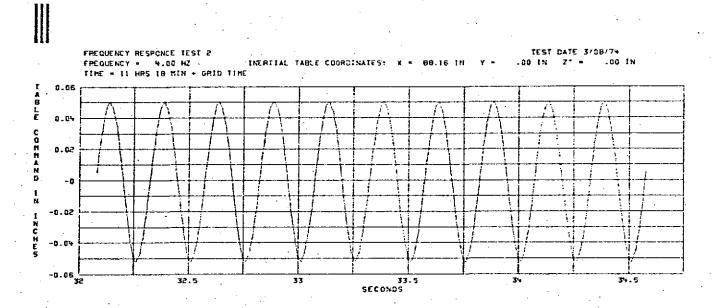




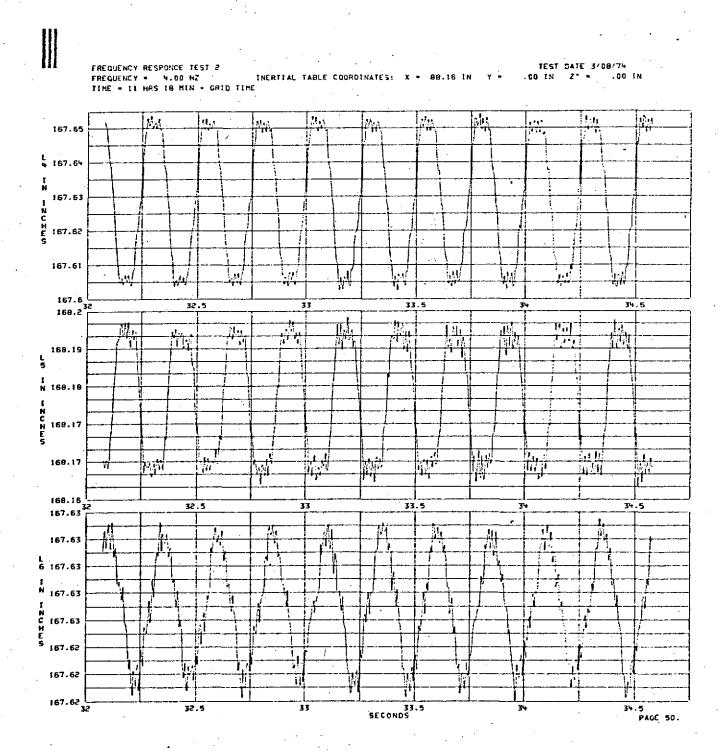


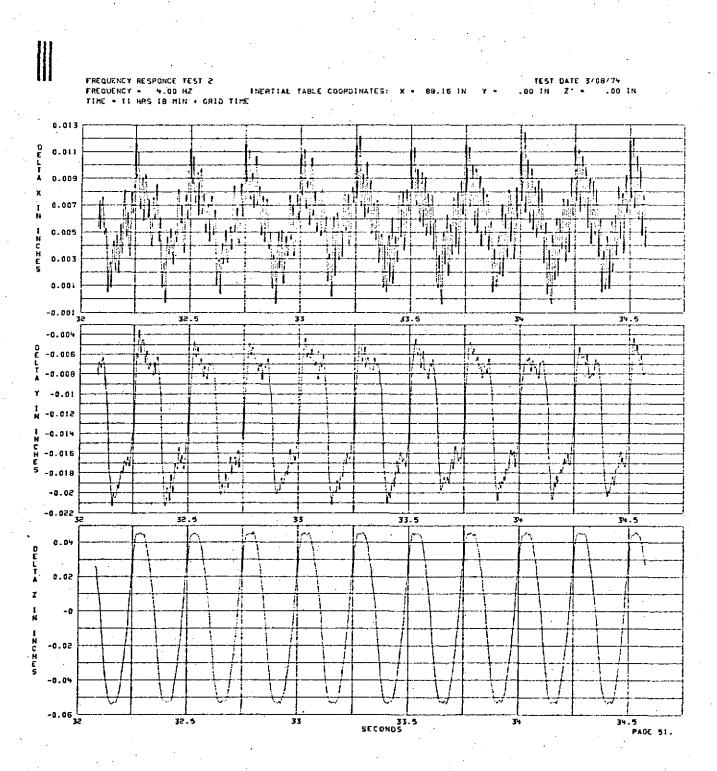


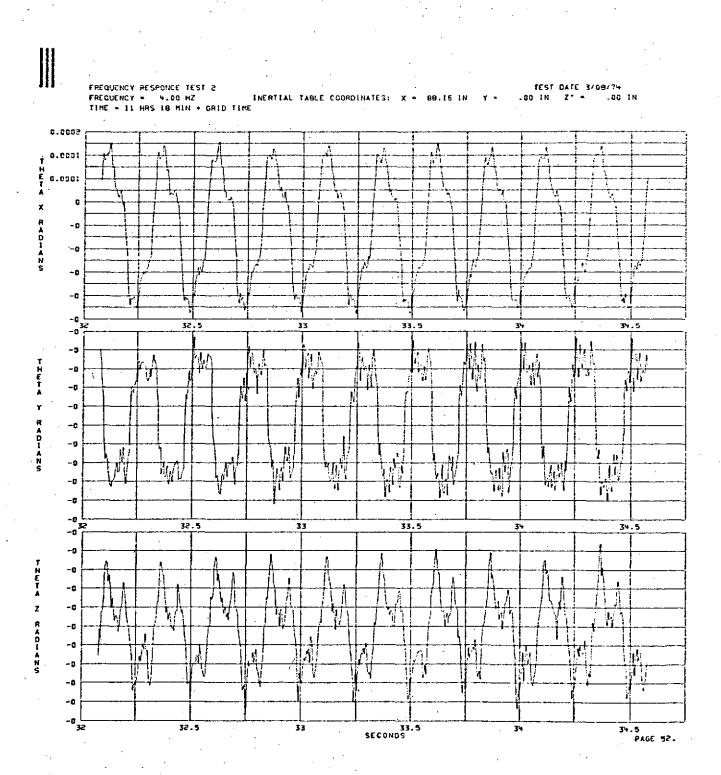


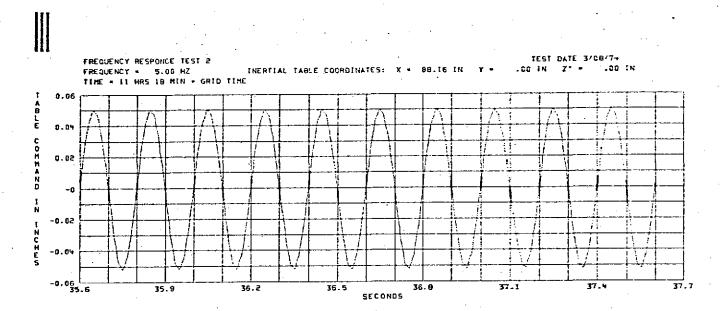


FREQUENCY RESPONCE TEST 2 FREQUENCY - %.00 HZ TIME * II HRS 18 MIN + GRID TIME INERTIAL TABLE COORDINATES: 168.43 168.42 168.42 168.41 N C 168.41 169.4 168.4 168.39 168.39 167.93 167.92 L 2 167.91 1 N 157.9 1 N 167.89 C H E 167.89 167.87 167.86 167.85 L 160.10 168.17 £ 3 (68.16 I N 169.15 I N 150.14 C H £ 168.13 169.12 168.11 168.1 SECONDS 33.5 34.5 PAGE 49.

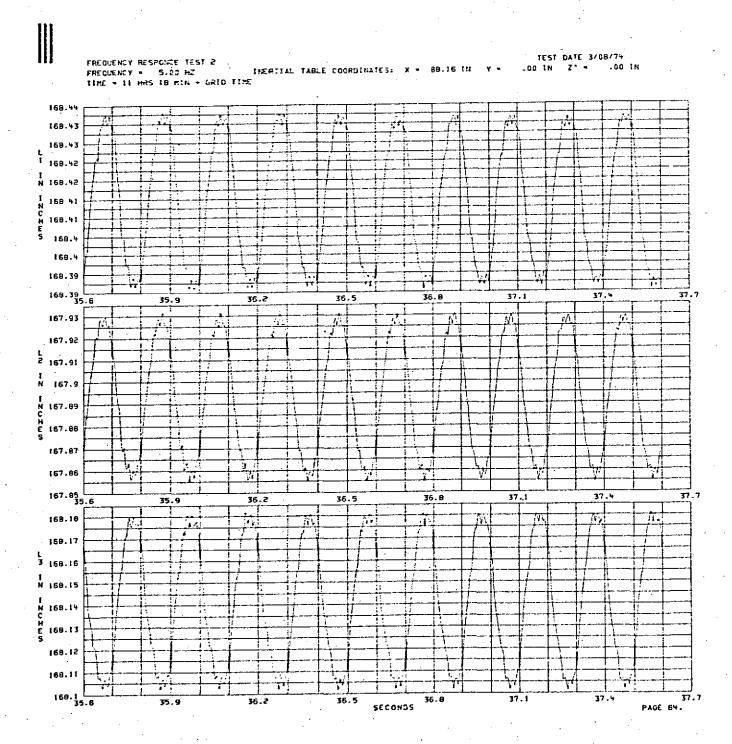


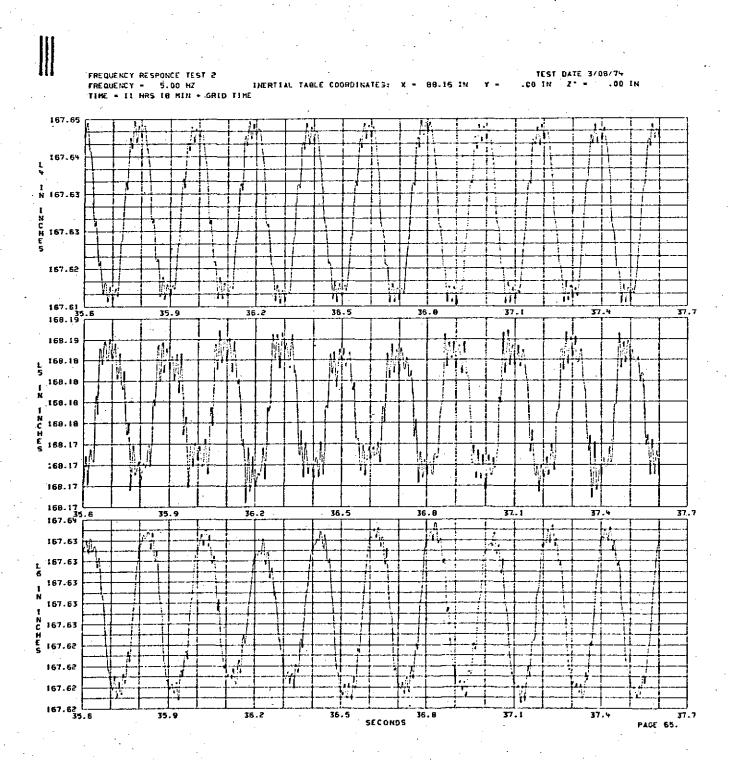


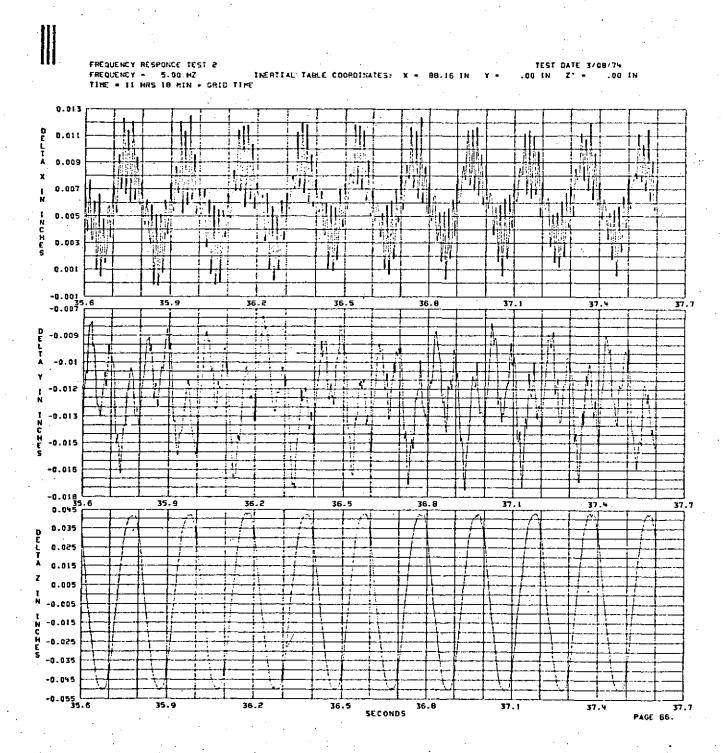


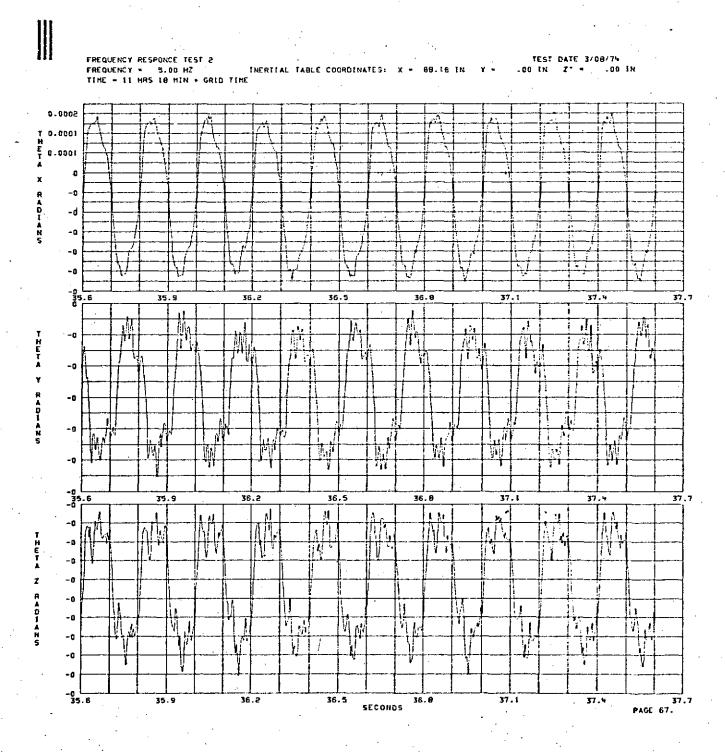


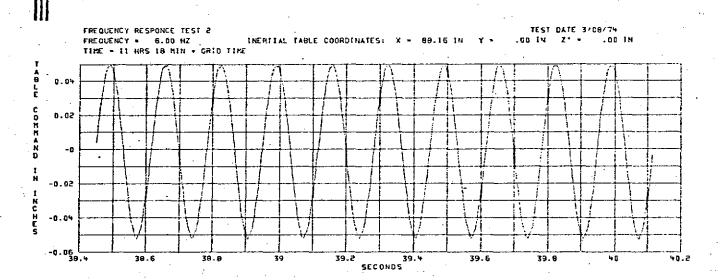
PAGE 63



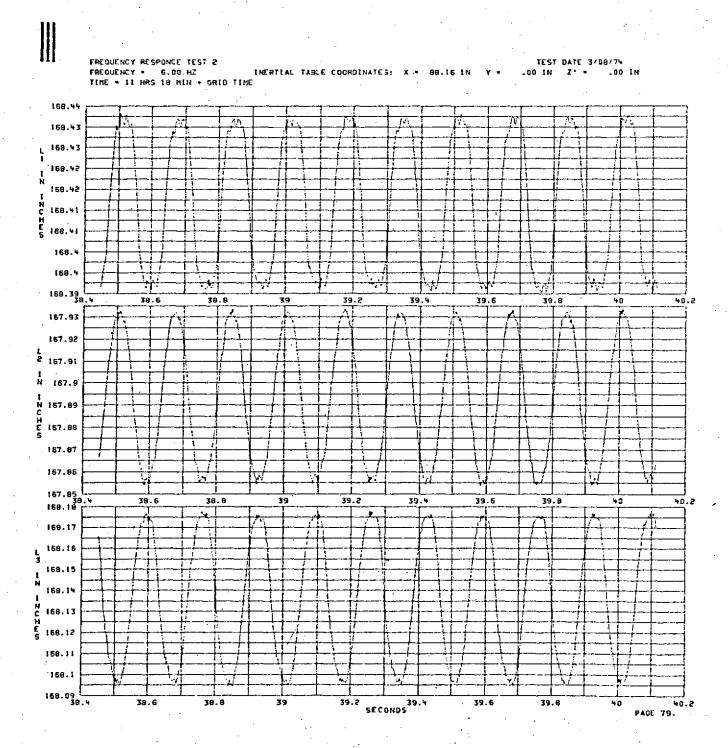








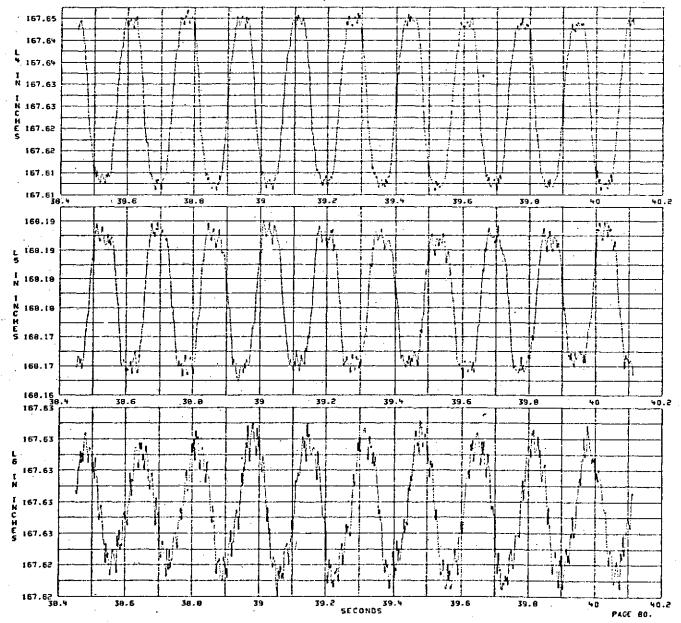
PAGE 78

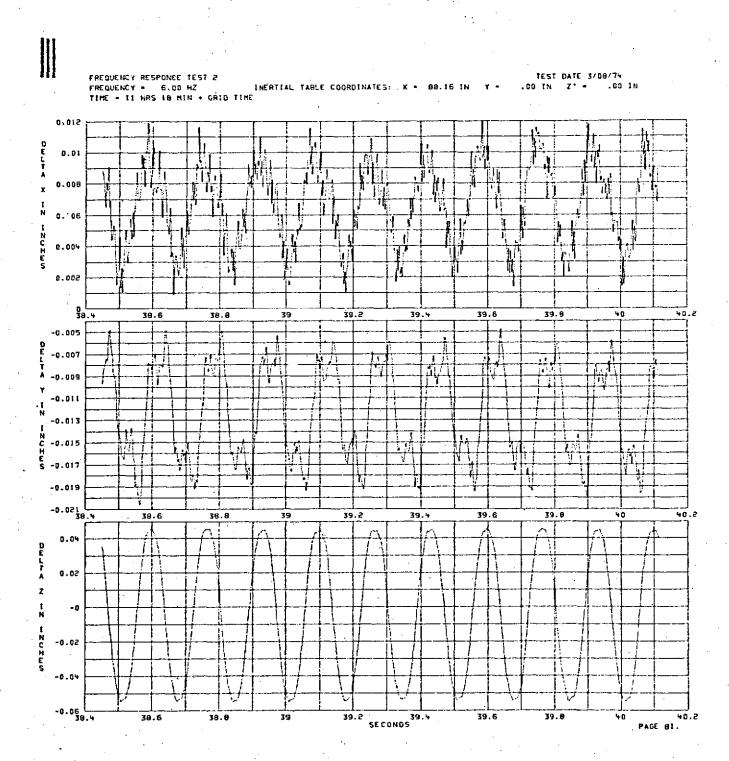


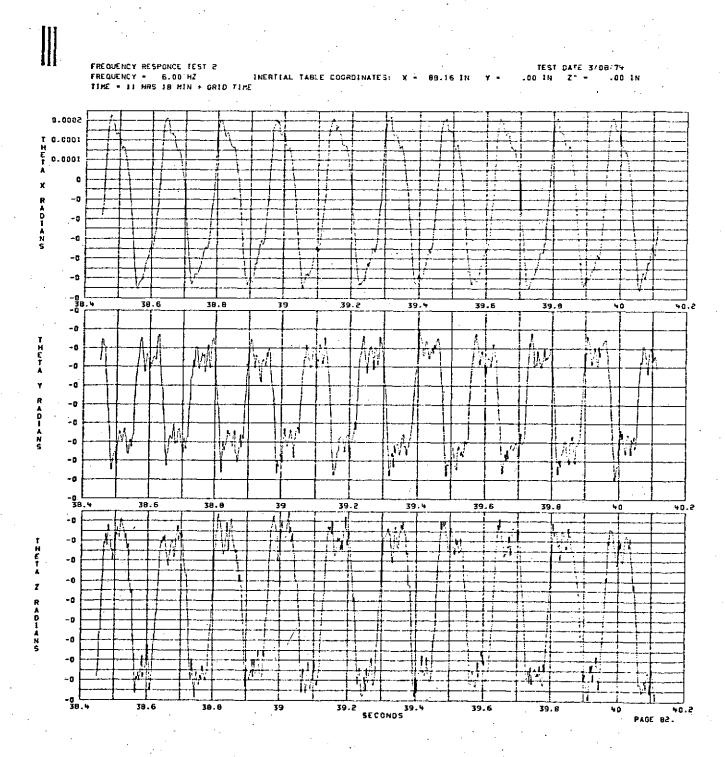
FREQUENCY RESPONCE TEST 2
FREQUENCY - 6.00 NZ
TIME - 11 HRS 18 NIN - GR

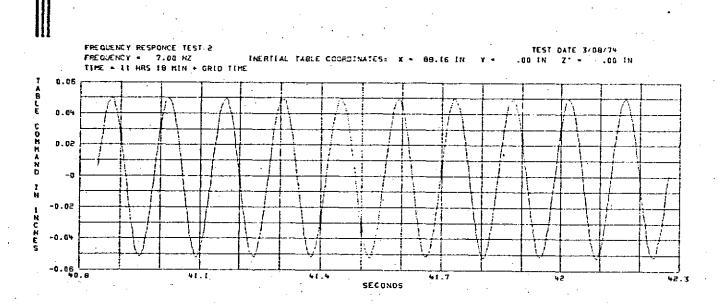
FREQUENCY RESPONCE TEST 2

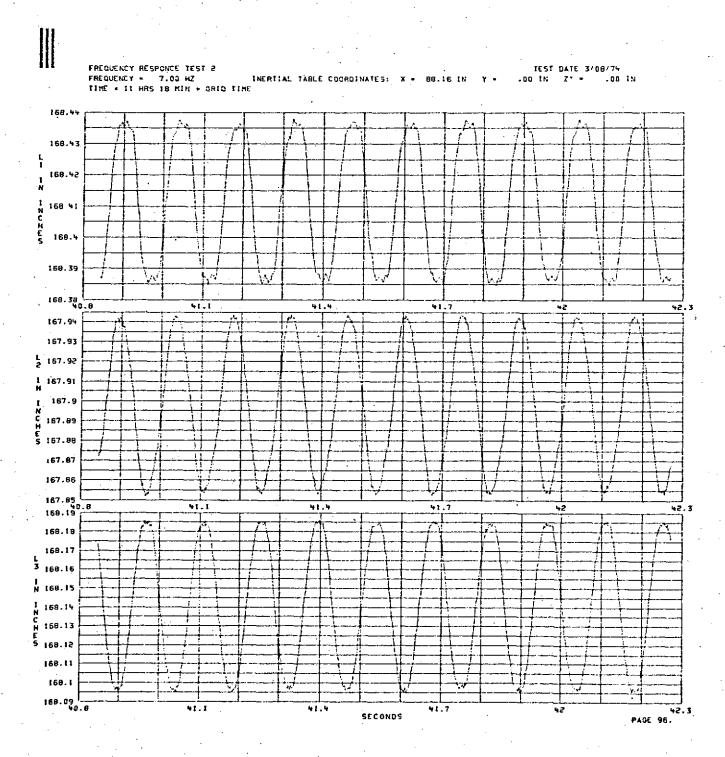
FREQUENCY = 6.00 HZ INERTIAL TABLE COORDINATES: X = 88.15 IN Y = .00 IN Z = .00 IN TIME = 11 HRS 18 MIN + GRID TIME

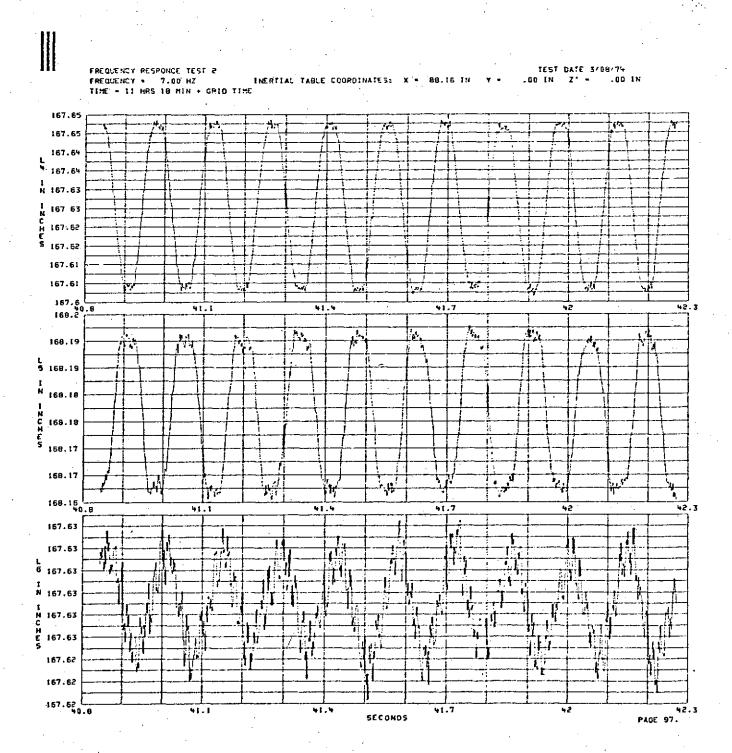


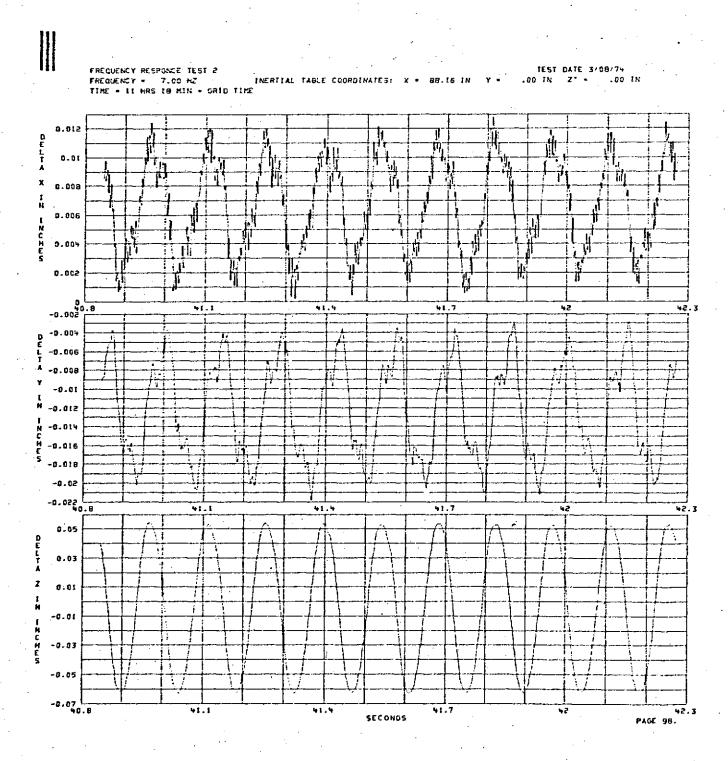


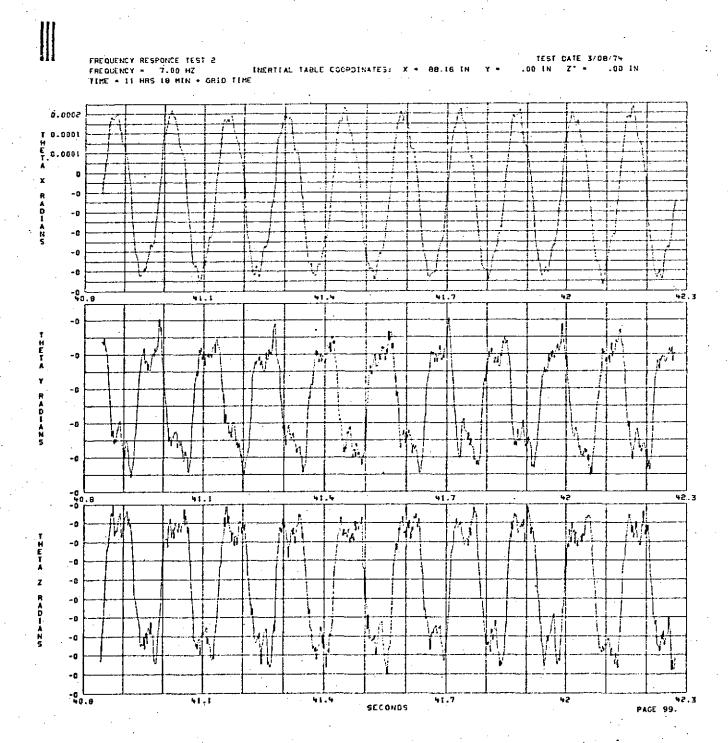


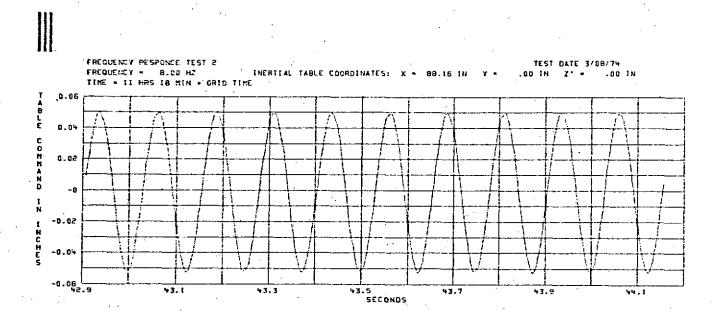


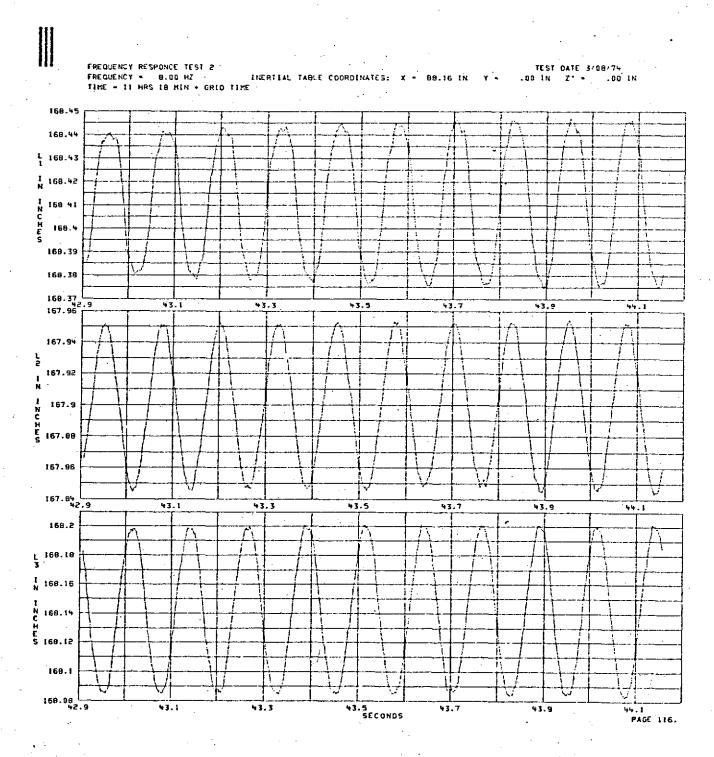


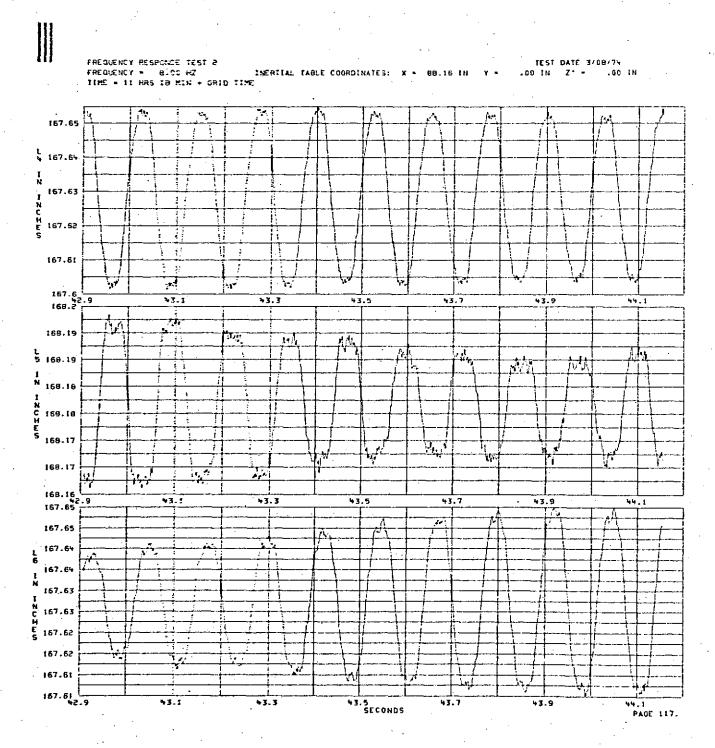


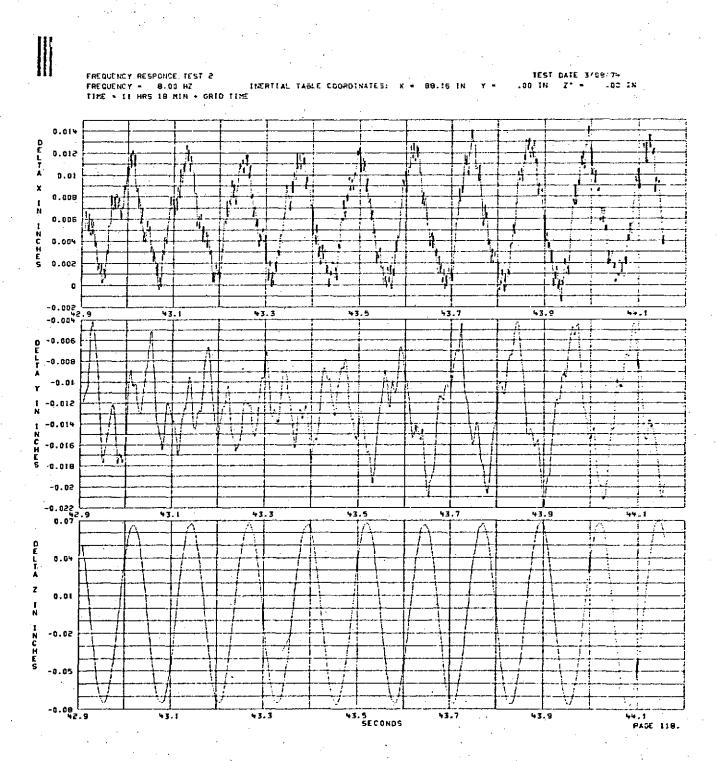


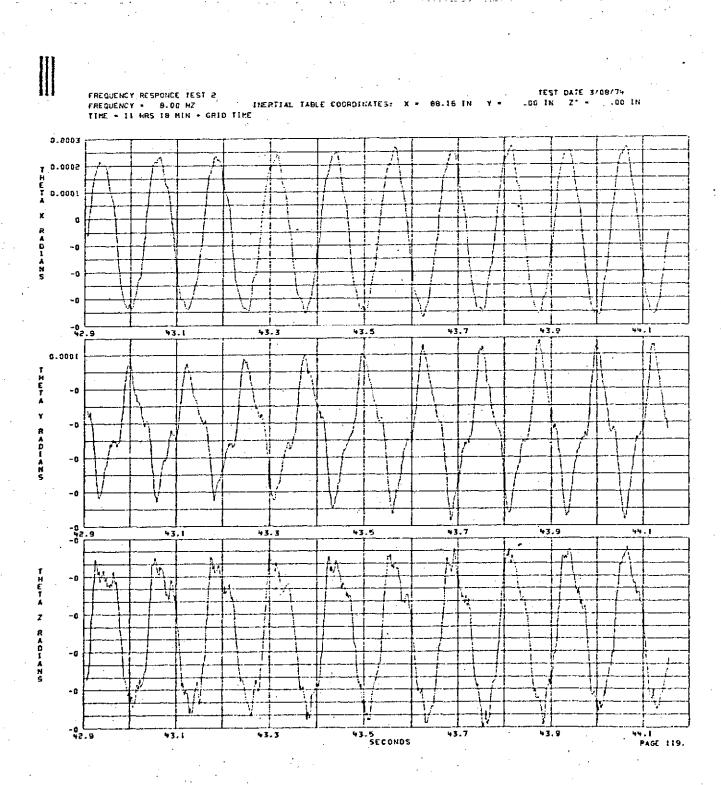










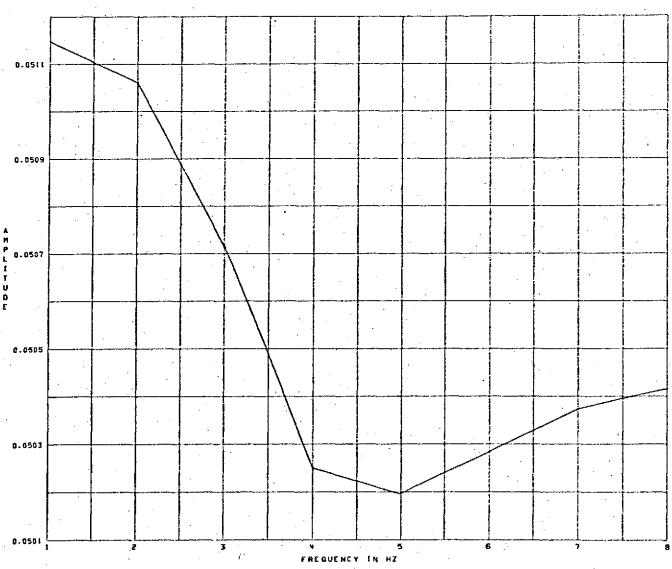


DATE PROCESSED - 09APR74

FREQUENCY RESPONCE TEST 2
REFERENCE SENSOR - TABCOM
TOTAL CYCLES PROCESSED = 0
FIRST FREQUENCY - 1.00 HZ
BANDHIDTH RANGE FOR FREQUENCY INTERVAL TO

 TOTAL PERIOD PROCESSED + FREQUENCY INCREMENTS + 40.76 SEC 1.00 HZ

.800 HZ



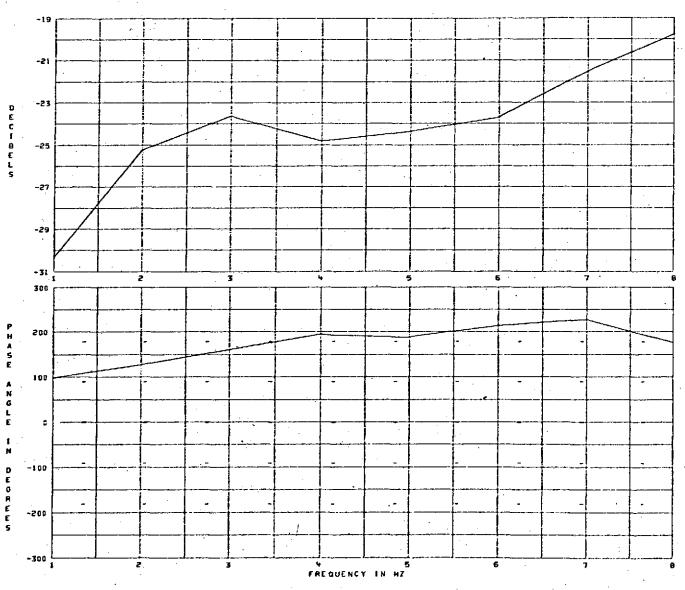
PAGE D.

FREQUENCY RESPONCE TEST 2

SENSOR -DELT X NORMALIZED BY REFERENCE SENSOR -TABCON
TOTAL CYCLES PROCESSED - 0
FIRST FREQUENCY - 1.00 MZ
BANDARIDTH RANGE FOR FREQUENCY INTERVAL TO 8.00 MZ MAS

DATE PROCESSED - 09APR74

TOTAL PERIOD PROCESSED - 40.76 SEC FREQUENCY INCREMENTS - 1.00 HZ



PAGE 1.

FREQUENCY RESPONCE TEST 8

SENSOR -DELT Y NORMALIZED BY REFERENCE SENSOR -TABCOM

TOTAL CYCLES PROCESSED - 0

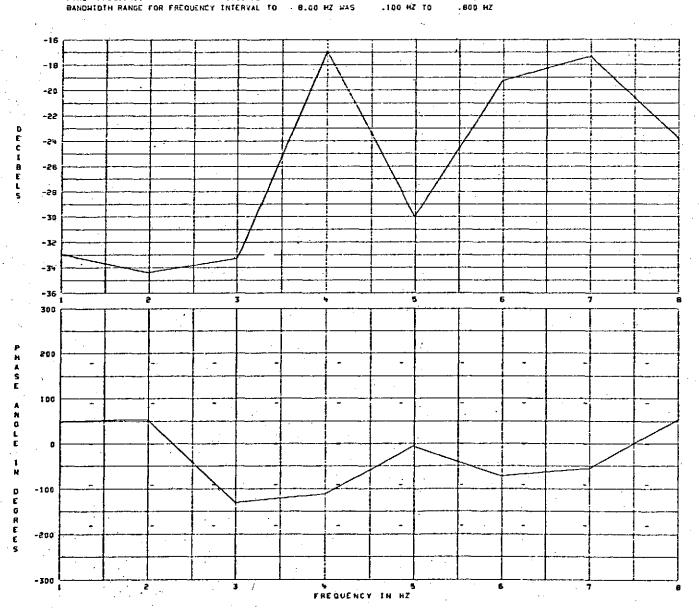
FIRST FREQUENCY 1.00 HZ

BANDHIDTH RANGE FOR FREQUENCY INTERVAL TO 8.00 MZ #AS

DATE PROCESSED - 09APR74

FREQUENCY INCREMENTS =

40.76 SEC 1.00 HZ



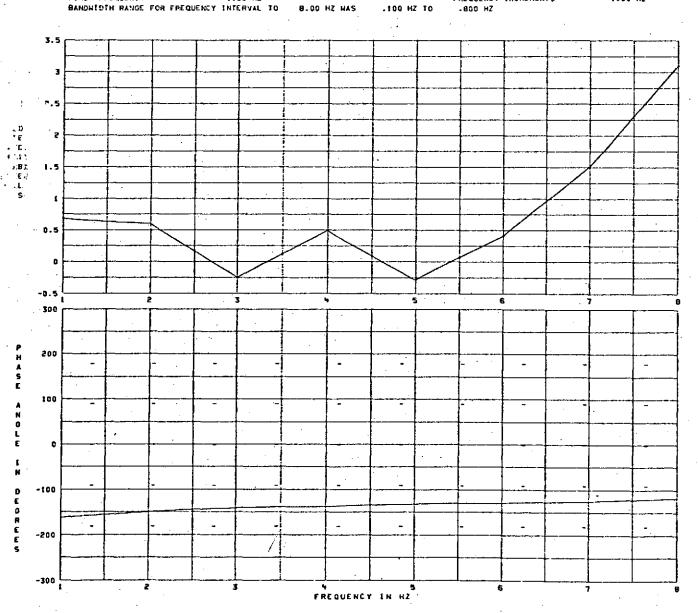
PAGE 2.

FREQUENCY RESPONCE TEST 2
SENSOR -DELT Z NORMALIZED BY REFERENCE SENSOR -TARCOM
TOTAL CYCLES PROCESSED * 0
FIRST FREQUENCY * 1.00 HZ
BAHDHIDTH RANGE FOR FREQUENCY INTERVAL TO 8.00 HZ HAS

DATE PROCESSED - 09APR74

TOTAL PERIOD PROCESSED = FREQUENCY INCREMENTS = .800 HZ

40.76 SEC 1.00 HZ

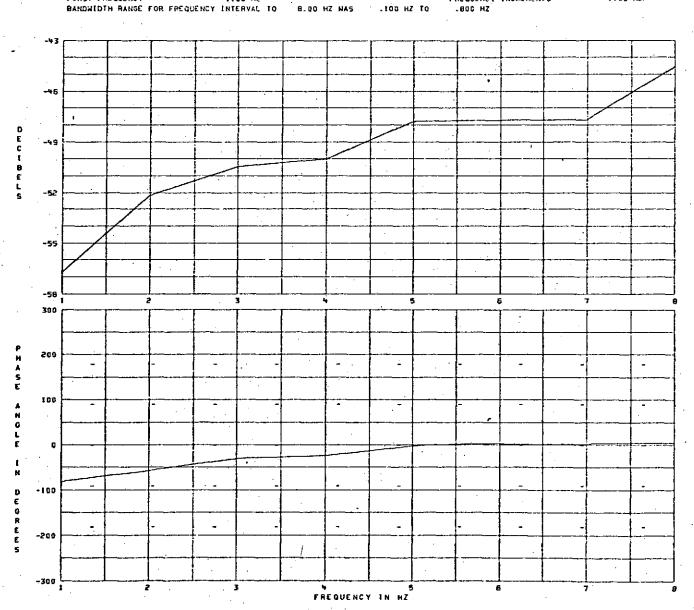


PAGE 3.

FREQUENCY RESPONCE TEST 2
SENSOR -XTHETA NORMALIZED BY REFERENCE SENSOR -TABCOM
TOTAL CYCLES PROCESSED = 0
FIRST FREQUENCY = 1.00 HZ
BANDAIDTH RANGE FOR FREQUENCY INTERVAL TO 8.00 HZ HAS

DATE PROCESSED - 09APR74

TOTAL PERIOD PROCESSED - 40.76 SEC FREQUENCY INCREMENTS - 1.00 HZ.



PAGE 4.

FREQUENCY RESPONCE TEST 2

SENSOR -YTHETA NORMALIZED BY REFERENCE SENSOR -FABCOM
TOTAL CYCLES PROCESSED - 0

FIRST FREQUENCY - 1.00 HZ

BANDWIDTH RANSE FOR FREQUENCY INTERVAL TO 8.00 HZ WAS

DATE PROCESSED - 09APR74

TOTAL PERIOD PROCESSED • 40.76 SEC FREQUENCY INCPEMENTS • 1.00 HZ .800 HZ

-51 -54 -57 -60 -63 300 200 100 0 -100 -200 FREQUENCY IN HZ

.100 HZ TO

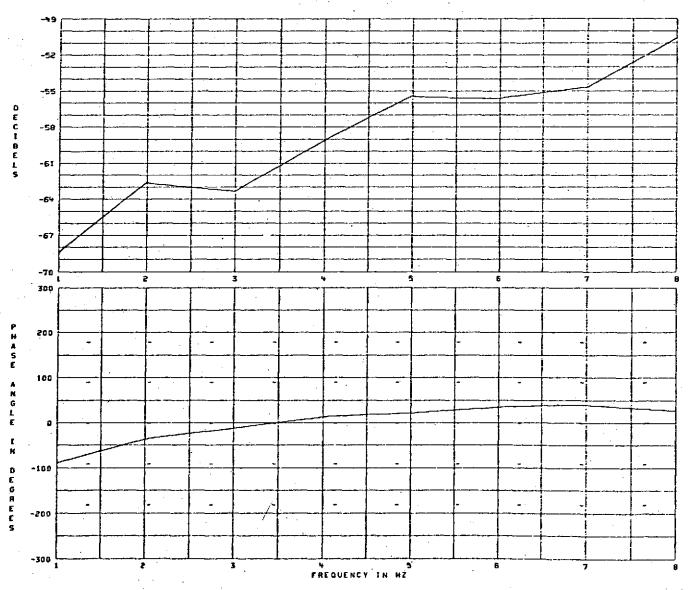
PAGE 5.

FREQUENCY RESPONCE TEST 2
SENSOR -ZTHETA NORMALIZED BY REFERENCE SENSOR -TABCOM
TOTAL CYCLES PROCESSED = 0
FIRST FREQUENCY = 1.00 MZ
BANDHIDTH RANGE FOR FREQUENCY INTERVAL TO 8.00 HZ WAS

DATE PROCESSED - 09APR74

TOTAL PERIOD PROCESSED = FREQUENCY INCREMENTS = 40.76 SEC 1.00 HZ

.800 HZ



PAGE 6.

APPENDIX C

TEST NO. 3 Y-AXIS

DOTS FREQUENCY RESPONSE TEST SUMMARY OF INPUT INERTIAL CONDITIONS AND TRANSFORM MATRIX

FREQUENCY RESPONCE TEST 3,

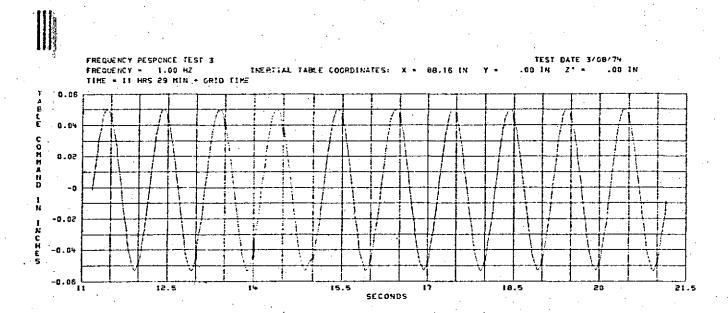
1EST DATE 3/08/74

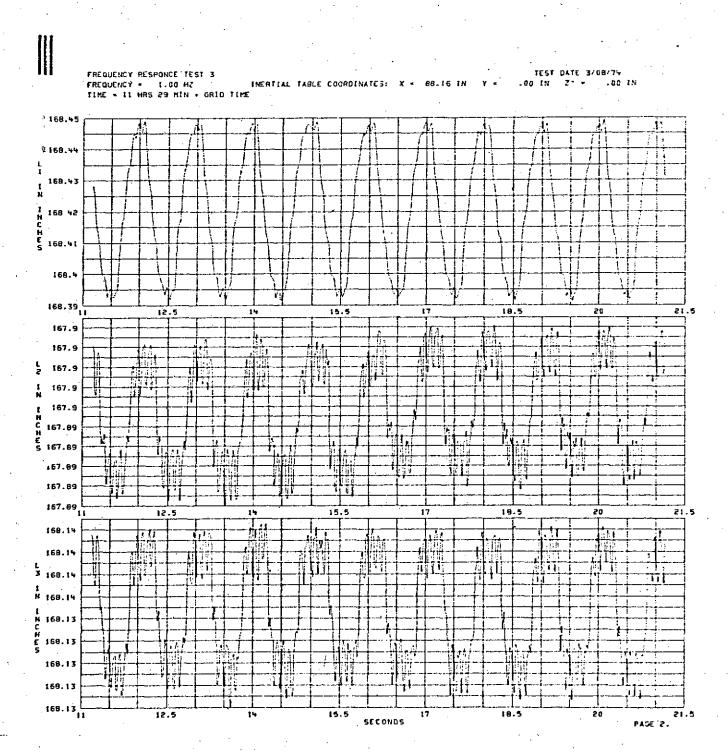
			TABLE	COORDINATES	80.159	.000	-000			
•	SERVO TABLE SHIVEL JOINTS		FLOOR SWIYEL .		011115	COMPONENTS OF ACTUATOR LENGTH		ACTUATOR		
ACTUATOR	×	. Y	Z	×	Y	Z.	×	Y	Z	LENGTH
	0000	25.1020	49.5000	219.4070	-64.3110	123.1790	-122.2480	89.4130	-73.6780	160.4272
2	.0000	-55.4190	3.0000	2:0.4290	-76.3800	116.1240	-:22.2700	20.9510	-113.1240	167.6879
3	.0000	-55.4190	-3-0600	210,4220	-74.5730	-116.0190	-122.2630	19.1540	113.8196	169.1355
4	.0000	25. t 020	-49.5000	210.4170.	-62.4120	-123.6830	-122.2590	87.5140	74.1830	167.6569
5	.0000	30.2980	-45.5000	210,4100	139.4630	-5.9750	-122.2510	-108.1650	-90.5250	168.1981
6.	.0008	30.2900	46.5000	210.3690	138.3890	8.0050	-122.2190	-108.0910	38.4950	167.6330

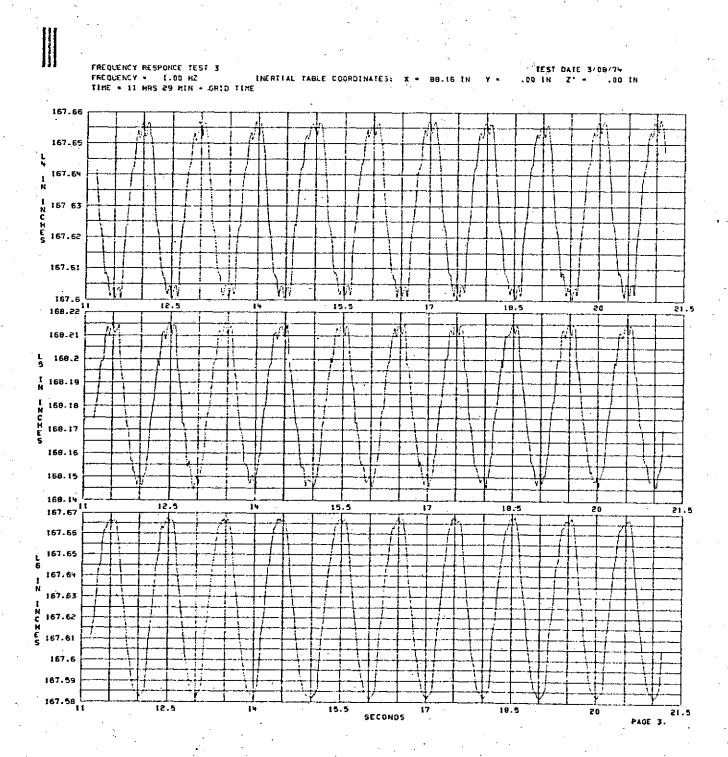
TRANSFORM MATRIX

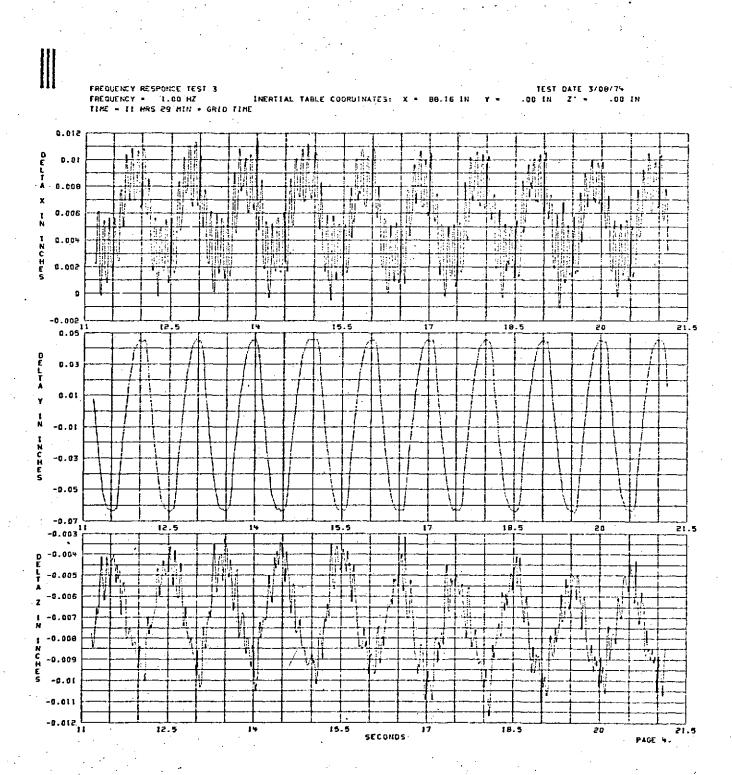
•					
227798+00	229422+60	228575+00	229554+00	228266+00	230510+00
.447118+00	10-550885	303266-01	.442709+00	416853+00	418525+00
222802+00	493159+00	.498501+00	.228740+00	276033+00	.269561.00
450573-02	.449077-02	- 449777-02	.448626-02	450071-02	,448595-02
648215402	-145547-02	146094-02	.650505-02	.794358-02	795999-02
.5%3719-02	835984-02	833211-02	.544980-02	.288540-02	.291975-02

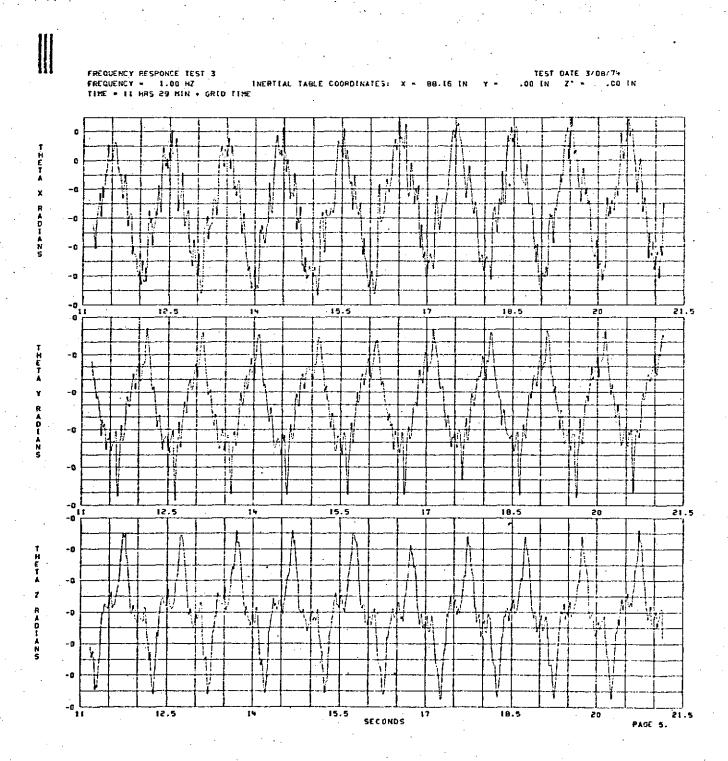
REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

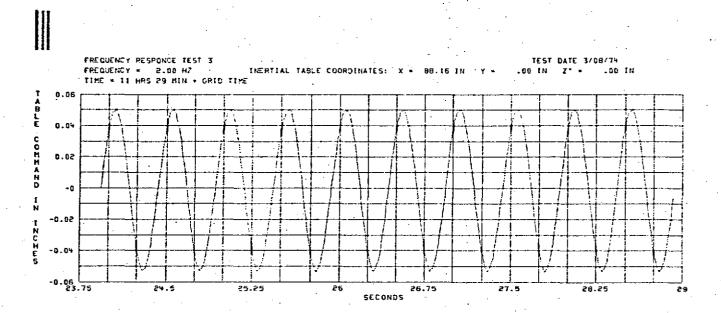




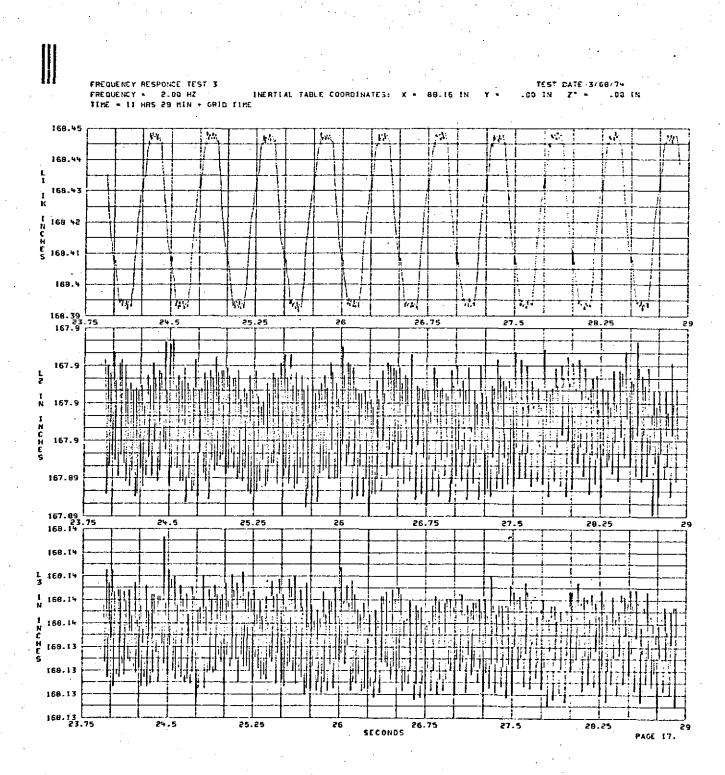


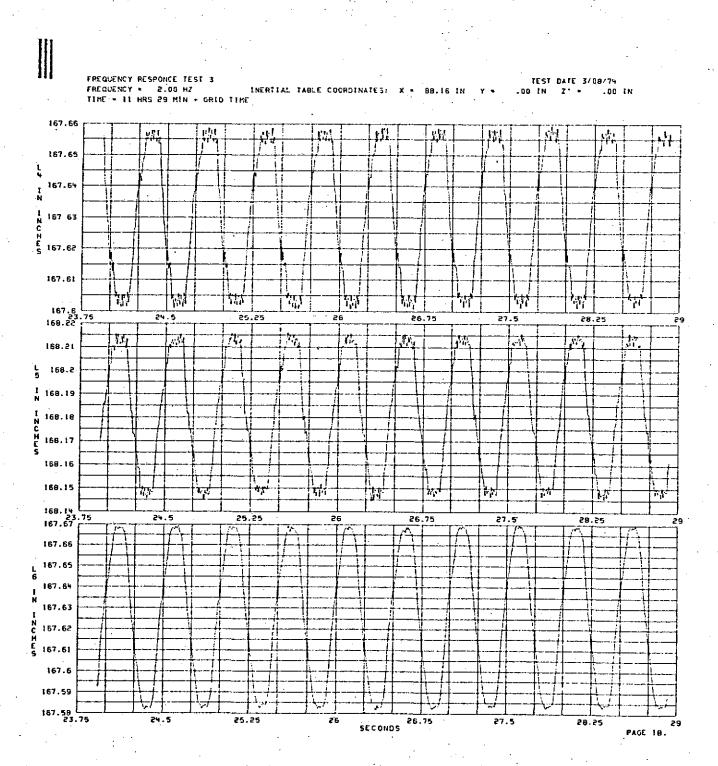


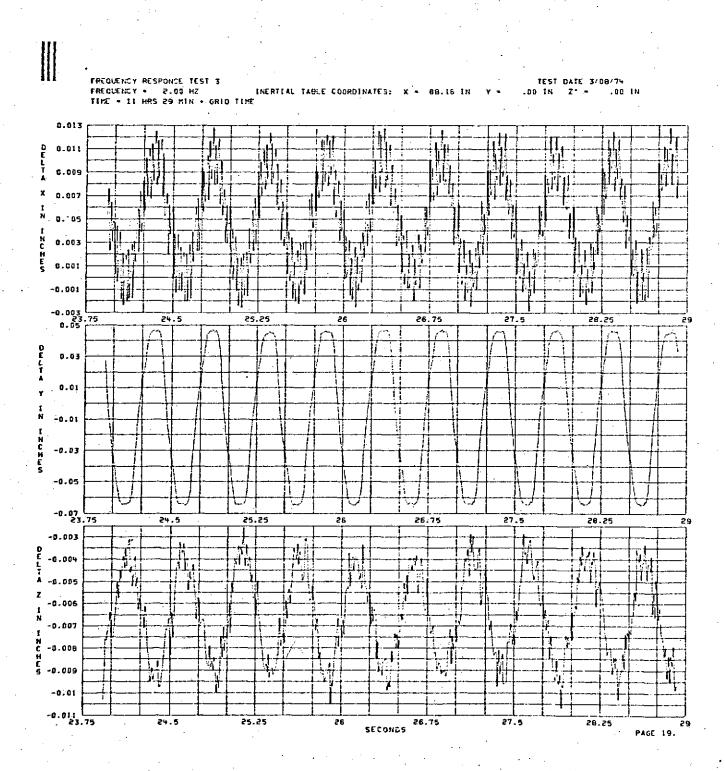


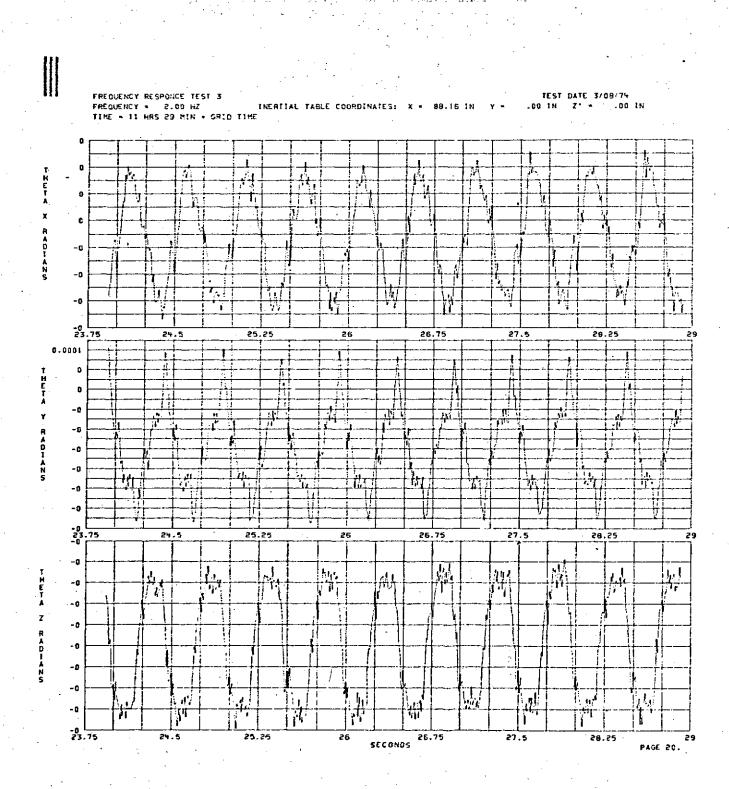


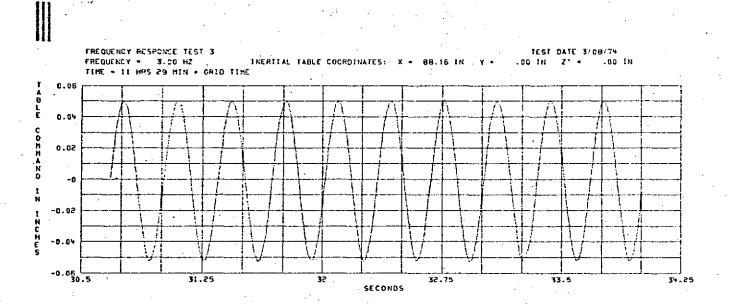
PAGE 15.

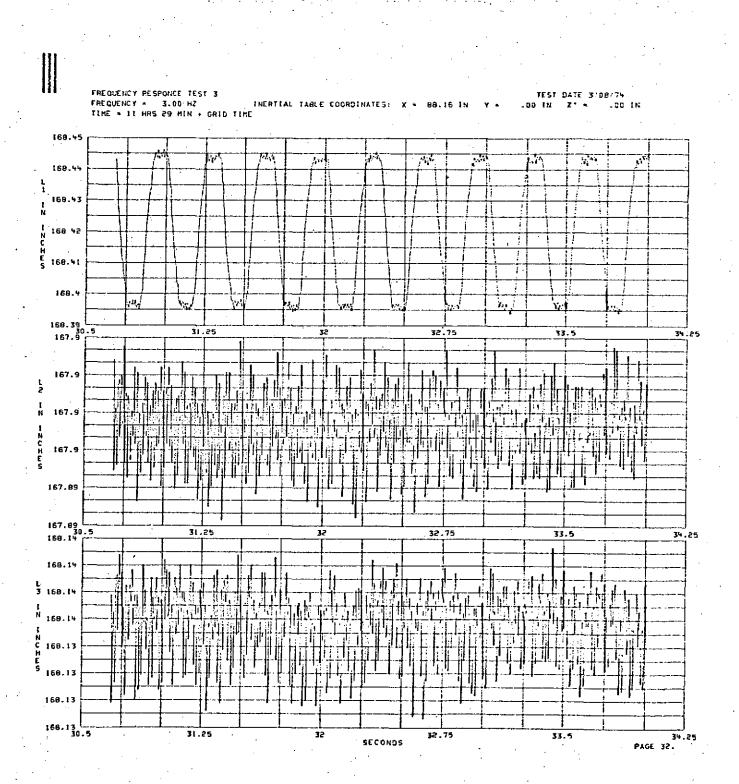






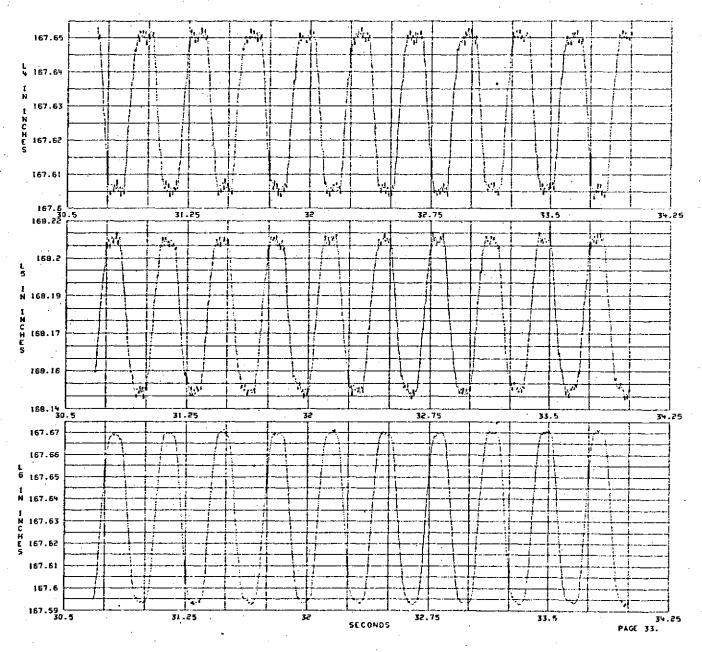


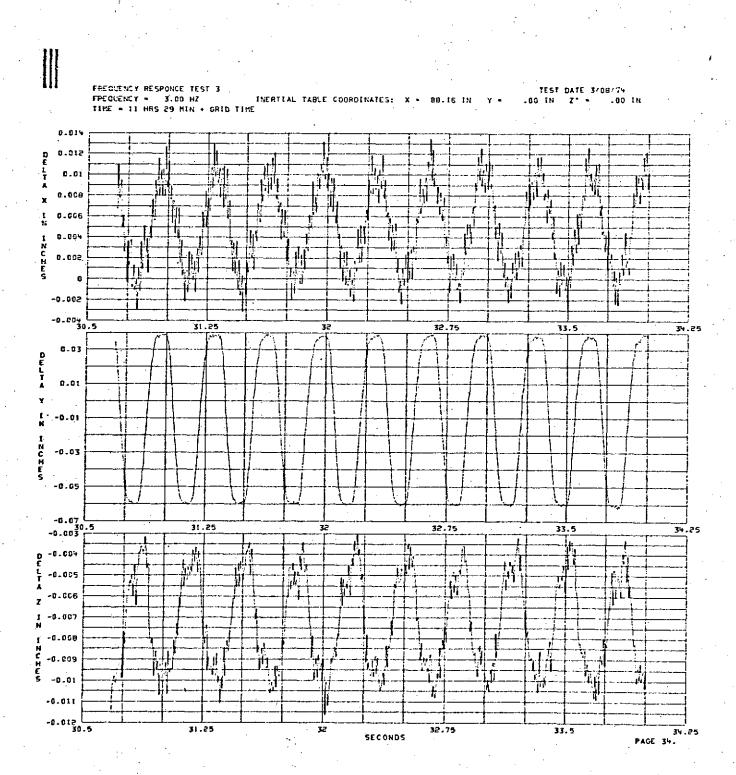


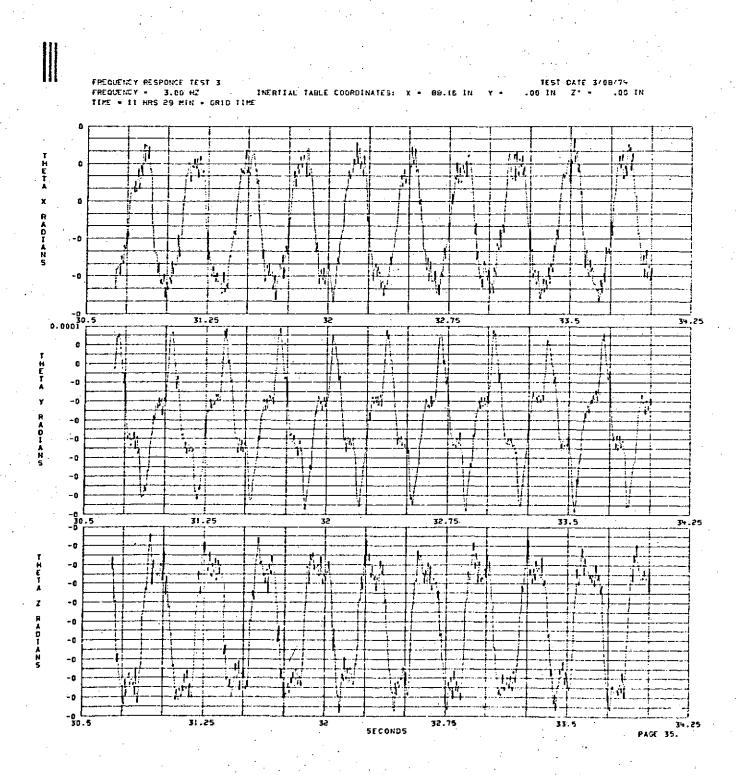


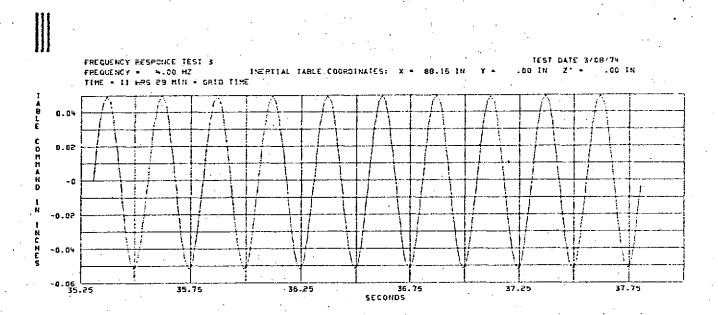
FREQUENCY RESPONCE TEST 3

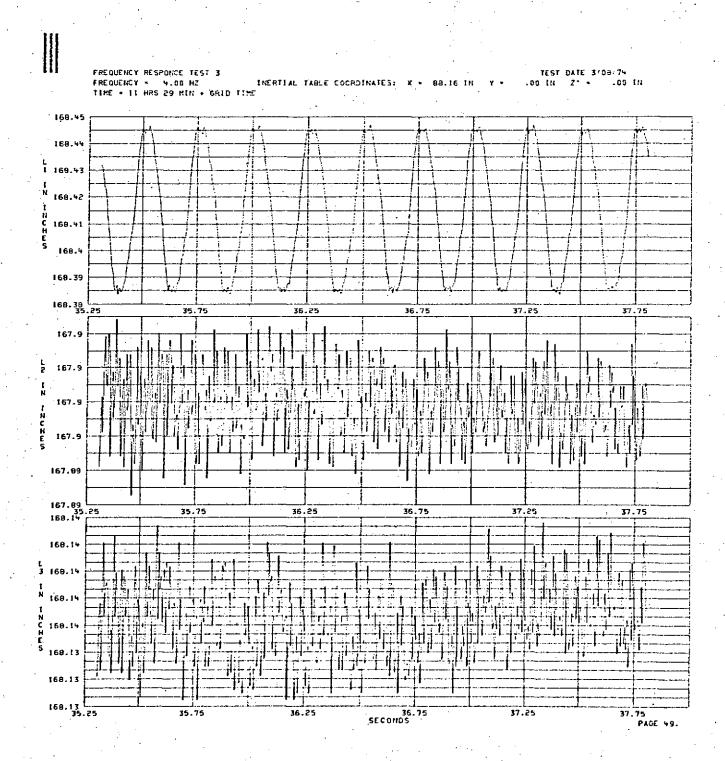
FREQUENCY = 3.00 HZ IMERTIAL TABLE COORDINATES: X = 88.15 IN Y = .00 IN Z* = .00 IN TIME = 11 HRS 29 MIN + GRID TIME

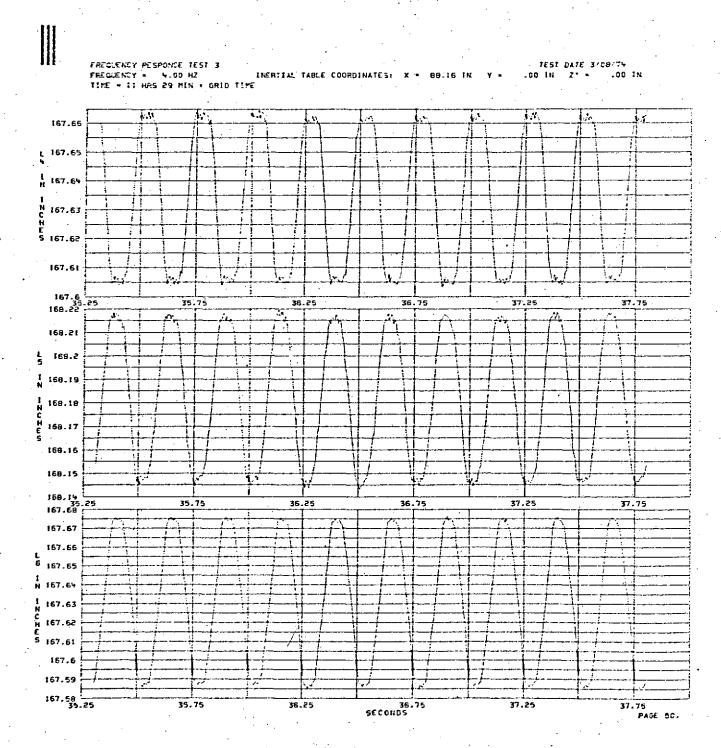


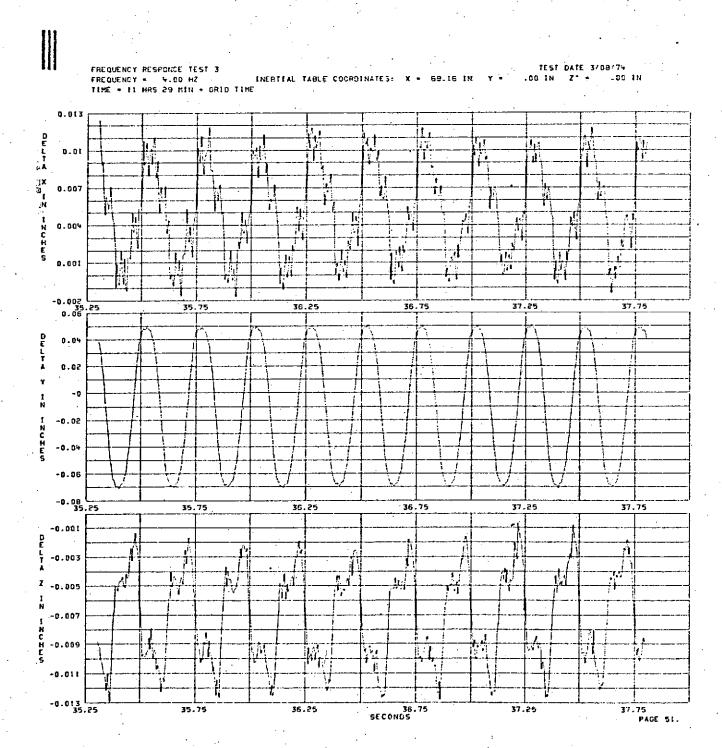


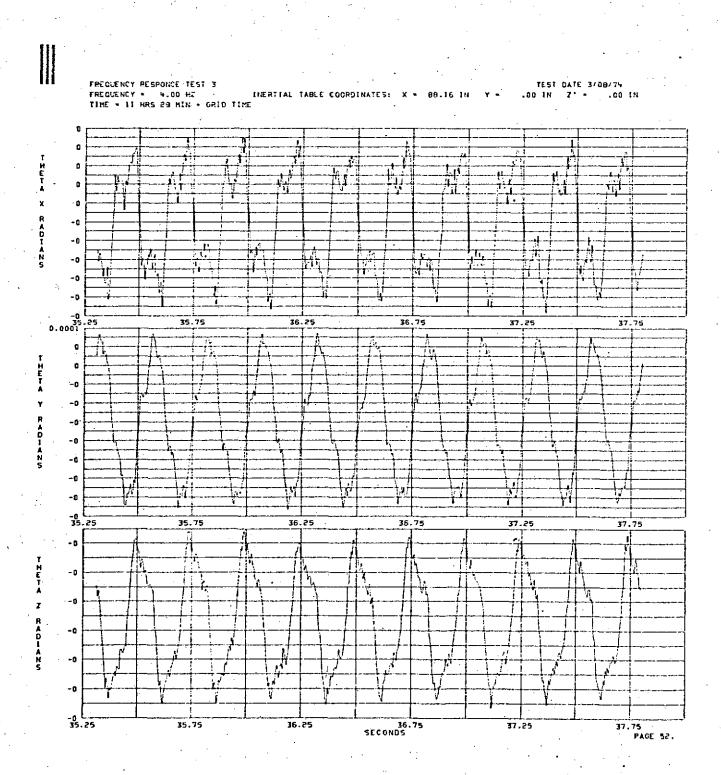


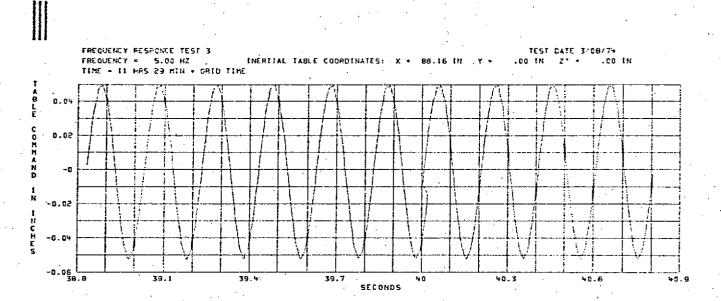


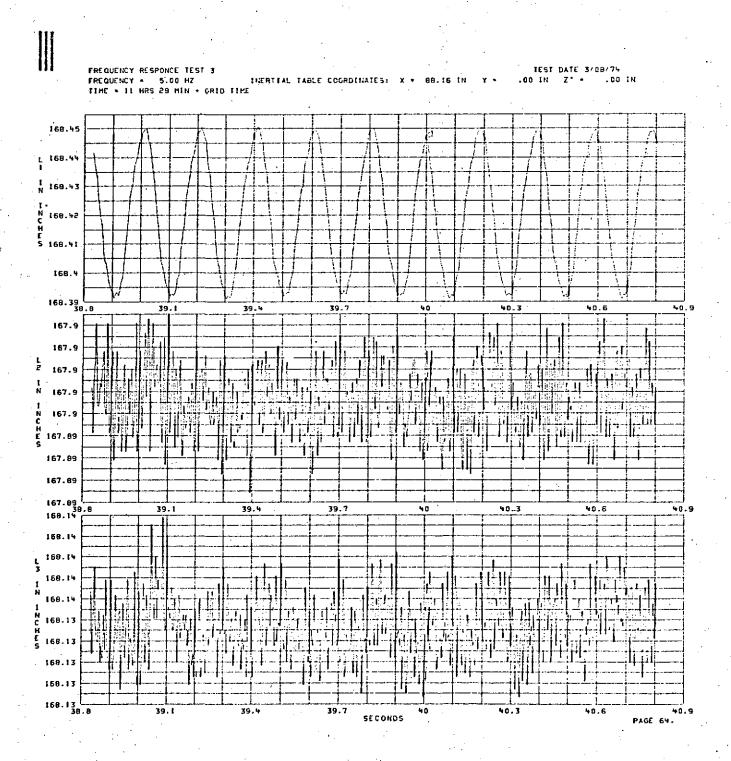


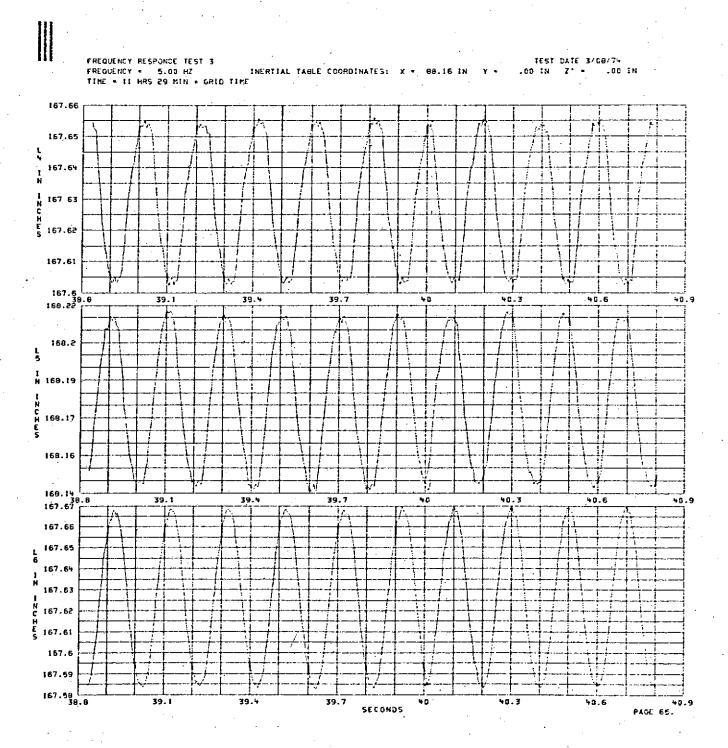


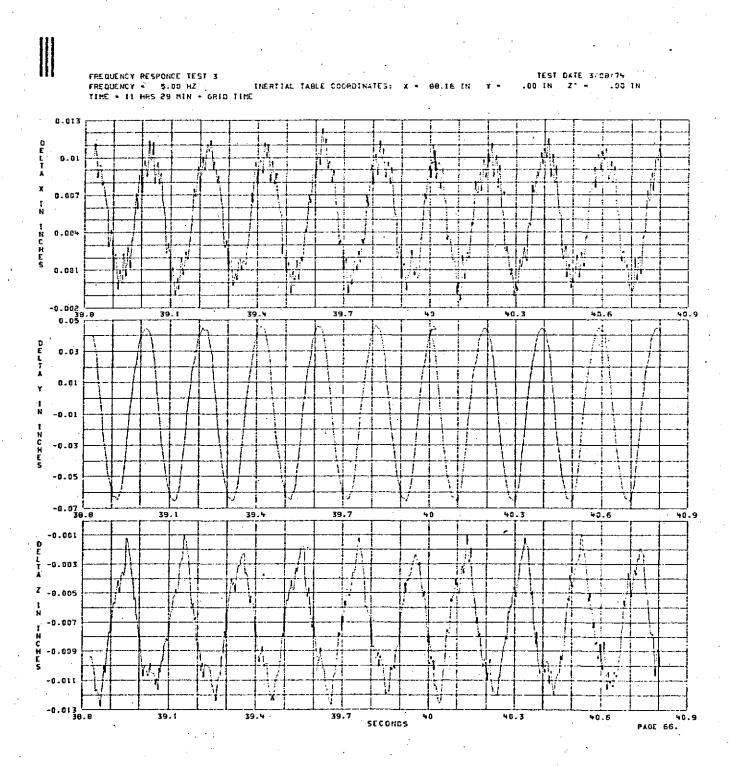


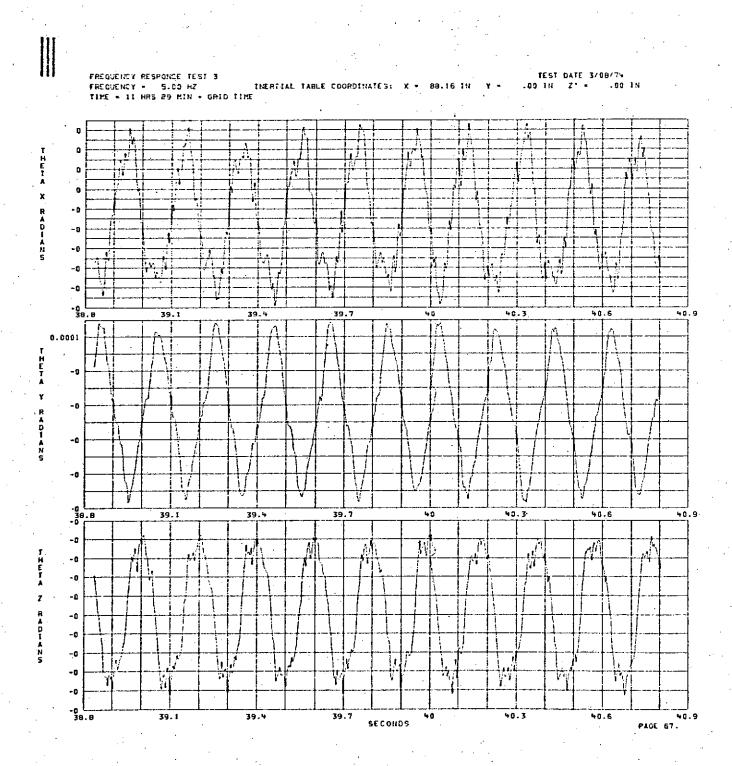


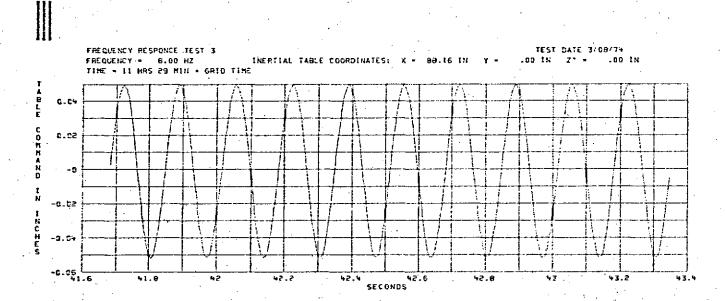




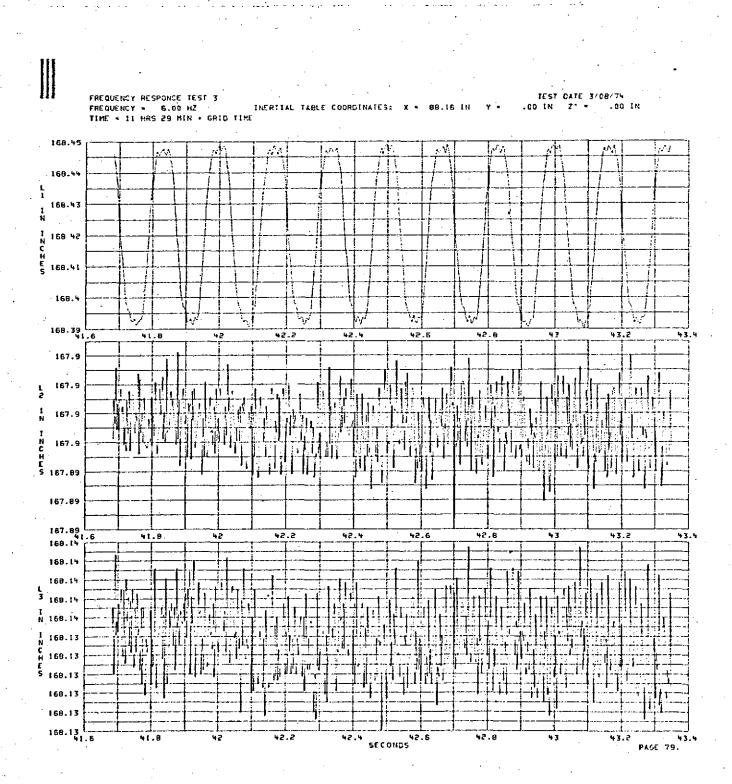


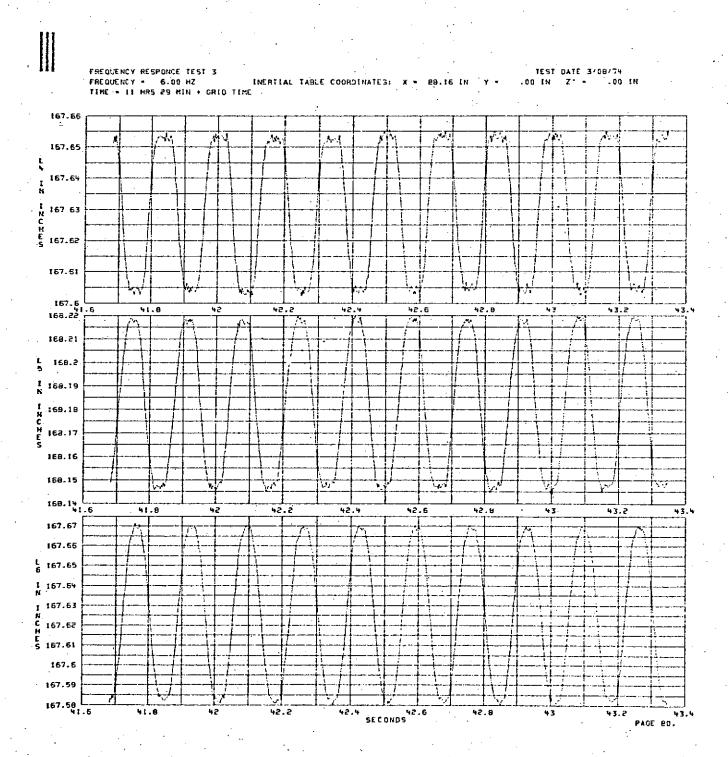


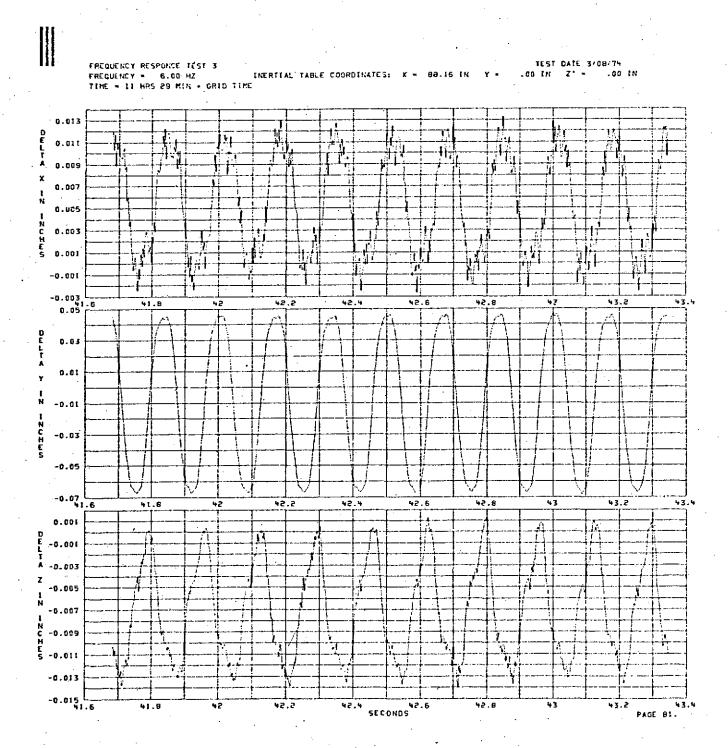


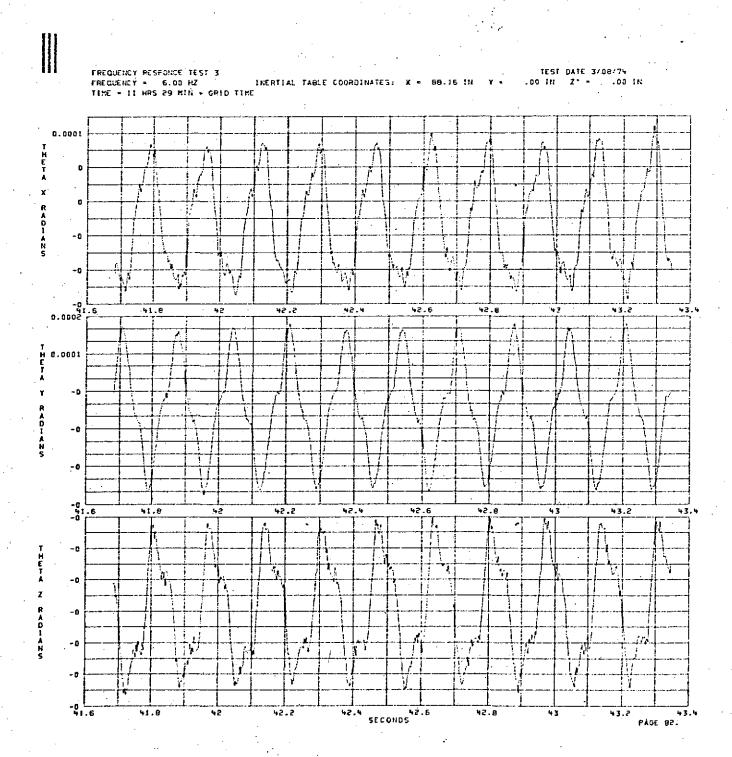


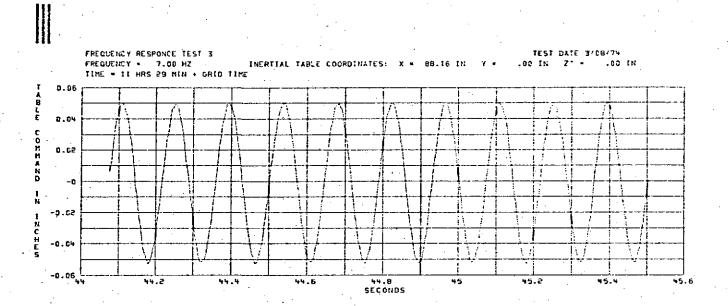
PAGE 78.

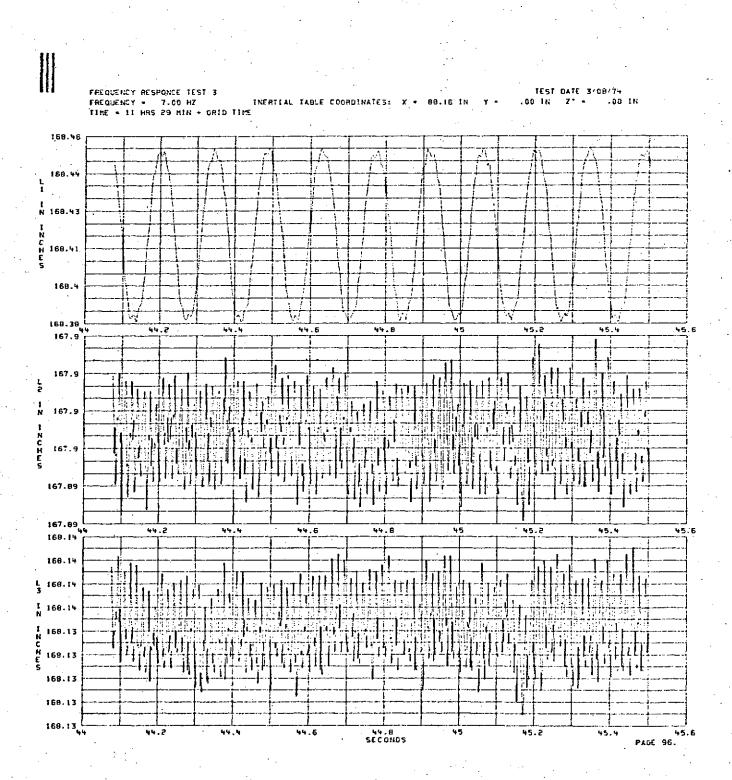


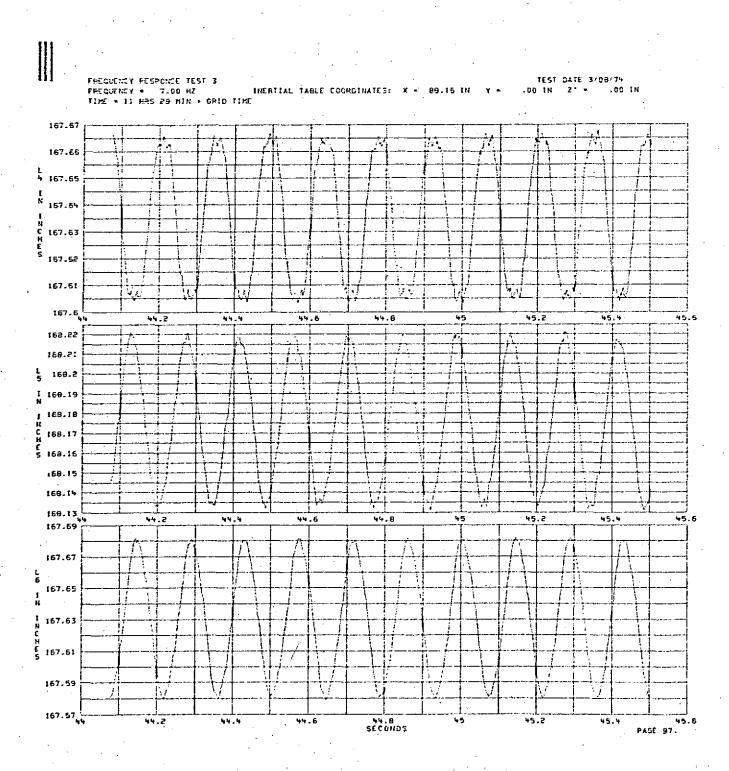


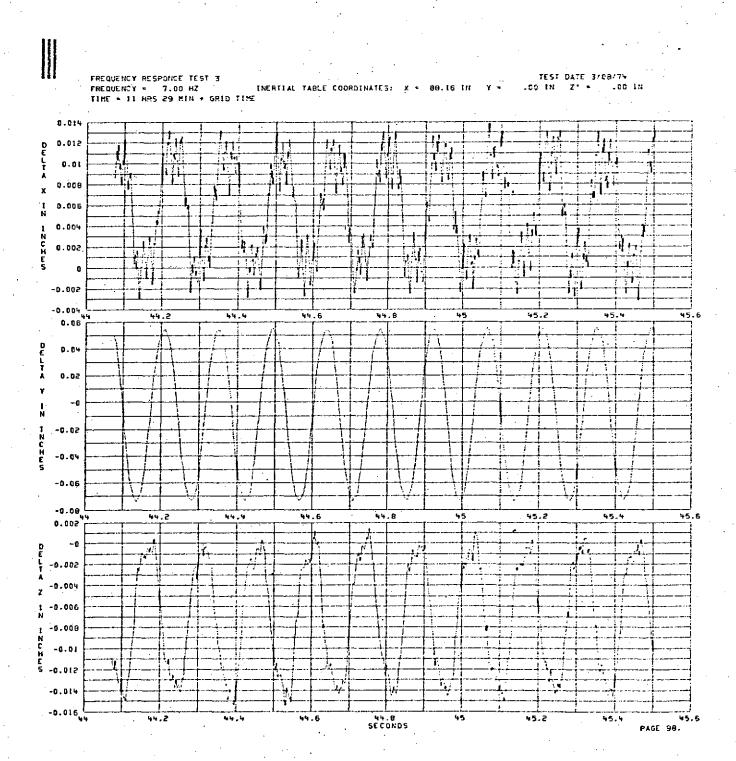


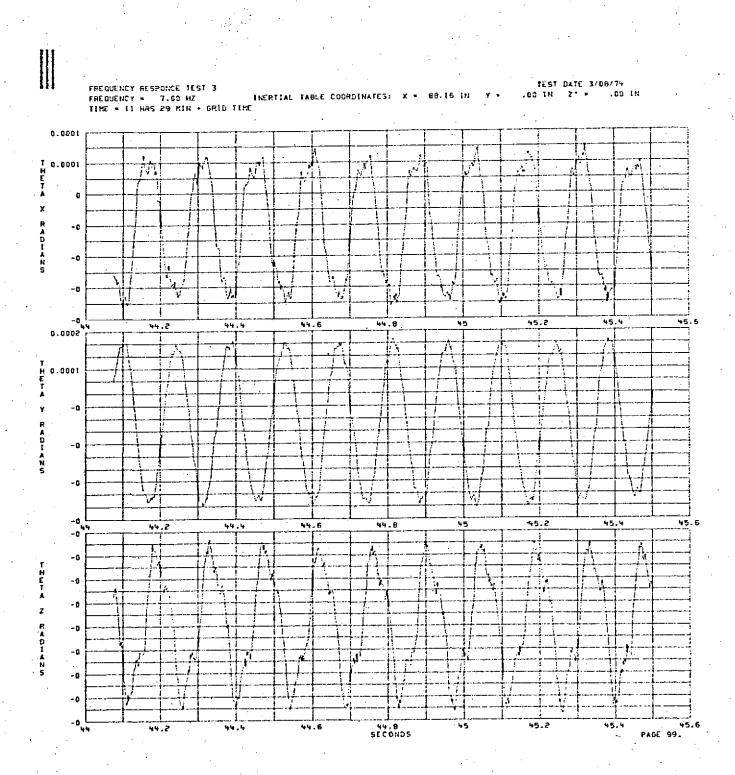


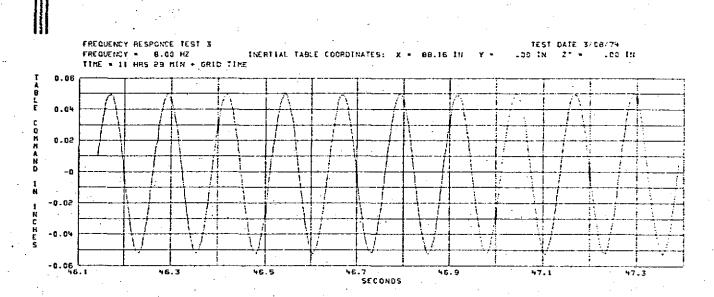


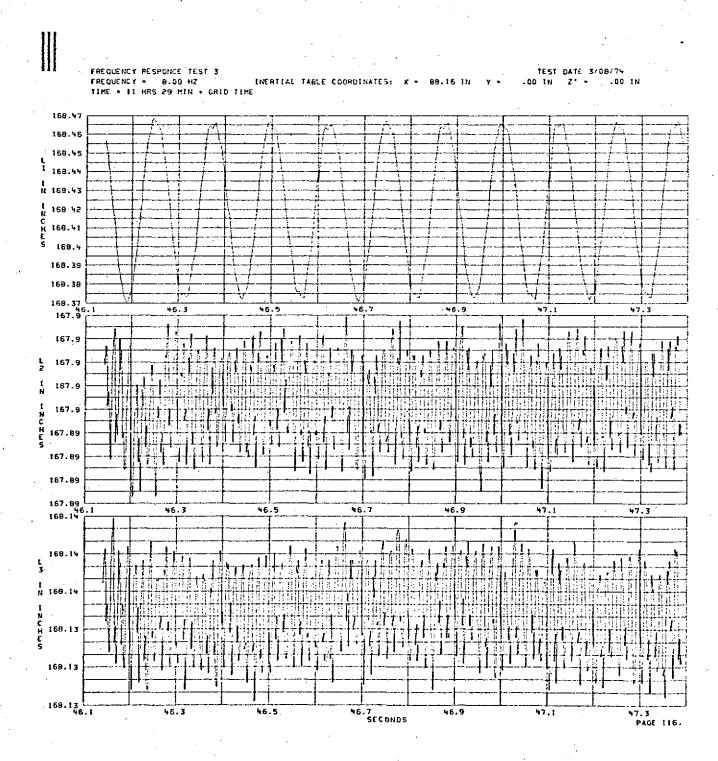


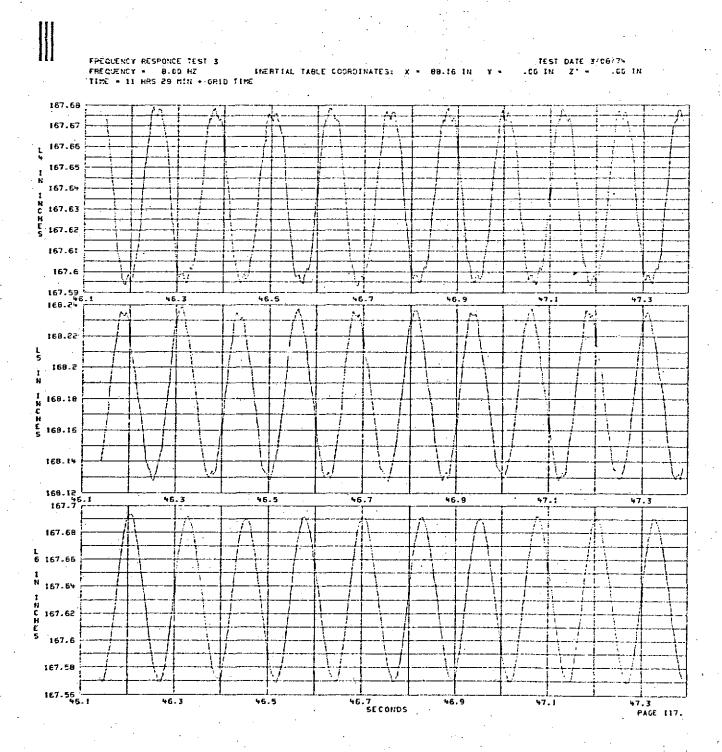


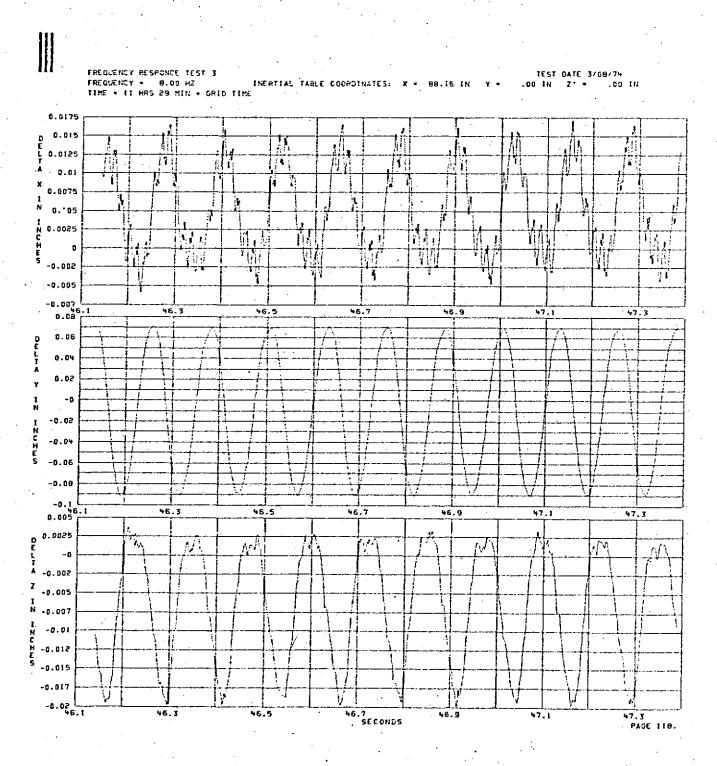


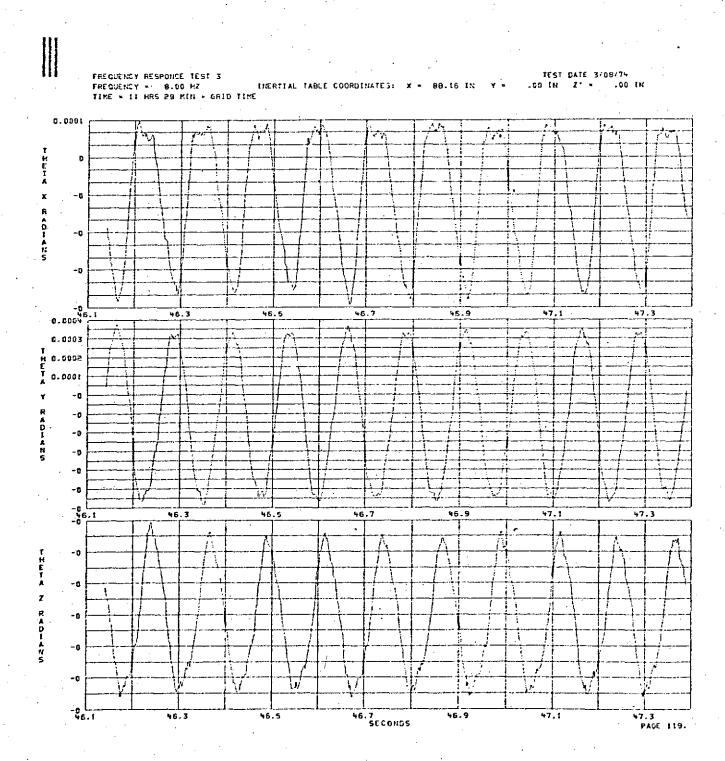


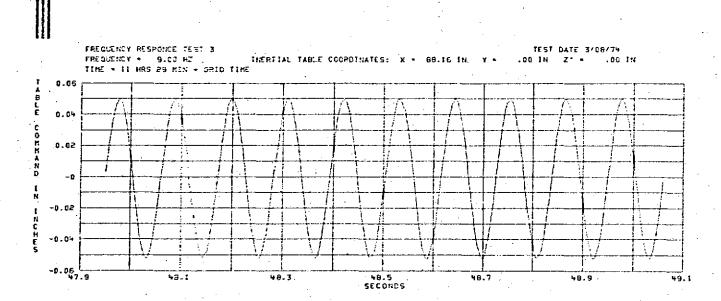




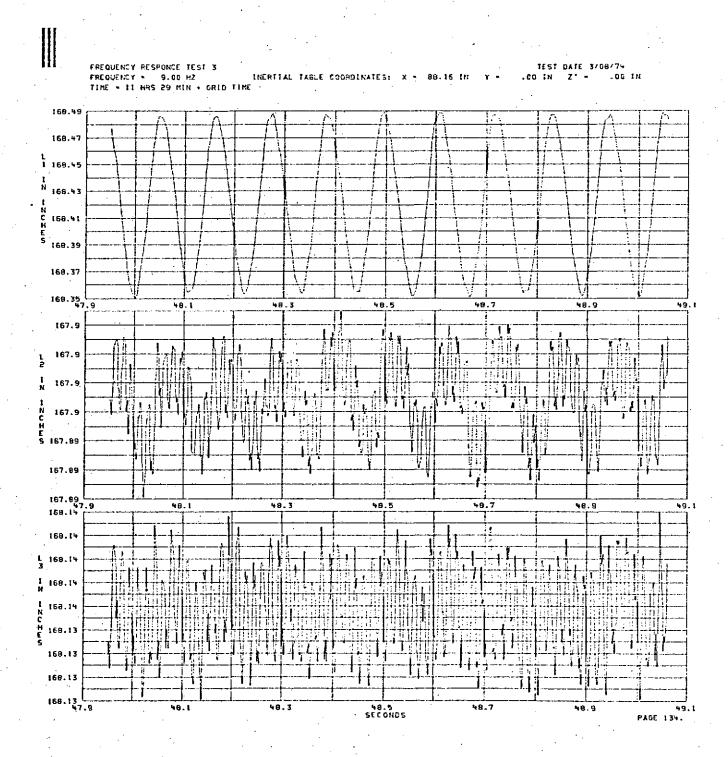




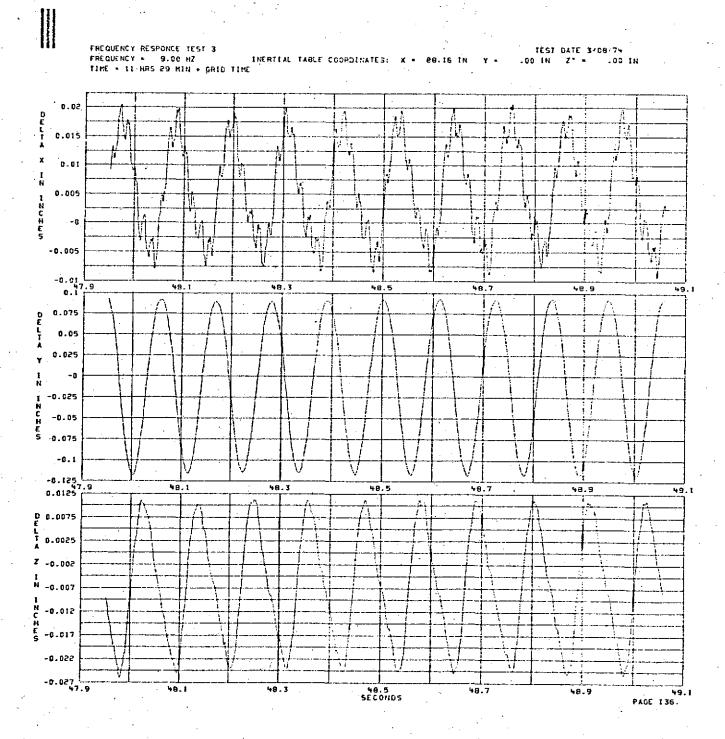


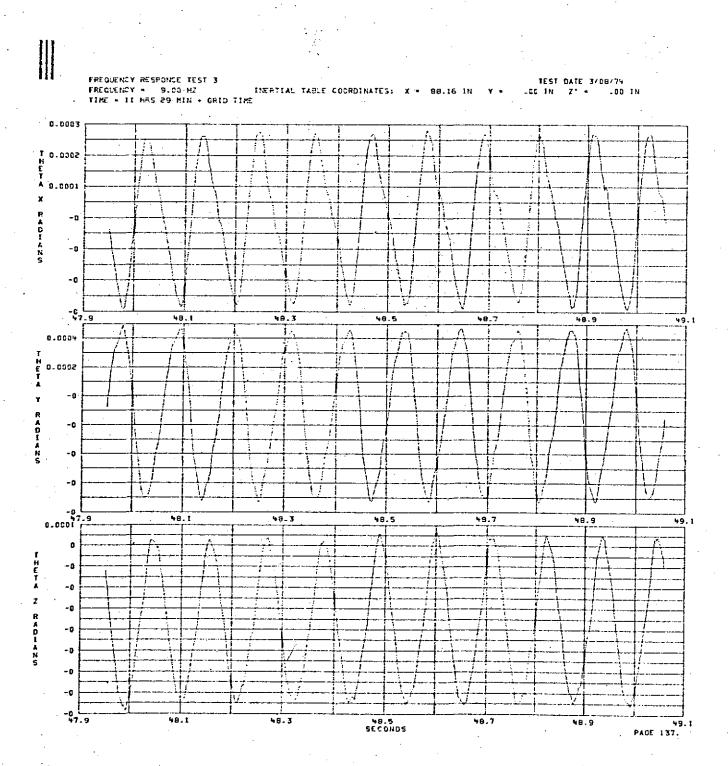


PAGE 133.



.00 IN FREQUENCY = 9.00 HZ TIME = 11 HRS 29 MIN + GRID TIME INERTIAL TABLE COORDINATES: X = 88.16 IN .00 IN 7" . 167.69 L 167.67 1 167.65 1 N 167.63 C H E S 167.61 167.59 167.57 L 168.26 49.1 48.3 48.5 48.7 48.9 4 : N 168.2 1 N C H 158.17 E S 168.14 168.11 48.3 46.1 48.5 49.1 167.71 167.69 I N 167.65 1 N 167.63 C H E 167.61 167.59 167.55 40.7 48.9 PAGE 135.





FREQUENCY RESPONSE TEST 3

REFFRENCE SENSOR - TARCOM

TOTAL CYCLES PROCESSED - 0

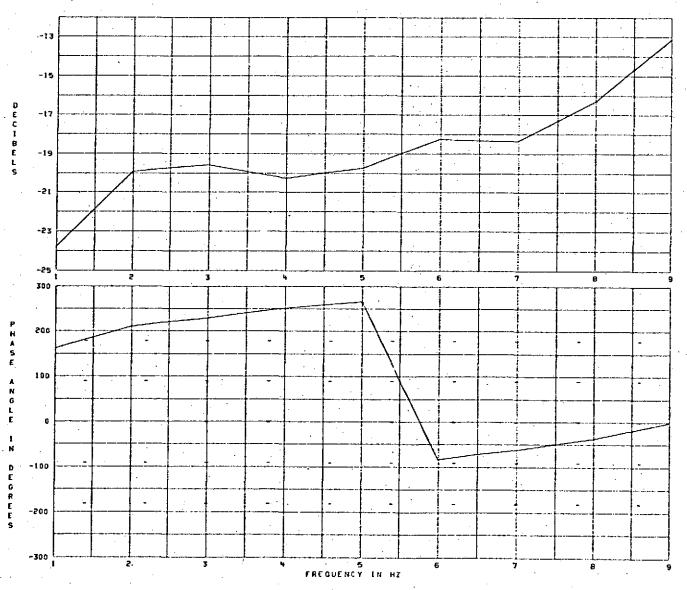
FIRST FREQUENCY - 1.00 HZ

BANDHIDTH PANSE FGR FREQUENCY INTERVAL TO DATE PROCESSED - 894PR74 TOTAL PERIOD PROCESSED *
FREQUENCY INCREMENTS' *
.900 HZ 42.43 SEC 1.00 HZ 9.00 HZ WAS .100 HZ TO 0.0511 0.0509 0.0507 C.0505 0.0503 0.0501 FREQUENCY IN HZ

FREQUENCY RESPONCE TEST 3
SENSOR -DELT X NORMALIZED BY REFERENCE SENSOR -TABCOM
TOTAL CYCLES PROCESSED > 0
FIRST FREQUENCY = 1.00 HZ
BANDWIDTH RANGE FOR FREQUENCY INTERVAL TO 9.00 HZ WAS

BATE PROCESSED - 09APR74

TOTAL PERIOD PROCESSED + 42.43 SEC FREQUENCY INCREMENTS + 1.00 HZ 1.900 HZ



.100 HZ TQ

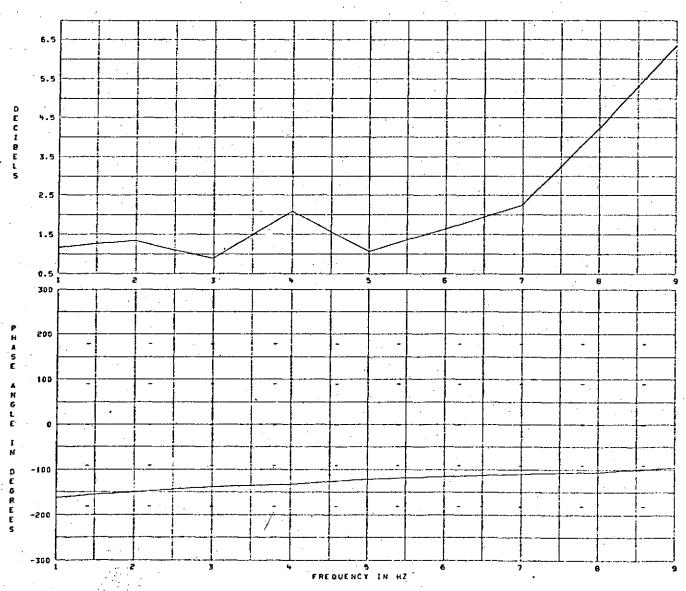
PAGE 1.

FREQUENCY RESPONSE TEST 3
SENSOR -DELT Y NORMALIZED BY REFERENCE SENSOR -TABCOM
TOTAL CYCLES PROCESSED = 0
FIRST FREQUENCY = 1.00 HZ
BANDHIDTH FANGE FOR FREQUENCY INTERVAL TO 9.00 HZ WAS

DATE PROCESSED - 09APR75

FREQUENCY INCREMENTS .

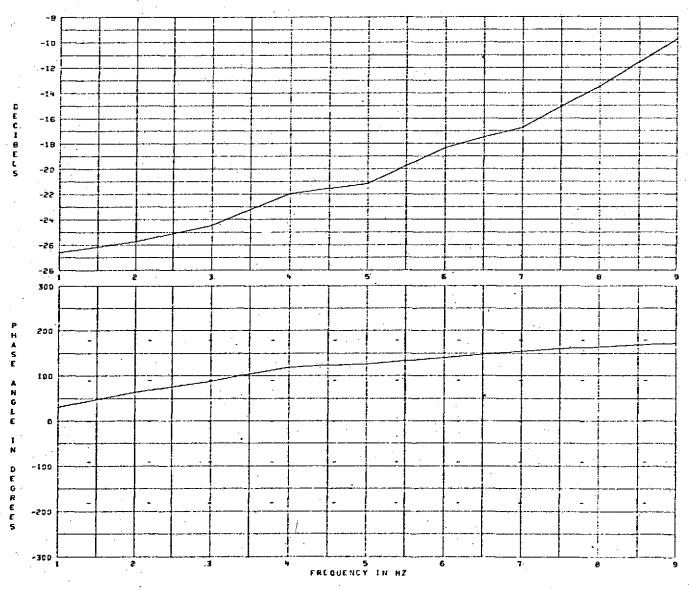
42.43 SEC 1.00 HZ



PAGE 2.

DATE PROCESSED - SSAPR74

FREQUENCY RESPONCE TEST 3
SENSOR -DELT Z NORMALIZED BY REFERENCE SENSOR -TABCOM
TOTAL CYCLES PROCESSED - 0
FIRST FREQUENCY - 1.00 HZ
BANGRIDTH PANGE FOR FREQUENCY INTERVAL TO 9.00 HZ HAS TOTAL PERIOD PROCESSED FREQUENCY INCREMENTS .909 MZ 42.43 SEC 1.00 HZ 9.00 HZ #45 .100 HZ TO



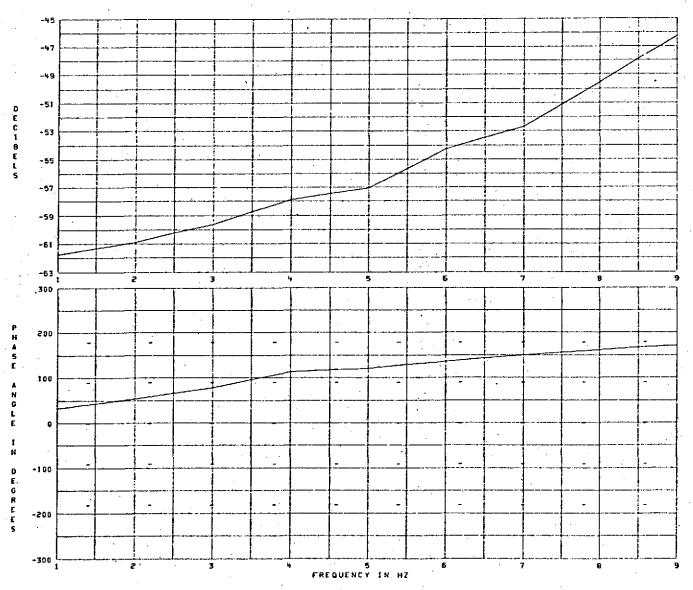
FREQUENCY RESPONCE TEST 3

SENSOR -XTHETA NORMALIZED BY REFERENCE SENSOR -TABCOM
TOTAL CYCLES PROCESSED - D

FIRST FREQUENCY - 1.00 HZ
BANDHIDTH RAYSE FOR FREQUENCY INTERVAL TO 9.00 HZ HAS

DATE PROCESSED - 09APR74

FOTAL PERIOD PROCESSED • 42.43 SEC FREQUENCY INCREMENTS • 1.00 HZ .900 HZ



.130 HZ TO

FREQUENCY RESPONSE TEST 3

SENSOR -YTHETA NORMALIZED BY REFERENCE SENSOR -TAGGOM
TOTAL CYCLES PROCESSED - 0

FIRST FREQUENCY - 1.00 HZ

TOTAL PERIOD PROCESSED .

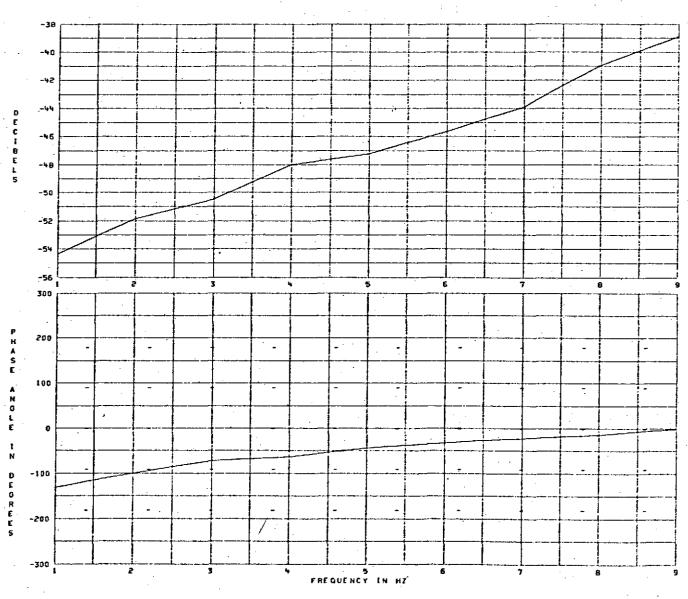
1.00 HZ

DATE PROCESSED - 09APR74

BANDRIDTH RANGE FOR FREQUENCY INTERVAL TO

.100 HZ 10

FREQUENCY INCREMENTS



PAGE 5.

FPEQUENCY RESPONCE TEST 3

SENSOR -ZTHETA NORMALIZED BY REFERENCE SENSOR -TABCOM
TOTAL CYCLES PROCESSED = 0

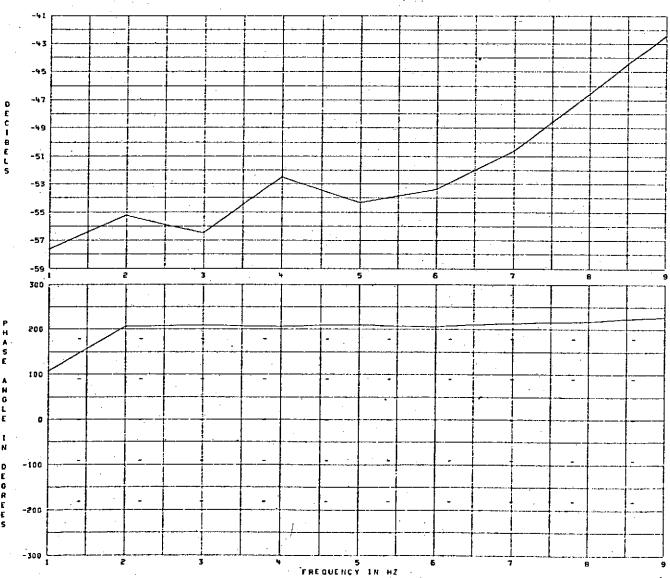
FIRST FREQUENCY = 1.00 HZ
BANDHIDTH RANGE FOR FREQUENCY INTERVAL TO 9.00 HZ HAM

TOTAL PERIOD PROCESSED . FREQUENCY INCPEMENTS - .900 HZ

1.00 HZ

9.00 HZ WAS

.100 HZ TO



PAGE 6.

APPENDIX D

TEST NO. 4 X-AXIS

DDIS FREQUENCY RESPONSE TEST SUMMARY OF INPUT INERTIAL CONDITIONS AND TRANSFORM MATRIX

FREQUENCY RESPONCE TEST 4

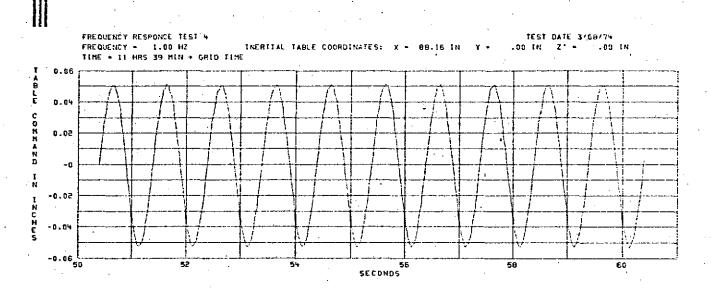
TEST DATE: 3/08/74

			TABLE CO	DORDINATES	86.153	.00	.000			•
	SERVO TABLE SHIVEL JOINTS			FLOOR SHIVEL J		otuts	COMPONENTS OF ACTUATOR LENGTH		ACTUATOR	
ACTUATOR	x	Y	7	x x	Y	Z	х.	Y	· 2	LENGTH
1	.6000	25.1020	49.5000	210.4070	-64.3110	123.1700	-122.2480	89.4130	-73.6780	168.4272
2	0500	-55.4193	3.0000	210.4290	-76.380C	116.1240	-182.2700	20.9610	-113.1240	167.8879
3.	.0000	-55.4190	-3.0000	2:0.4220	-74.5730	-116.8193	-122.2630	19.1540	113.8190	168.1365
4	10000	25.1020	-49.5009	210.4170	-62.4120	-123-6930	-122.2560	87.5140	74.1830	167.6569
5	.0000	30.2980	~45.5300	210.4100	139.4630	-5.9750	-122.2510	-108.1650	-40.5250	169.1991
В	.0900	30.2980	46.5000	210.3690	138.3890	B.0050	-122.2100	~108.0910	38.4950	167.6330

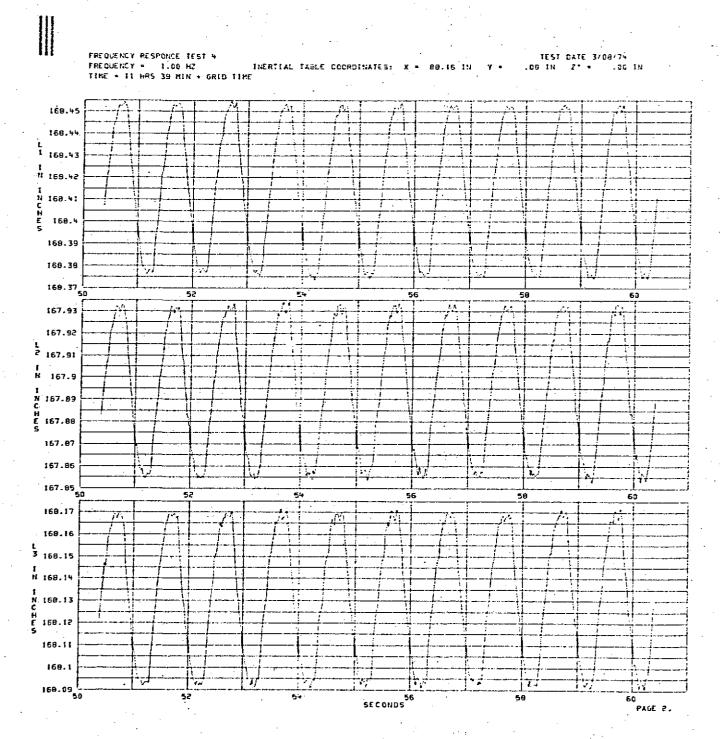
TRANSFORM MATRIX

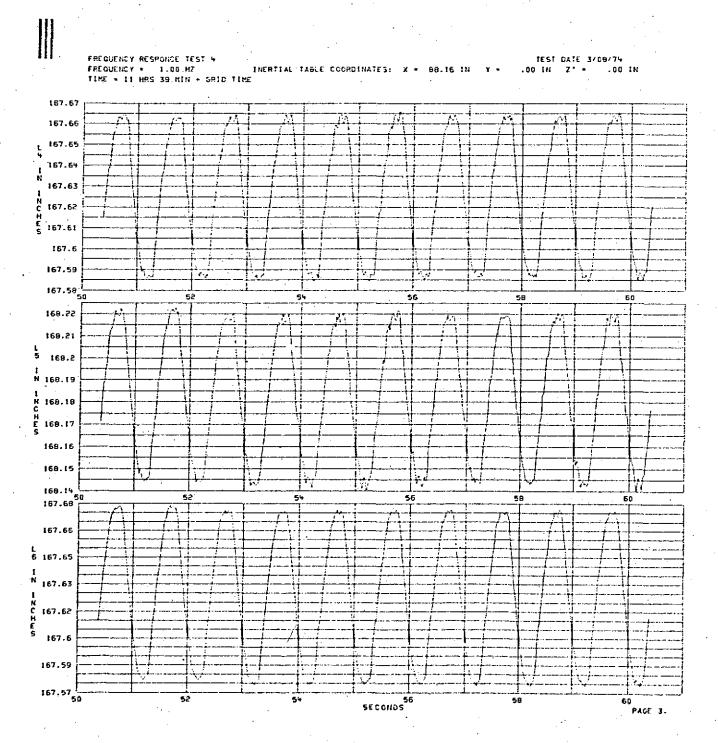
227790-00	eese	228575+00	229554+00	228266+00	230510+00
.447110+00	23602201	303266-01	.442709+00	416853+00	418525+00
222802+00	~.498159+00	.49,8501+00	.228740+00	276033+00	.26965:+00
450573-02	_449077-02	449777-02	.449626-02	450071-02	.448595-02
*.648215-02	.145547-02	146094-02	.650505-02	.794358-02	796998-02
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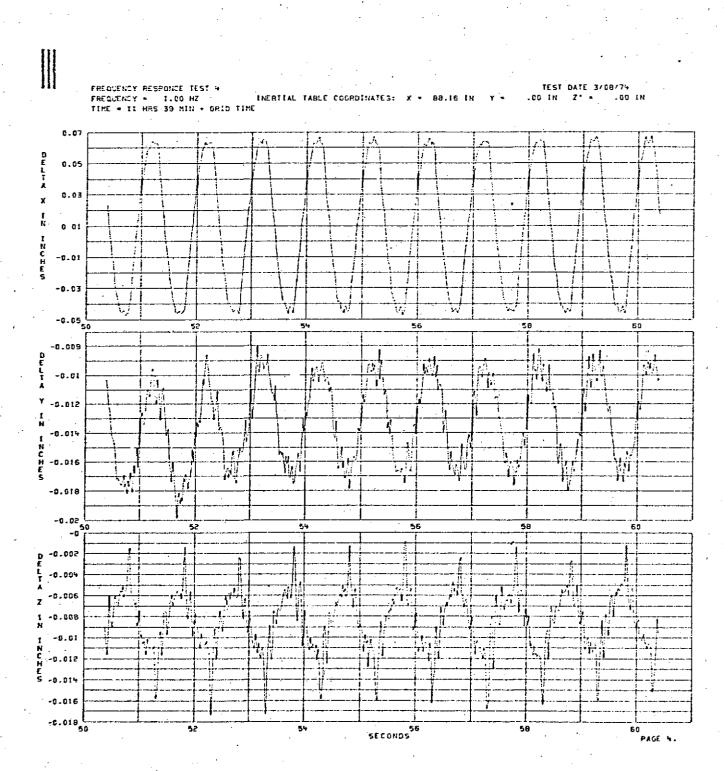
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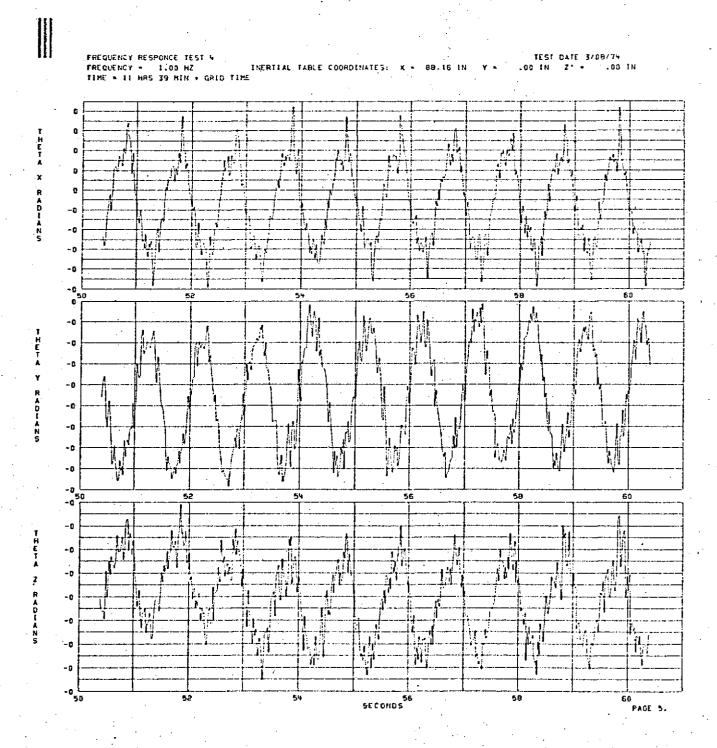


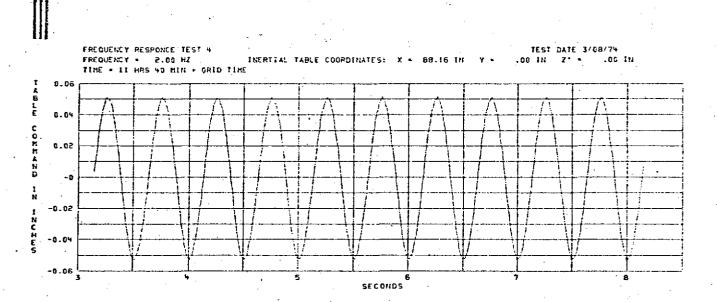
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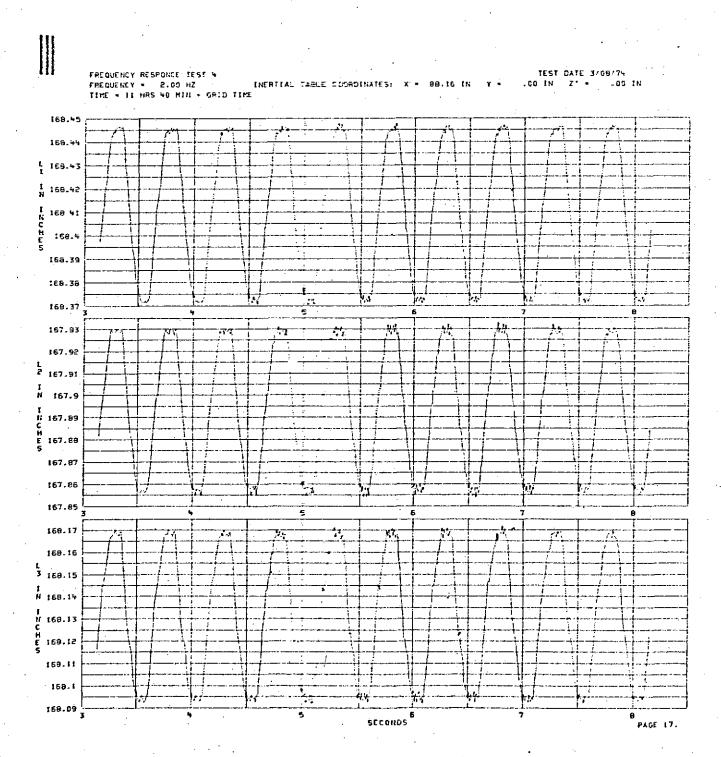


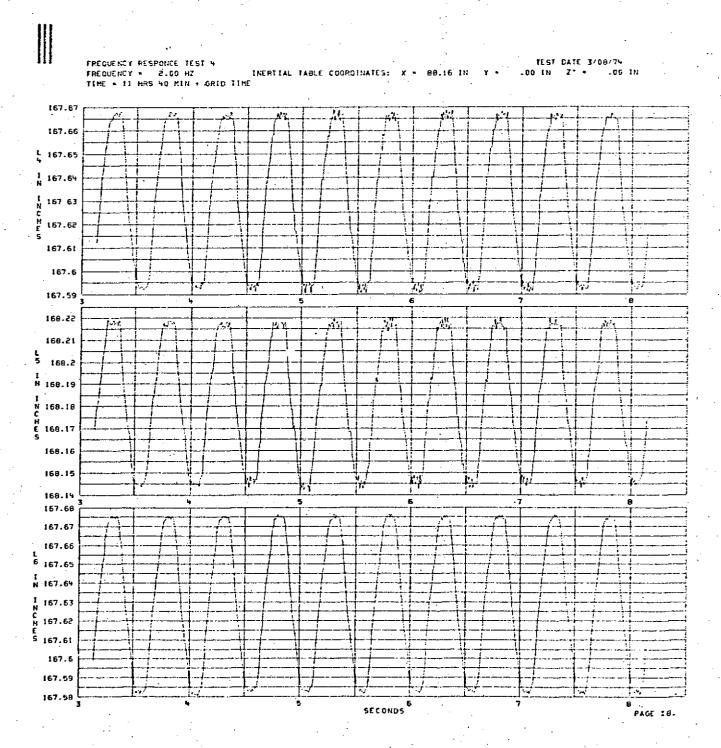


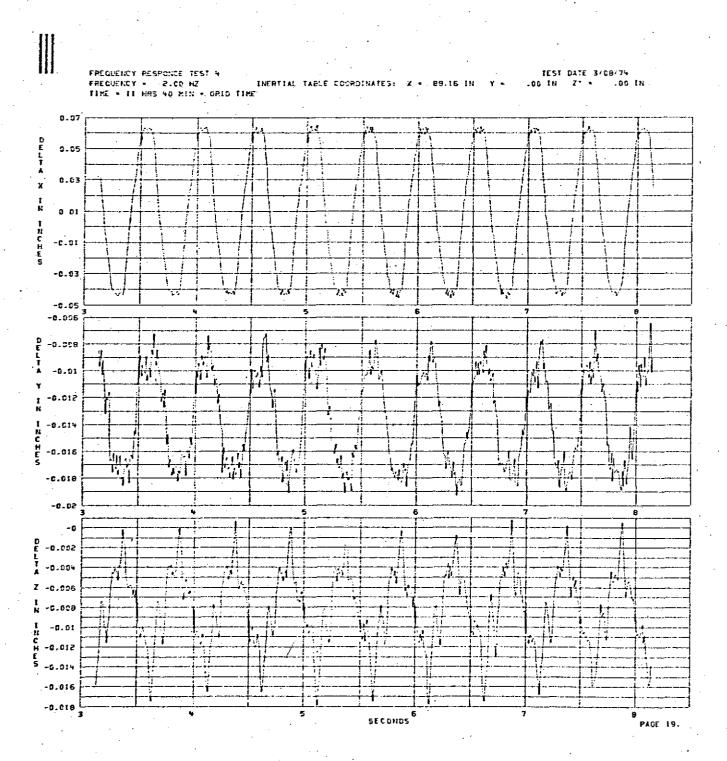


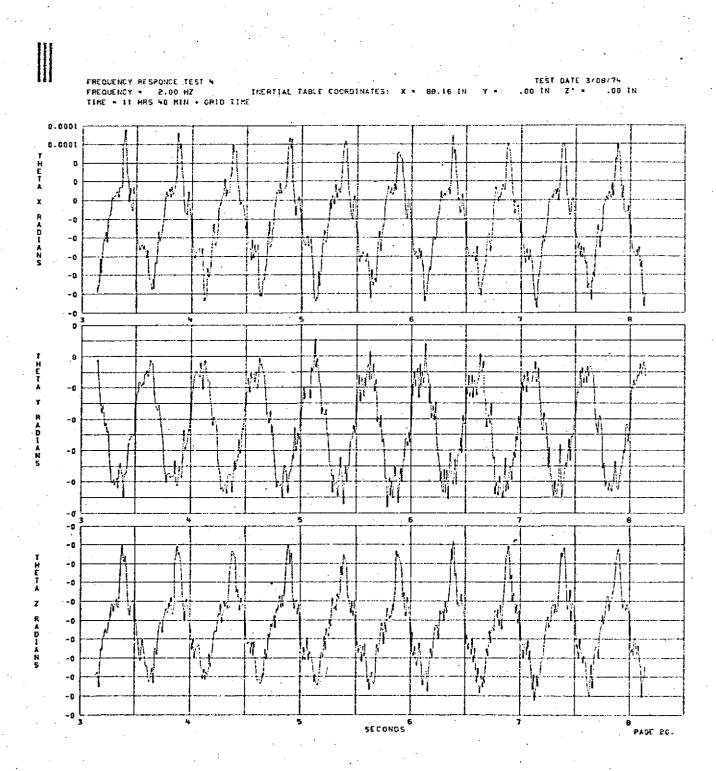


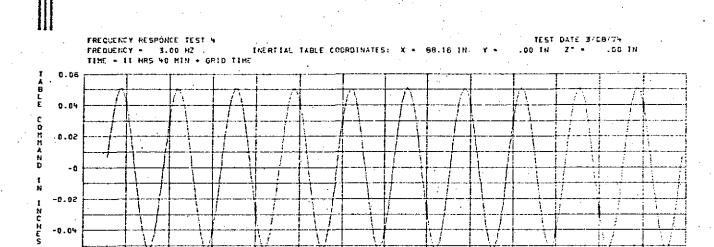
PAGE 16.











11.25

SECONDS

12.25

12.75

-0.02

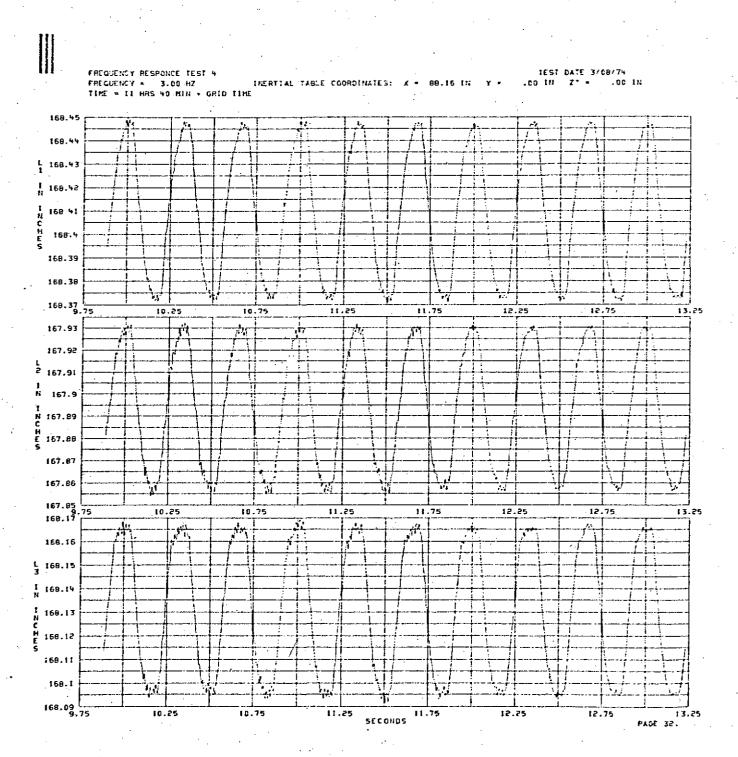
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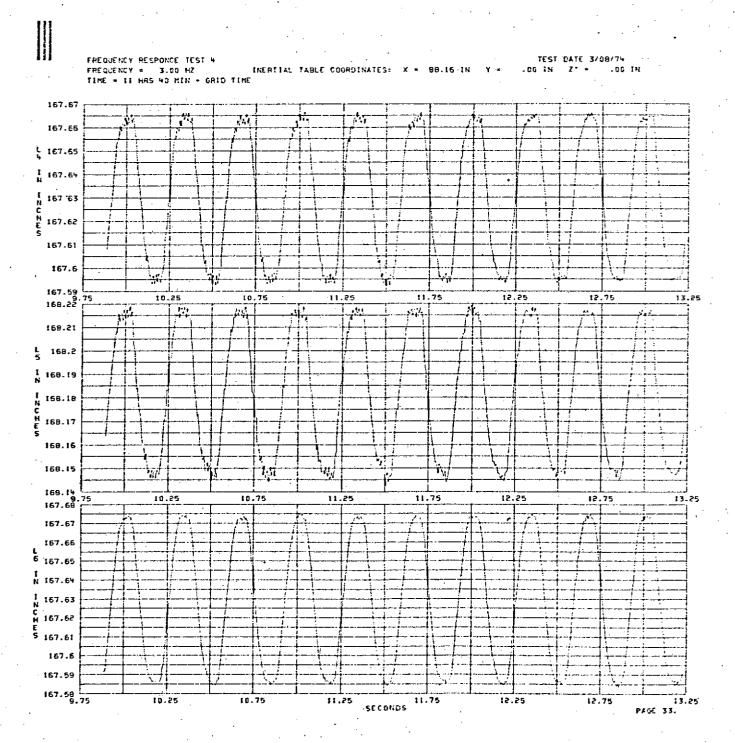
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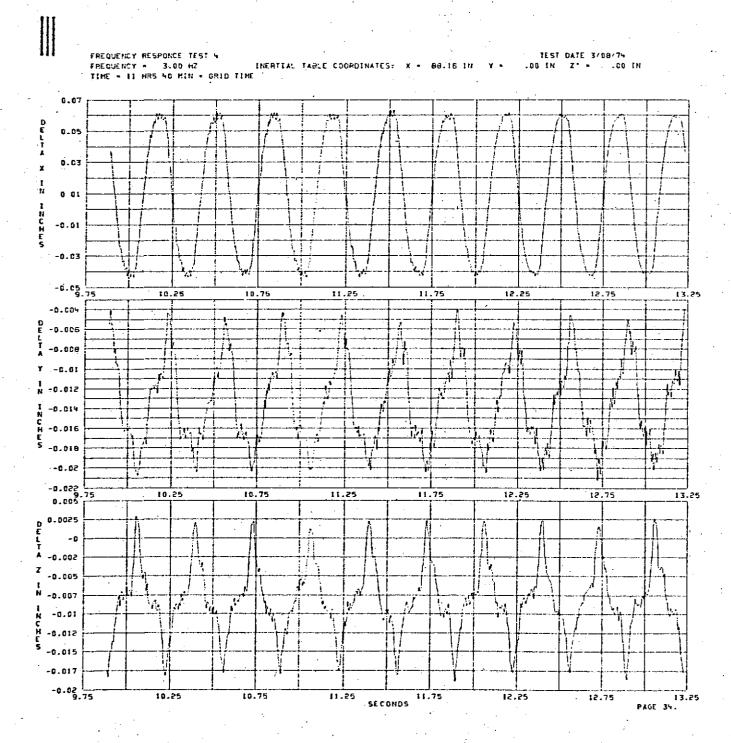
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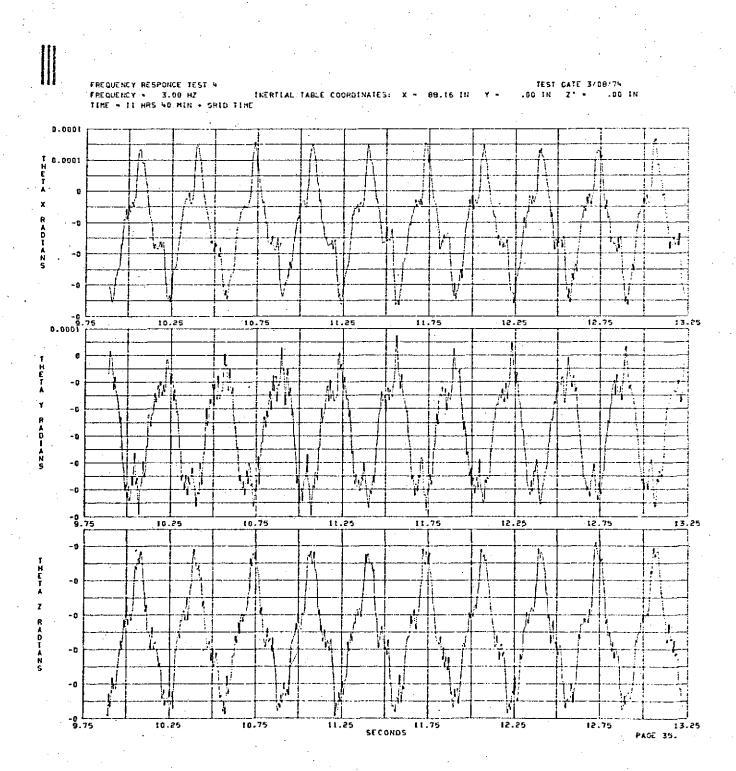
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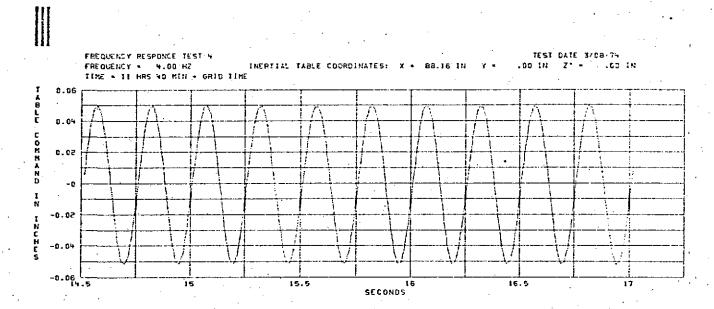
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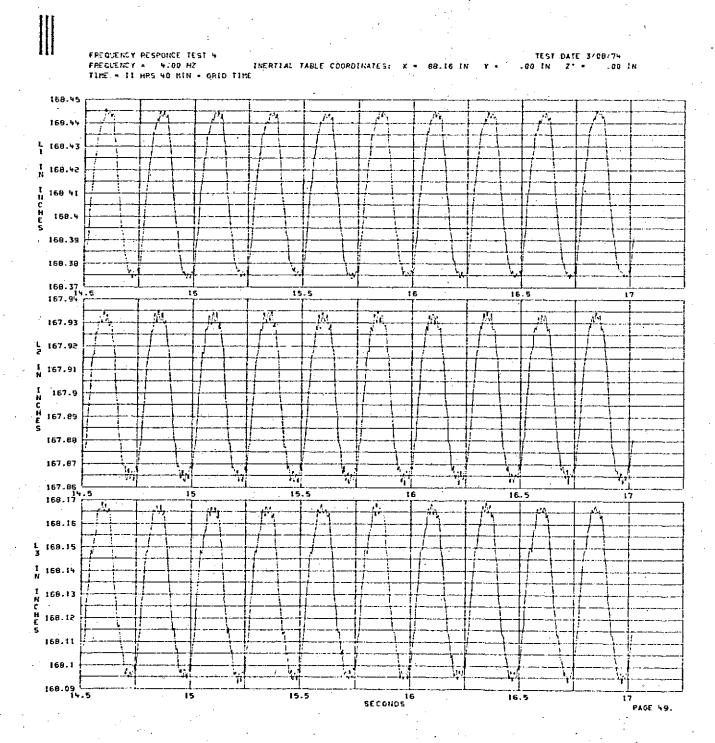


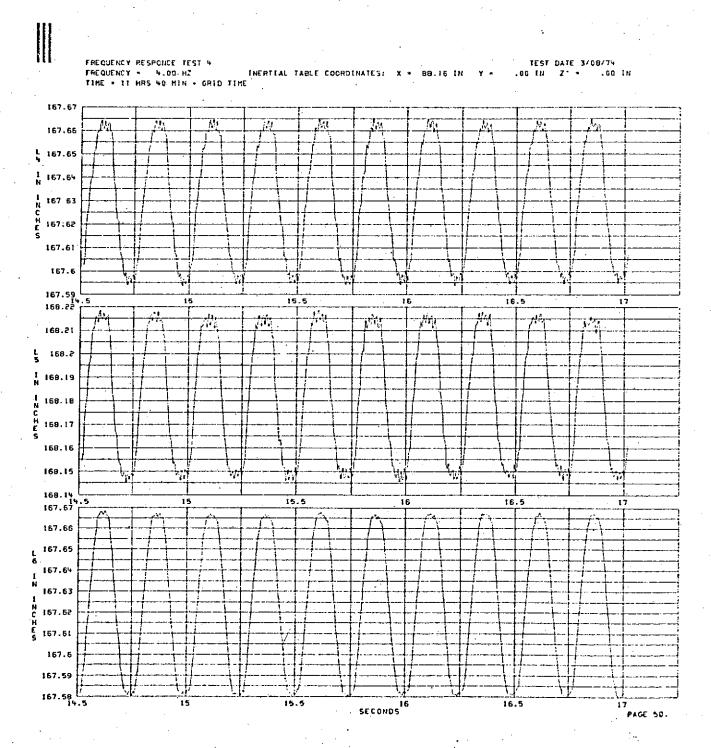




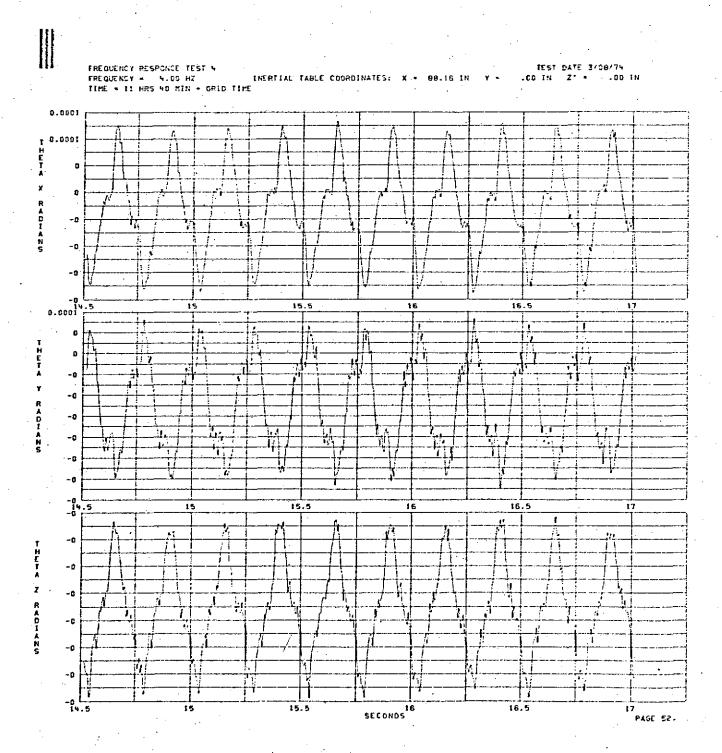


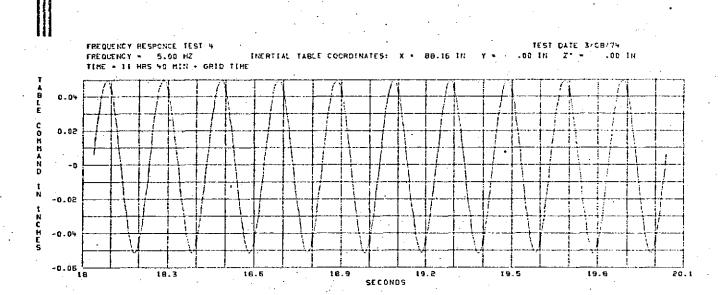
PAGE 48



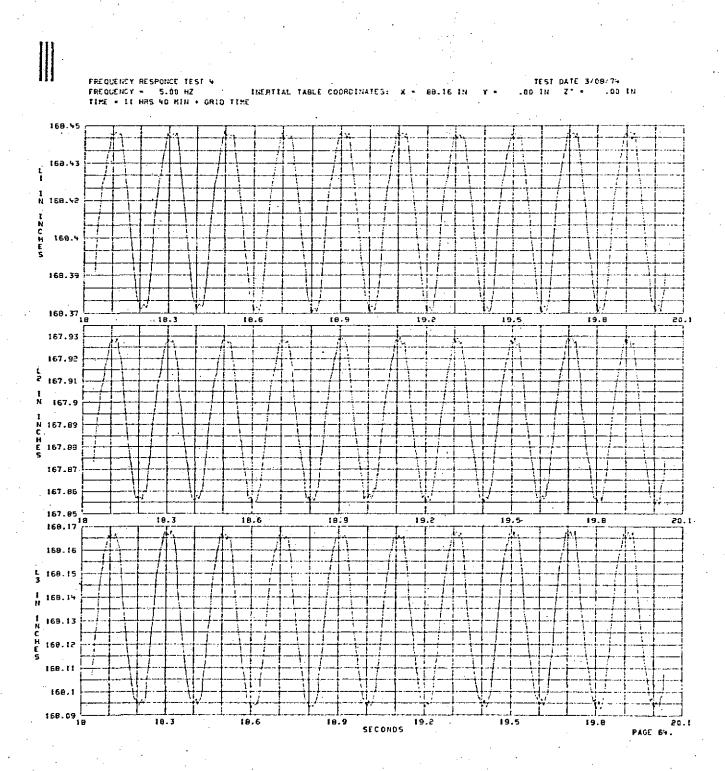


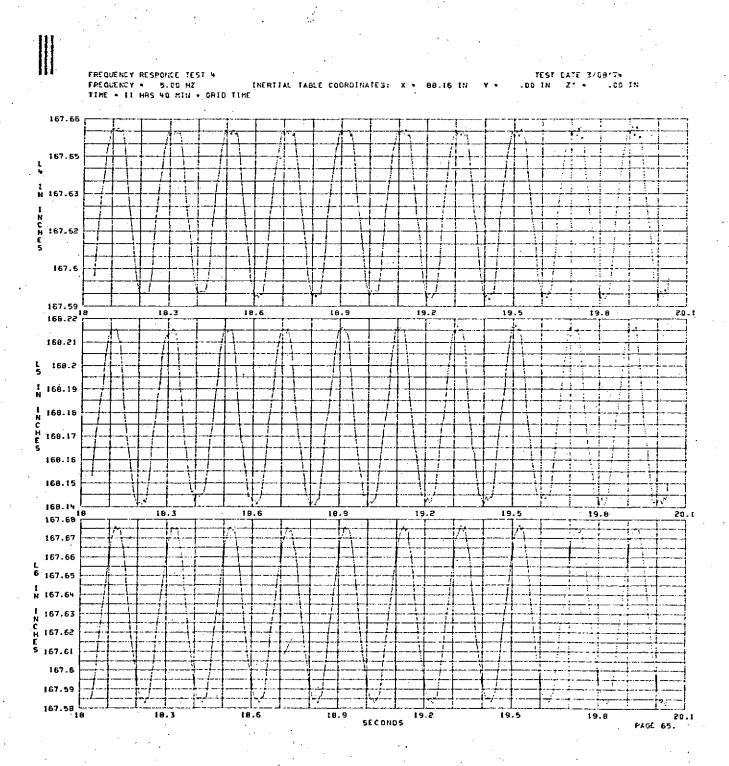
FREQUENCY RESPONCE TEST 4 FREQUENCY = 4.00 HZ TIME = 11 HRS NO HIN + GRID TIME IMERTIAL TABLE COORDINATES: X 0.07 0.05 0.03 0 01 -0.0t -0.03 -0.05 15.5 16.5 -0.002 -0.005 -0.007 -0.01 S10.0- H -0.015 C H -0.017 -0.02 -0.022 -0.025 L 15.5 15.5 -0.001 -0.003 Z -0.005 -0.007 -0.009 -0.011 -0.013 -0.015 16 SECONDS 16.5

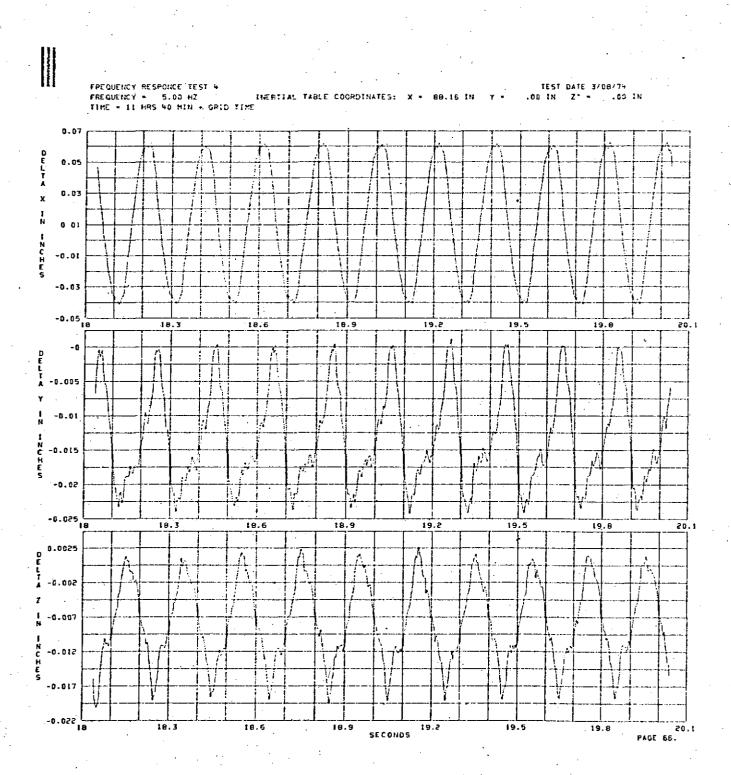


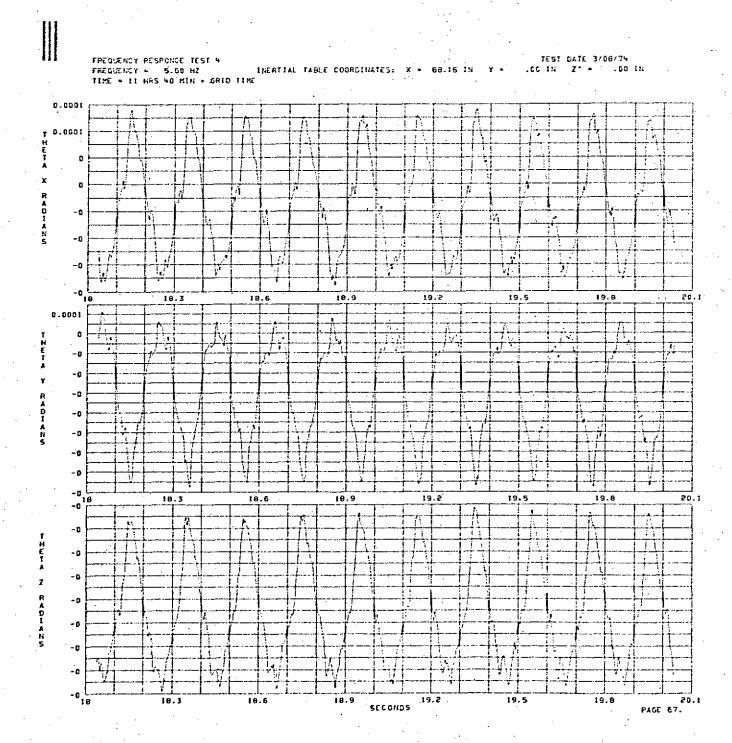


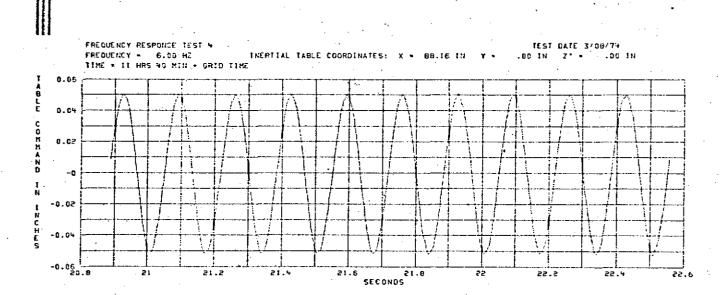
PAGE 63.

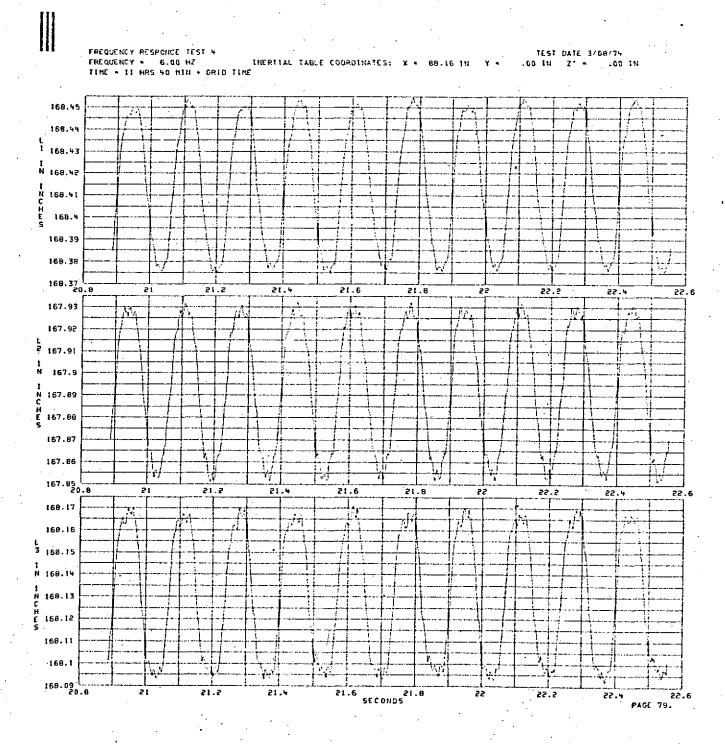


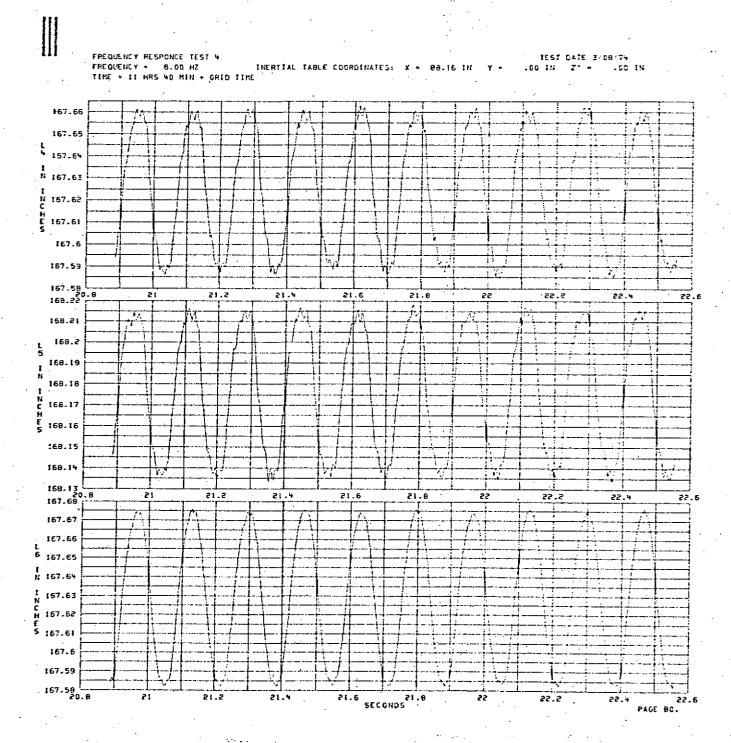


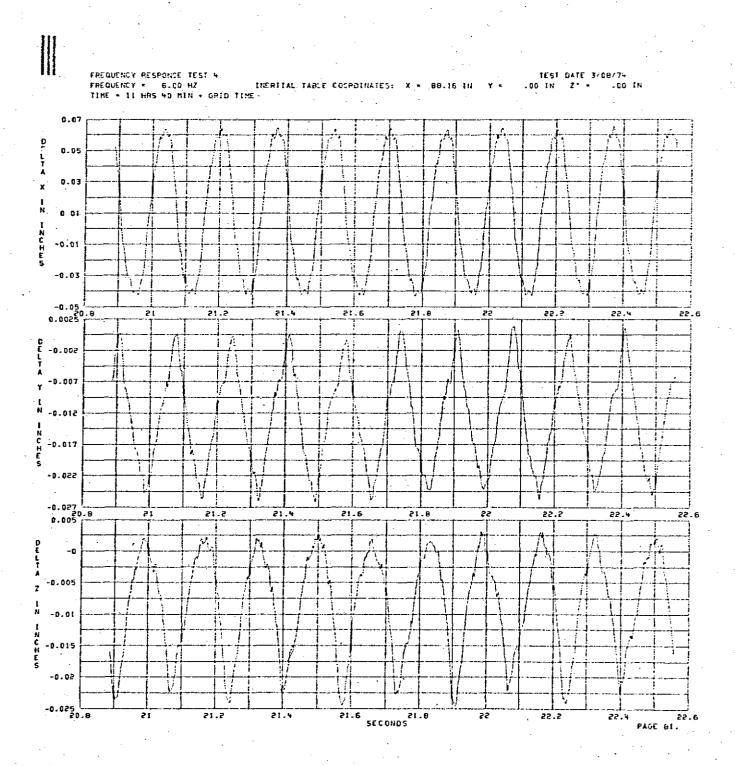


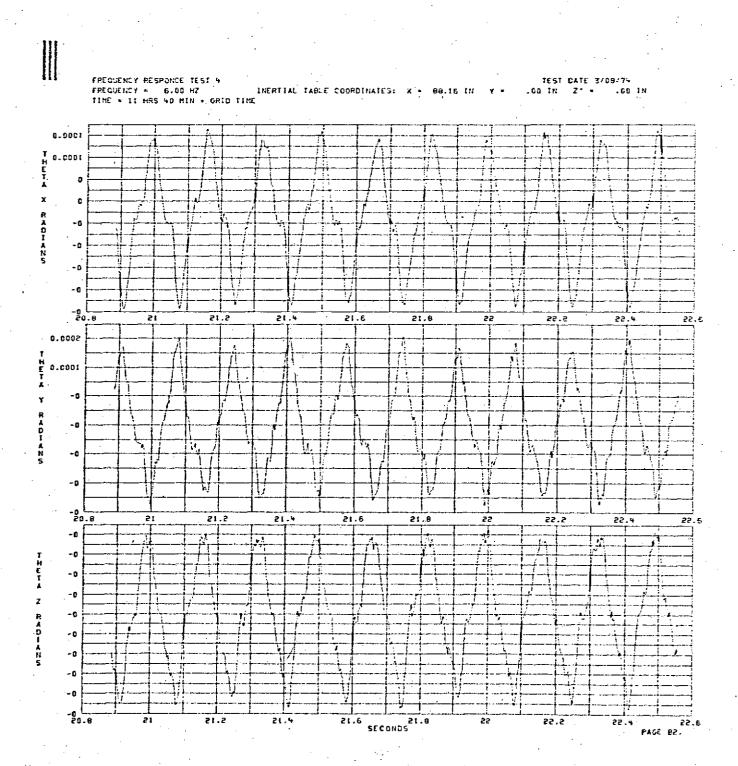


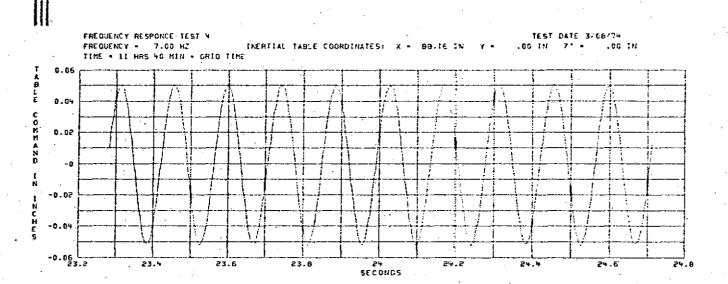




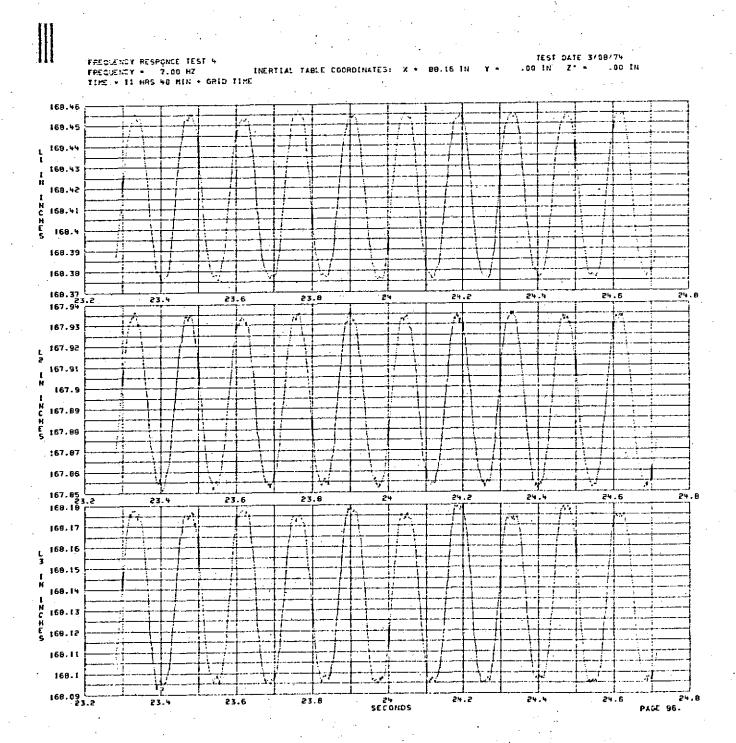


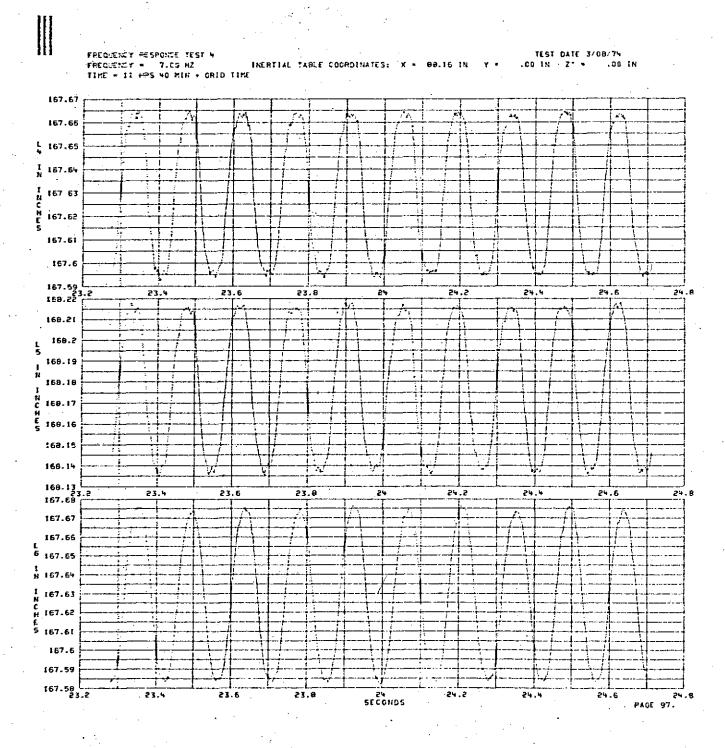


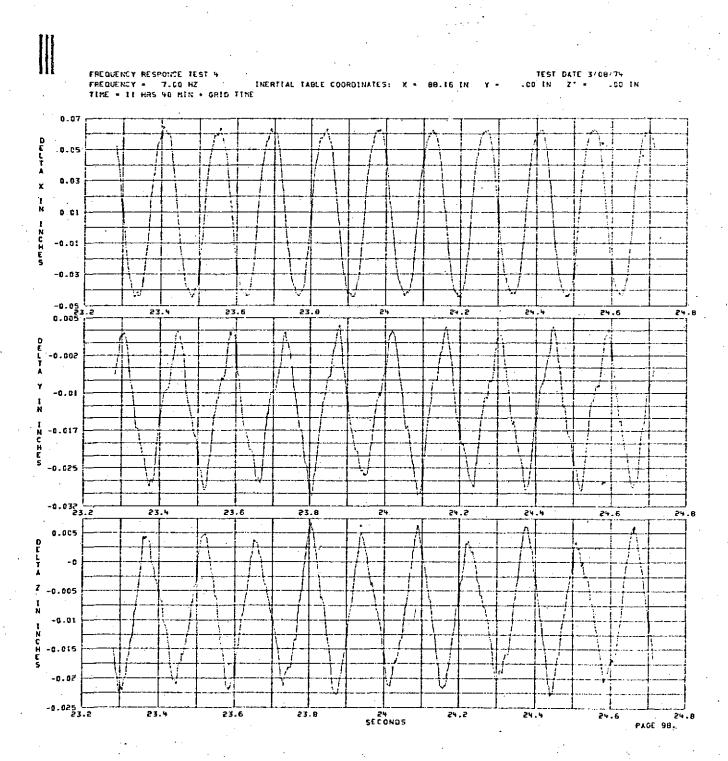


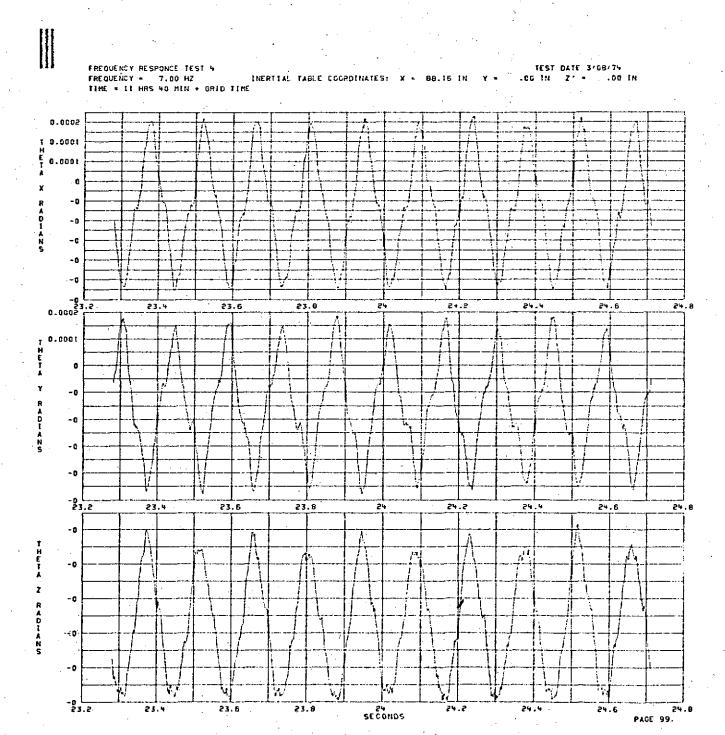


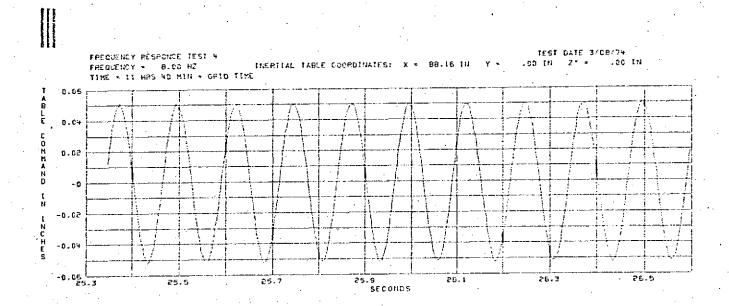
PAGE 95







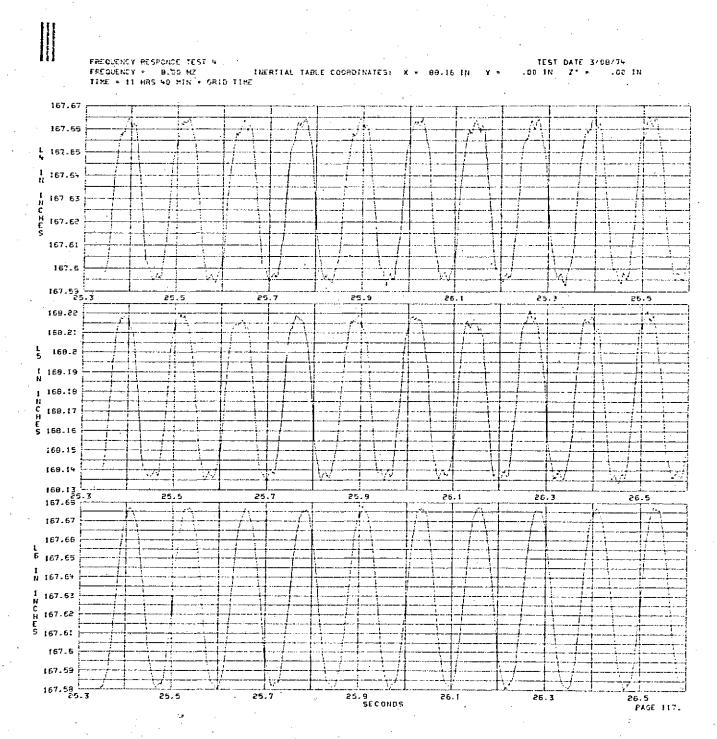


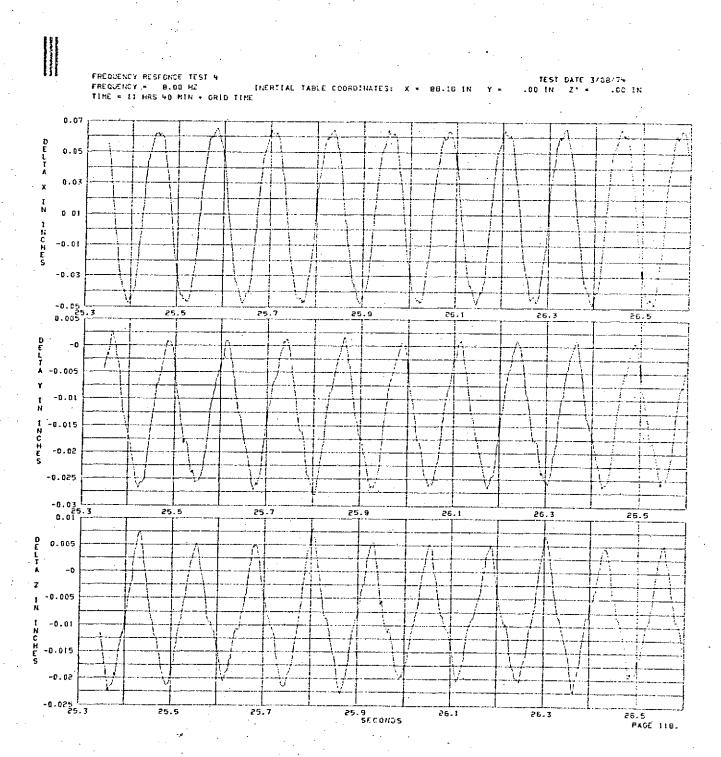


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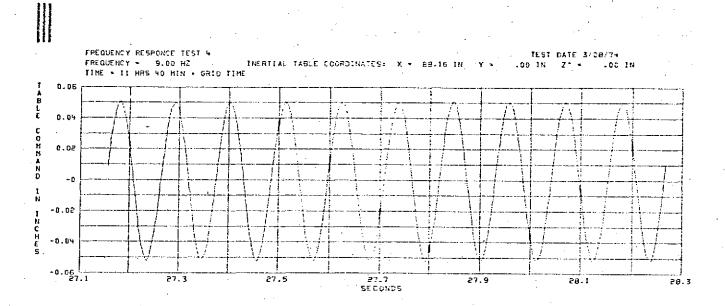
PAGE 115.

TEST DATE 3/08/74 FREQUENCY RESPONCE TEST 4 FREQUENCY = 0.00 HZ TIME = 11 HRS 40 MIN + GRID TIME .DS IN INERTIAL TABLE COORDINATES: X - 88.16 IN 163.46 168.45 168.44 168.43 168.42 C 168.41 168.4 160.39 160.38 169.37 25.3 167.95 26.5 167.94 167.93 ž _{167.92} I N 167.91 167.9 С Н 167.89 E . 5 167.88 167-87 167.86 167.05 25.3 169.18 26.5 26.1 25.5 25.7 25.9 168.17 168.16 l 3_{. 158-15} N 168.14 169.13 C 168.12 160.11 168.1 150.09 159.00 25.9 5ECONOS 26.5 PAGE 115. 25.7 25.5 26.1 26.3

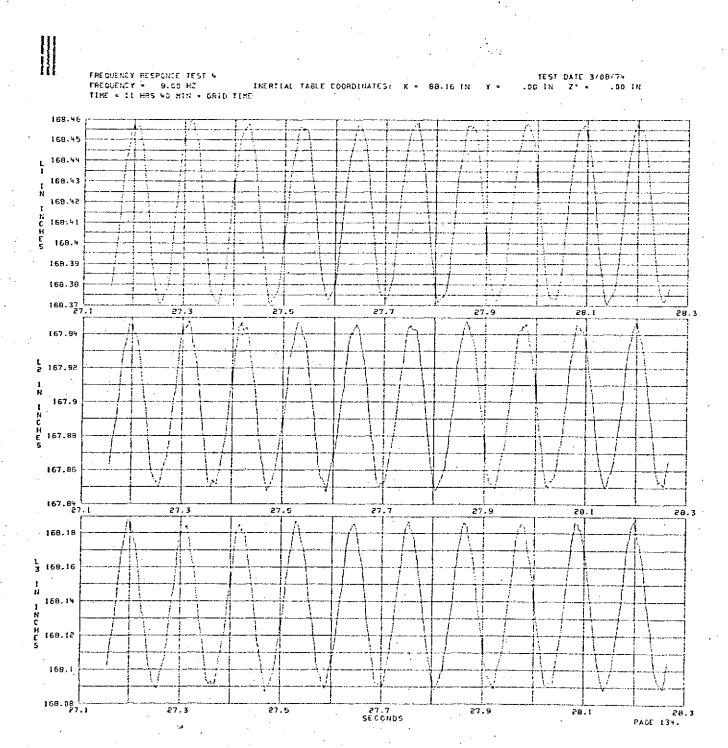


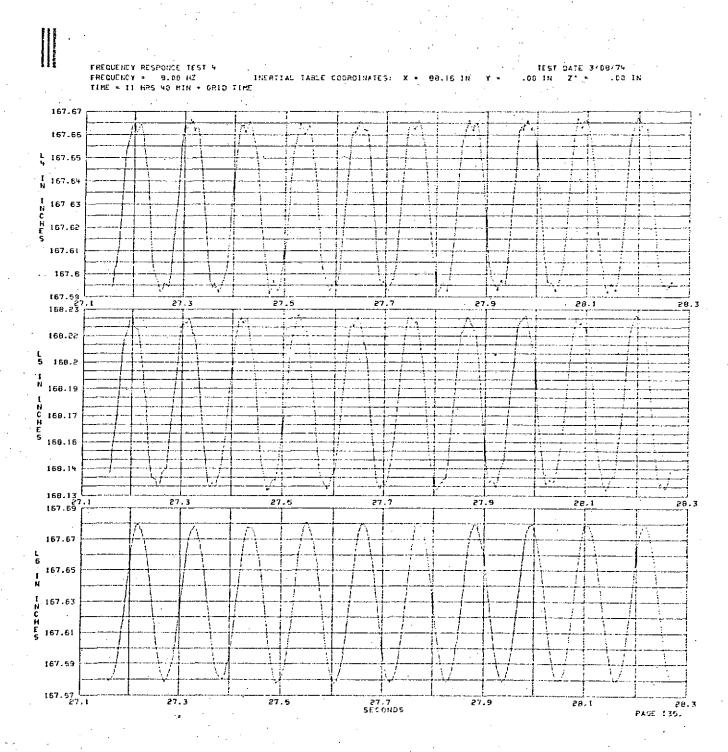


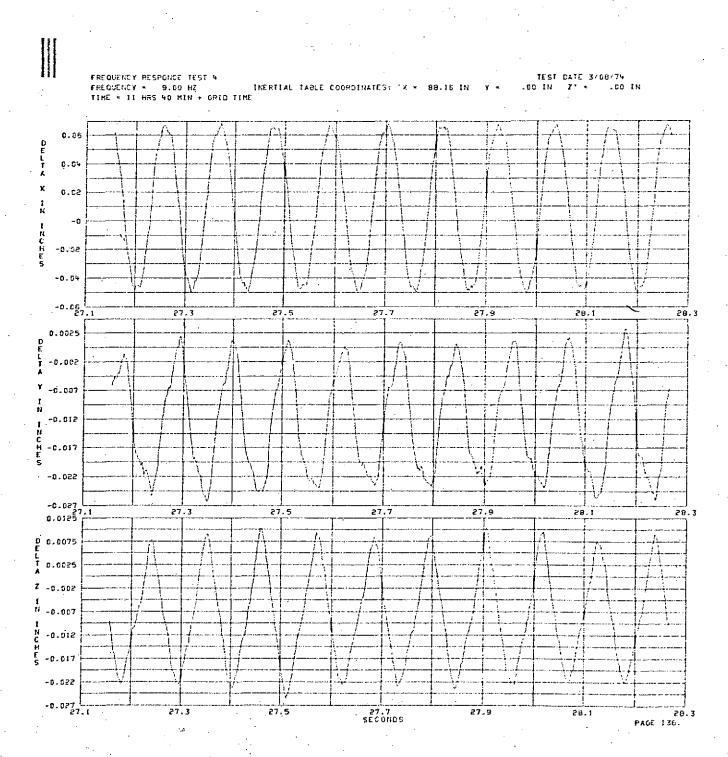
FREQUENCY RESPONCE TEST 4
FREQUENCY = 0.00 HZ 1
TIME = 11 HRS 40 MIN • GRID TIME INERTIAL TABLE COORDINATES: X = 88.16 In .00 IN 9.0002 T 0.0001 H E [T 0.0001 -0 - c -0 25.5 0.0003 (-25.9 0.0002 1000.0 -0 -0 25.3 25.5 25.7 25.9 26.3 26.5. -0 ,- D -0 -0 <u>L</u> 25.3 25.5 25.9 5600NDS 25.7 26.1 26.3 26.5 PAGE 119.

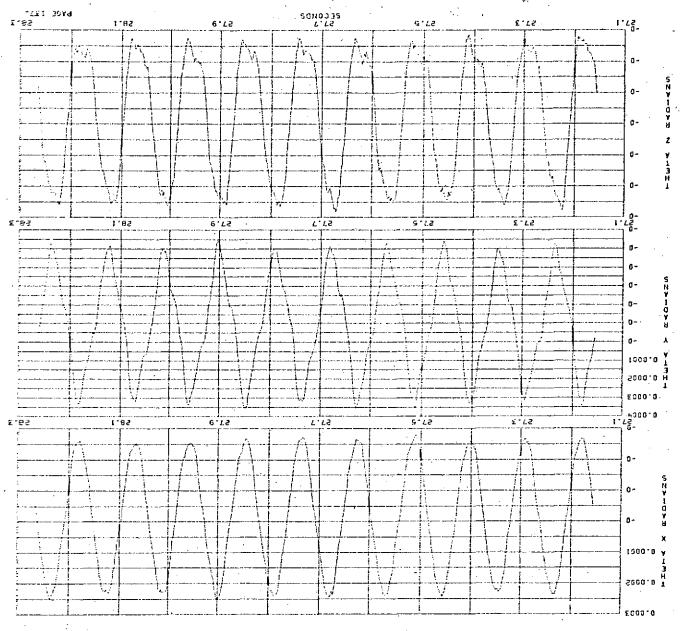


PAGE 133.

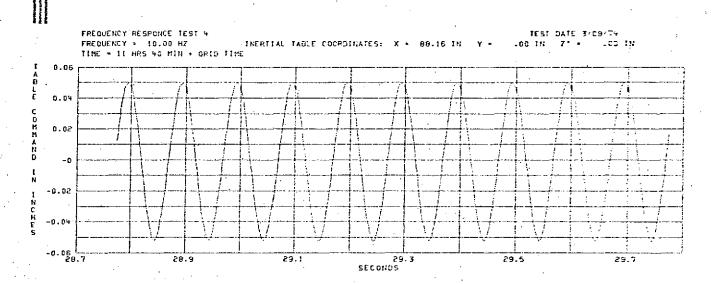




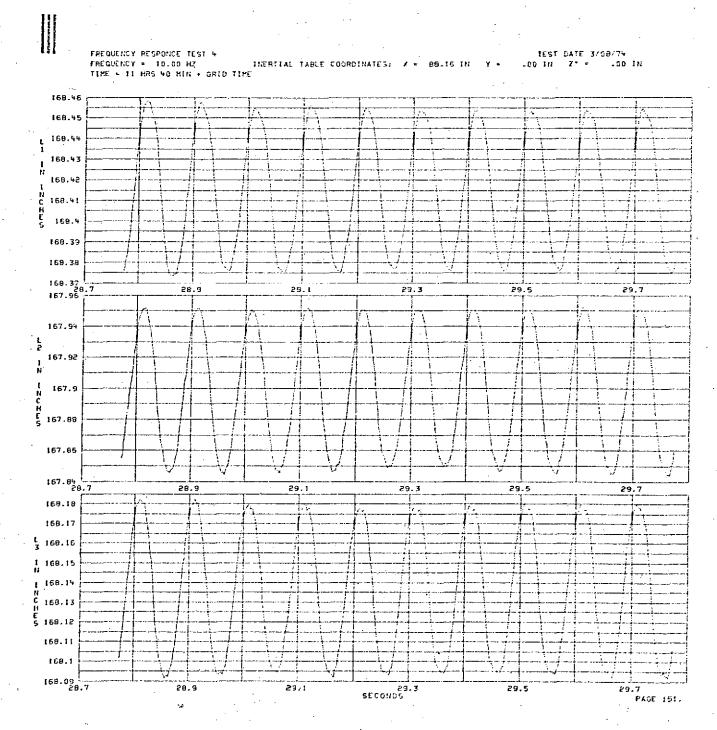


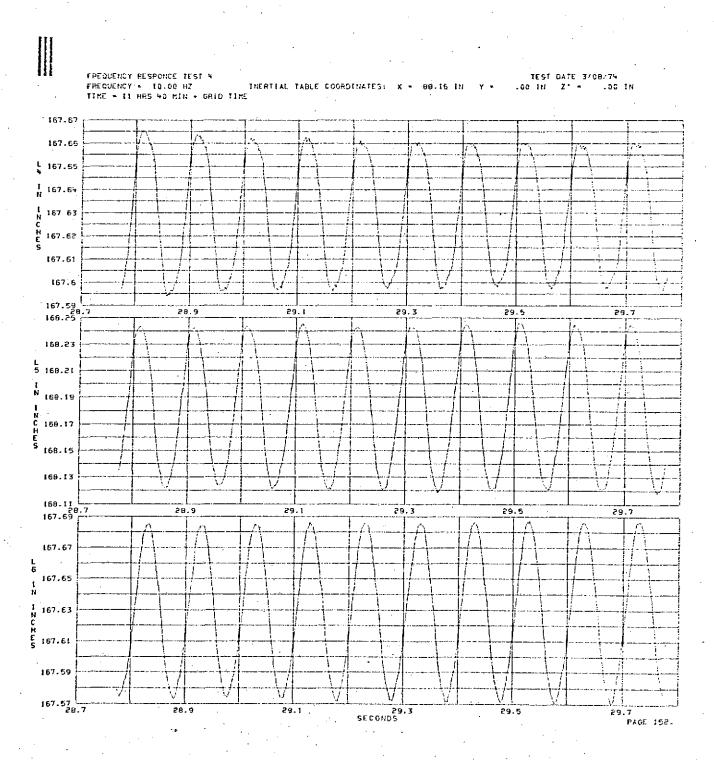


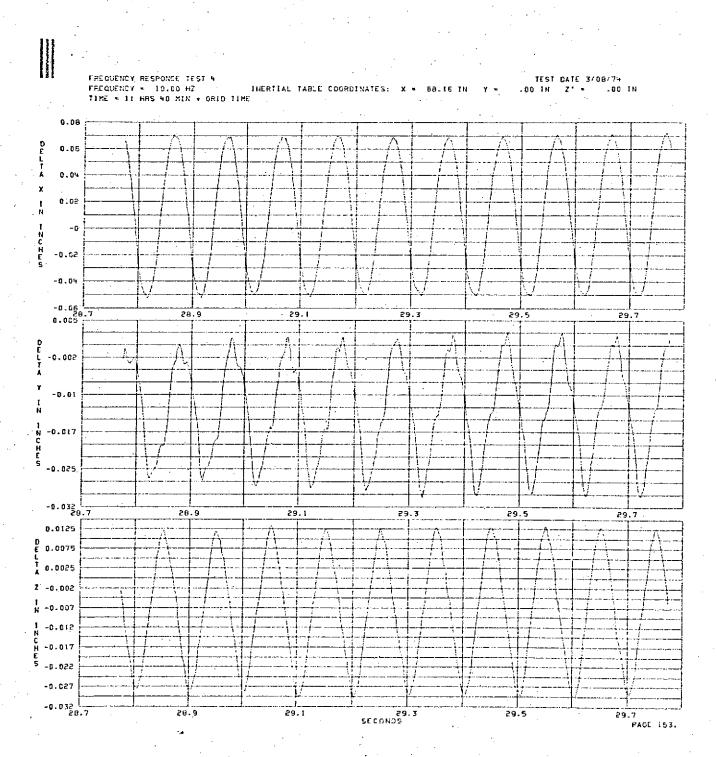
FREQUENCY RESPONSE 1531 + 1231 + 1

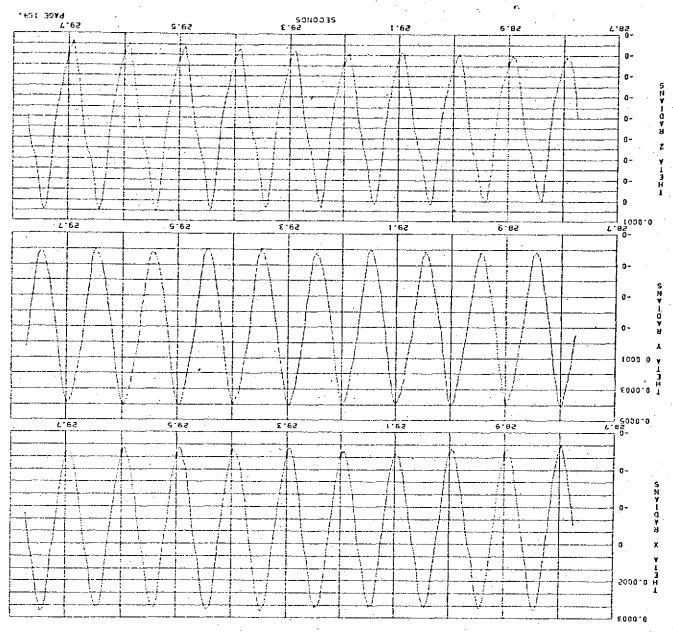


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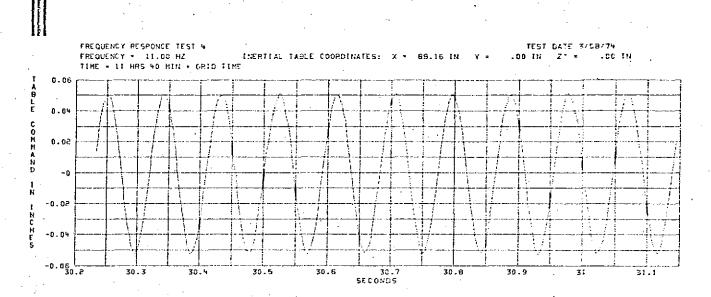




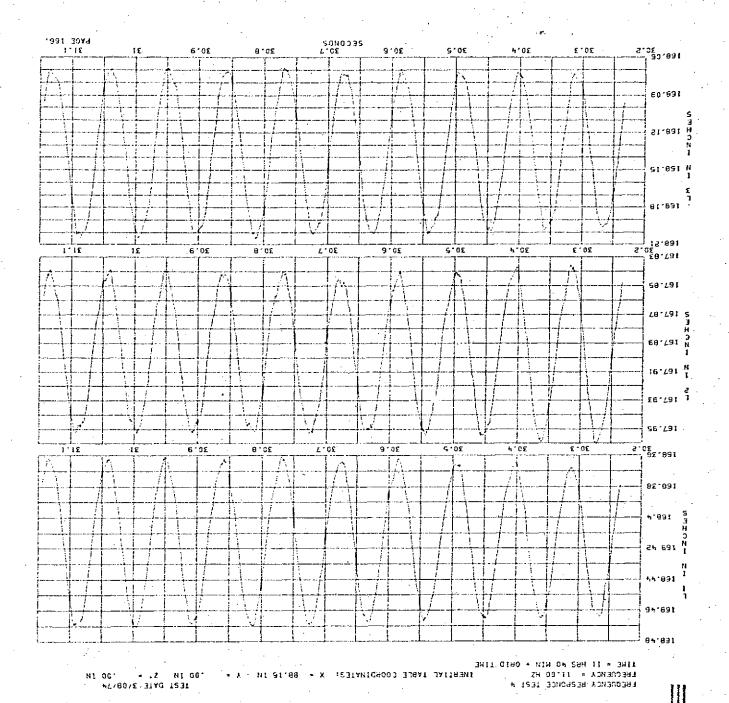


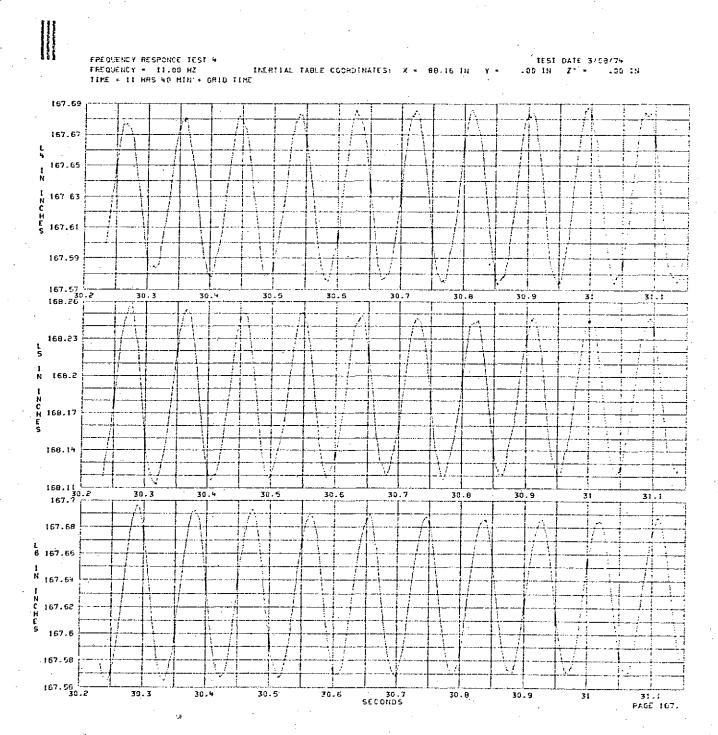
THE CUENCY RESPONCE TEST θ THERTIAL TABLE COORDINATES: X = 88.16 IN FREDENCY = 10.406 HZ THE THE TABLE COORDINATES: X = 88.16 IN

47,63/E.3.30 T23T NI 00. - 'S MI 00.



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FREQUENCY RESPONCE TEST 4
FREQUENCY = 11.00 H2
TIME = 11 HRS 40 MIN + GRID TIME INERTIAL TABLE COORDINATES: 89.16 lu 0.09 0.07 0.05 0.03 0 01 -0.01 -0.03 0.03 0.02 0.01 -0 -0.01 -0.02 -0.03 -0.04 -0.06 30.7 30.3 30.8 30.9 31.1 0.6025 -0.005 -0.012 -0.02 -0.027 30.3 30.4 30.5 30.6 30.7 SECDIDS 30.8 30.9 31 31.1 PAGE 168.

TEST DATE 3/09-74 FREQUENCY RESPONCE TEST 4

FREQUENCY = 11.00 HZ INERTIAL TABLE COORDINATES; X = 88.16 in

TIME = 11 HRS 40 Hin + GRID TIME 0.0004 0.0003 B 0.0002 0.0001 Û -0 ~0 -9 -0 S.0200.0 30.4 30.5 30.€ 30.7 30.9 30.3 39.8 0,8604 0.0002 - 0 -0 -0 30.5 30.4 30.5 30.3 30.G 30.7 30.8 30.9 14 -0 -0

30.6

30.5

31

PAGE 169.

30.8

30.9

-0

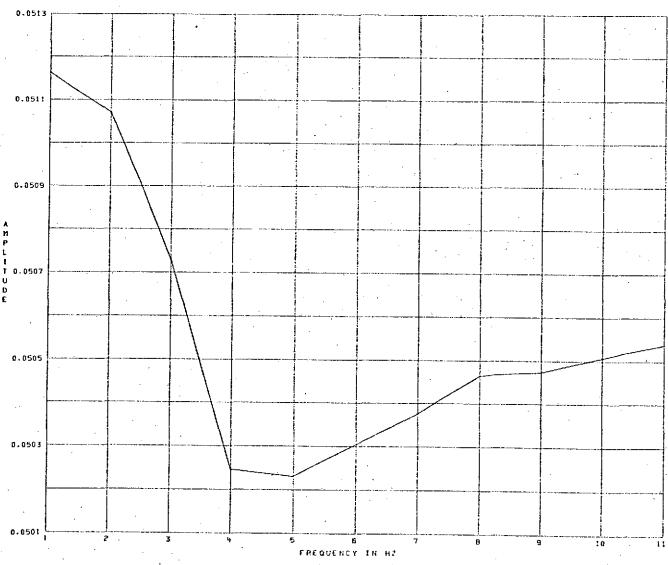
-0 -0

30.2

30.3

DATE PROCESSED - 09APR74

FREQUENCY RESPONCE TEST 4
REFERENCE SENSOR - TÁBCOM
TOTAL CYCLES PROCESSED = 0
FIRST FREQUENCY = 1.00 HZ
BANDMIDTH RANGE FOR FREQUENCY INTERVAL TO 11.00 HZ MAS TOTAL PERIOD PROCESSED *
FREQUENCY INCREMENTS *
1.100 HZ 45.30 SEC 1.00 HZ



PAGE 8.

FREQUENCY RESPONCE TEST 4
SENSOR -DELT X NORMALIZED BY REFERENCE SENSOR -TARCOM
TOTAL CYCLES PROCESSED = 0
FIRST FREQUENCY = 1.00 HZ

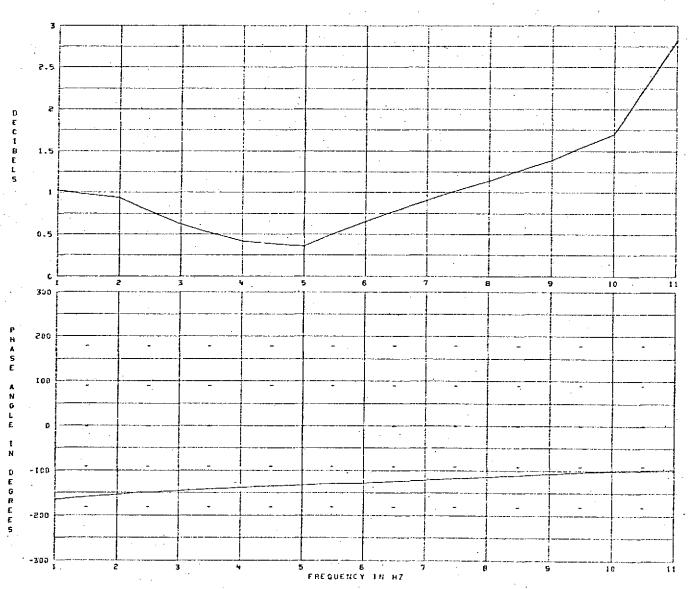
TOTAL PERIOD PROCESSED = FREQUENCY INCREMENTS ==

45.30 SEC 1.00 HZ

DATE PROCESSED - 09APR74

BANDWIDTH RANGE FOR FREQUENCY INTERVAL TO 11.00 HZ WAS

1.100 HZ



PAGE L.

DATE PROCESSED - 094PR74

FREQUENCY RESPONCE TEST 4

SENSOR -DELT Y NORMALIZED BY REFERENCE SENSOR -TABCOM

TOTAL CYCLES PROCESSED = 0

FIRST FREQUENCY = 1.00 HZ

BANDHIDIH HAMSE FOR FREQUENCY INTERVAL TO 11.00 HZ WAS

.100 HZ TO 1.100 HZ

TOTAL PERIOD PROCESSED = FREQUENCY INCREMENTS = 45.30 SEC 1.00 HZ

-2.5 -7.5 -10 -12.5 -15 -17.5 -20 -22.5 -25 10 300 200 100 0 I N -100 -500 -300 6 FREQUENCY IN HZ

PAGÉ 2.

FREQUENCY RESPONCE TEST 4
SENSOR -DELT Z NORMALIZED BY REFERENCE SENSOR -TABCOM
TOTAL CYCLES PROCESSED = D
FIRST FREQUENCY = 1.00 HZ
BANDMIDTH RANGE FOR FREQUENCY INTERVAL TO 11.00 HZ HAS

DATE PROCESSED - 09APR74

TOTAL PERIOD PROCESSED = 45.30 SEC FREGUENCY INCREMENTS = 1.00 HZ

-10 -12 -14 -16 -18 -20 -52 -24 10 300 200 100 D E G R -100 -2¢0 -300 10 FREQUENCY IN HZ

PAGE 3.

-

DATE PROCESSED - 59APR74

FREQUENCY RESPONCE TEST 4

SENSOR -XTHETA NORMALIZED BY REFERENCE SENSOR -TABOON

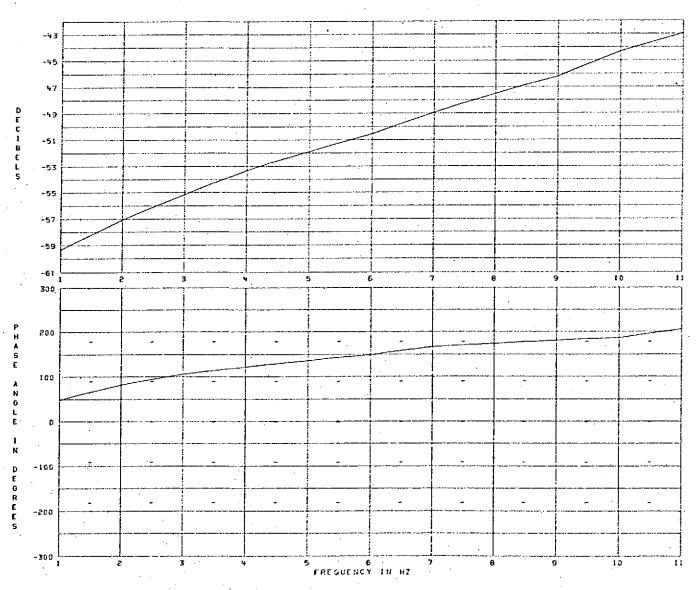
TOTAL CYCLES PROCESSED = 0

FIRST FREQUENCY = 1.00 HZ

BANDWIDTH RANGE FOR FREQUENCY INTERVAL TO 11.00 HZ WAS

TOTAL PERIOD PROCESSED = FREQUENCY INCREMENTS = .100 HZ TO 1.100 HZ

45.30 SEC 1.00 HZ



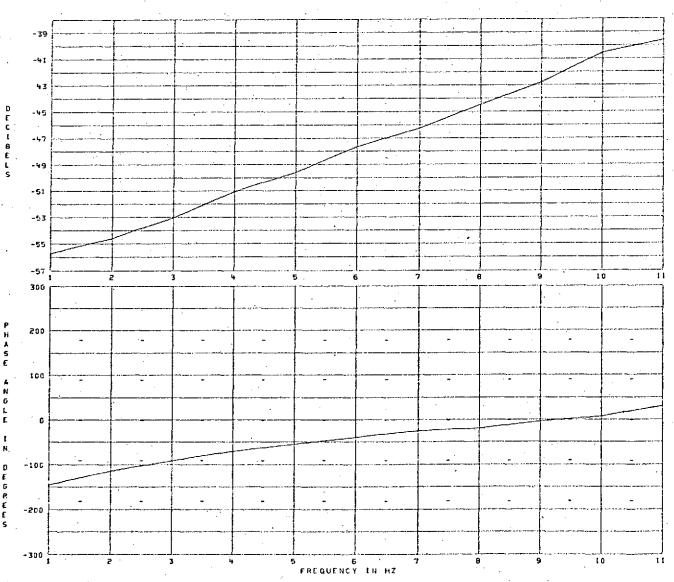
FREQUENCY RESPONCE TEST 4
SENSOR -YTHETA NORMALIZED BY REFERENCE SENSOR -TABCOM
TOTAL CYCLES PROCESSED - 0
FIRST FREQUENCY - 1.00 HZ
BANDWIDTH RANGE FOR FREQUENCY INTERVAL TO 11.00 HZ WAS

DATE PROCESSED - 09APR74

TOTAL PERIOD PROCESSED = FREQUENCY INCREMENTS =

45.30 SEC 1.00 HZ

.100 HZ TO 1.100 HZ



PAGE 5.

DATE PROCESSED - 09APR74

FREDUENCY RESPONCE TEST 4

SENSOR -ZIHETA NGAMALIZED BY REFERENCE SENSOR -TABCOM
TOTAL CYCLES PROCESSED 7 0
FIRST FREDUENCY 1.00 HZ
BANDATOTH RANGE FOR FREQUENCY INTERVAL TO 11.00 HZ WAS

TOTAL PERIOD PROCESSED = FREQUENCY INCREMENTS = 1-100 HZ

.100 HZ TO

45.30 SEC 1.00 HZ

